

# Small Washcoat Diffusion Resistance, Further Developments

Edward J Bissett



# Review and Preview

- Asymptotic solution for small **dimensionless diffusion resistance**,  $D_{inv}$ .
  - Introduced at 2014 CLEERS
  - “An Asymptotic Solution for Washcoat Pore Diffusion in Catalytic Monoliths”, Bissett, **Emission Control Science and Technology**, Vol. 1, No. 1, pp. 3-16 (2015)
- Summary
  - Alternative to approaches using Thiele modulus, ad hoc linearization
  - Recognize that “standard” approach (no washcoat gradients) is  $D_{inv} = 0$  limit.
  - Generalize to  $O(D_{inv})$  to capture dominant effects of small diffusion resistance.
  - Practical aftertreatment regime of catalyst effectiveness,  $D_{eff} \approx O(10^{-6} \text{ m}^2/\text{s})$
  - Permits all features common to standard approach
    - Large, fully nonlinear reaction system
    - Many species, coverages
  - Also dual washcoat layers
  - Equivalent computational speed
- Preview
  - How does this asymptotic solution fit with other approximations using Thiele modulus?
  - Small concentrations and mass transport limits

# Connections with Thiele modulus

- Asymptotic **solution** of **nonlinear** reaction/diffusion equations
  - No linearizations to obtain effectiveness factors or internal mass transfer coefficients
  - Large systems of reactions, species, coverages
- However, can still do “**simplest problem**”, single-species, linear reactant:

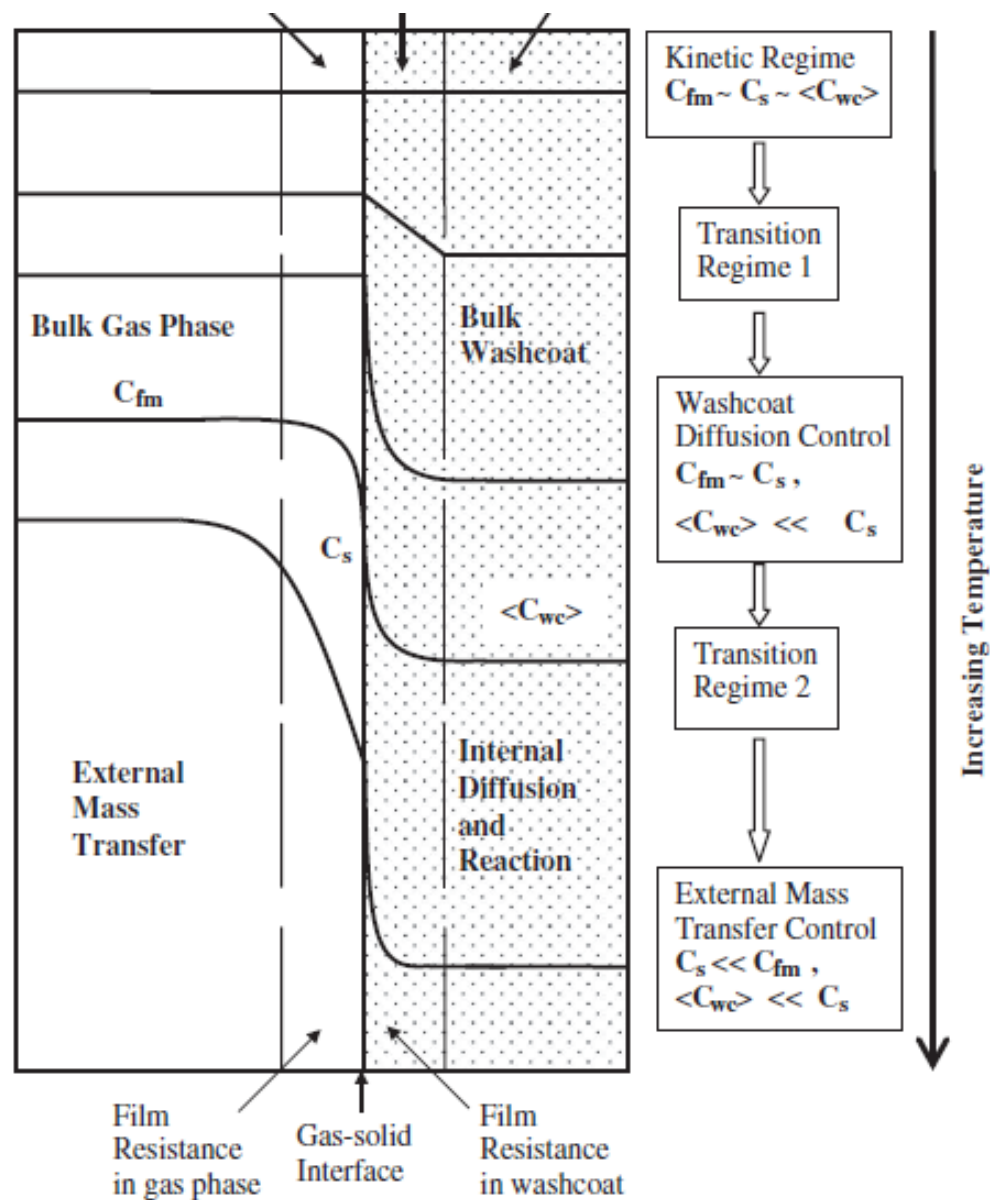
$$\frac{\partial^2 \omega}{\partial x^2} = \varphi^2 \omega \quad 0 < x < 1$$

$$\frac{\partial \omega}{\partial x} = Bi(\omega - \omega_g) \quad x = 0$$

$$\frac{\partial \omega}{\partial x} = 0 \quad x = 1$$

- Thiele modulus,  $\varphi$ , satisfies  $\varphi^2 = D_{inv}(-R/\omega)$  with rate constant,  $k = -R/\omega$
- Biot number,  $Bi = D_{inv}K$ , controls size of gradients on each side of interface
- $D_{inv} \ll 1$  limit requires both  $\varphi$  and  $Bi$  small
- Sometimes done with simpler B.C.,  $\omega = 1$  at  $x = 0$ , but this obscures key points.
- Complete asymptotic analysis
  - Inspired by figure in “Overall mass transfer coefficients and controlling regimes in catalytic monoliths”, Joshi et al., Chemical Engineering Science, Vol. 65, pp. 1729-1747(2010), Figure 2.

Figure 2 from Joshi, et al. (2010)



# Breakdown for all asymptotic regimes for single linear reactant

- Full solution available,
  - e.g., “The Mathematical Theory of Diffusion and Reaction in Permeable Catalysts, Volume I, The Theory of the Steady State” Aris, Oxford University Press (1975)
- Either from full solution or governing equations. Simple exercise
- First divide into  $Bi$  regimes, then  $\varphi$
- Some regimes are “distinguished limits”, some are transitional sublimits

$$Bi = O(1)$$

$\varphi^2 \ll 1$	$\omega(x) \sim \omega_g \left[ 1 - \varphi^2 \left( 1/Bi + x - x^2/2 \right) \right]$	$\omega_g \approx \omega_s \approx \bar{\omega}$
$\varphi^2 = O(1)$	$\omega(x) = \frac{\omega_g}{\cosh \varphi + (\varphi/Bi) \sinh \varphi} \cosh(\varphi(1-x))$	$\omega_g > \omega_s > \bar{\omega}$
$\varphi^2 \gg 1$	$\omega(x) \sim \frac{\omega_g Bi}{\varphi} \exp(-\varphi x)$	$\omega_g \gg \omega_s \gg \bar{\omega}$

- Down: increasing temperature
- Blue: kinetic control,  $\omega_g \approx \bar{\omega}$
- Red: mass transfer control,  $\omega_g \gg \omega_s$
- Mass transfer control =>
  - Kinetics fast enough that channel gas “sees” no surface concentration
  - Channel gas satisfies  $W \frac{\partial \omega_g}{\partial z} = -K \omega_g$
  - **Reactor output independent of** local solution of **reaction/diffusion problem** in washcoat

# $Bi \gg 1$

$\varphi^2 \ll 1$	$\omega(x) \sim \omega_g \left[ 1 - \varphi^2 \left( 1 / Bi + x - x^2 / 2 \right) \right]$	$\omega_g \approx \omega_s \approx \bar{\omega}$
$\varphi^2 = O(1)$	$\omega(x) \sim \frac{\omega_g}{\cosh \varphi} \cosh(\varphi(1-x))$	$\omega_g \approx \omega_s > \bar{\omega}$
$Bi \gg \varphi^2 \gg 1$	$\omega(x) \sim \omega_g \exp(-\varphi x)$	$\omega_g \approx \omega_s \gg \bar{\omega}$
$\varphi^2 = O(Bi)$	$\omega(x) \sim \frac{\omega_g}{(1 + \varphi / Bi)} \exp(-\varphi x)$	$\omega_g > \omega_s \gg \bar{\omega}$
$\varphi^2 \gg Bi$	$\omega(x) \sim \frac{\omega_g Bi}{\varphi} \exp(-\varphi x)$	$\omega_g \gg \omega_s \gg \bar{\omega}$

- Corresponds to Joshi paper figure ( $D_{eff} \approx O(10^{-7} \text{ m}^2/\text{s})$ )
  - e.g.,  $\omega_g \approx \omega_s \gg \bar{\omega}$  only occurs when  $Bi \gg 1$
- As temperature ( $\varphi^2$ ) increases,  $\omega_s \gg \omega$  before  $\omega_g \gg \omega_s$
- Kinetic and transport control occur in only 1 extreme regime each

# $Bi \ll 1$

$\varphi^2 \ll Bi$	$\omega(x) \sim \omega_g \left[ 1 - \varphi^2 \left( 1 / Bi + x - x^2 / 2 \right) \right]$	$\omega_g \approx \omega_s \approx \bar{\omega}$
$\varphi^2 = O(Bi)$	$\omega(x) \sim \frac{\omega_g}{1 + \varphi^2 / Bi} \left[ 1 + \varphi^2 \left( \frac{\varphi^2 / (3Bi)}{1 + \varphi^2 / Bi} - x + x^2 / 2 \right) \right]$	$\omega_g > \omega_s \approx \bar{\omega}$
$Bi \ll \varphi^2 \ll 1$	$\omega(x) \sim \frac{\omega_g Bi}{\varphi^2} \left\{ 1 - Bi / \varphi^2 - \varphi^2 \left[ 1 / 6 - (1 - x)^2 / 2 \right] \right\}$	$\omega_g \gg \omega_s \approx \bar{\omega}$
$\varphi^2 = O(1)$	$\omega(x) \sim \frac{\omega_g Bi}{\varphi \sinh \varphi} \cosh(\varphi(1 - x))$	$\omega_g \gg \omega_s > \bar{\omega}$
$\varphi^2 \gg 1$	$\omega(x) \sim \frac{\omega_g Bi}{\varphi} \exp(-\varphi x)$	$\omega_g \gg \omega_s \gg \bar{\omega}$

- Our case of interest ( $D_{inv} \ll 1$ ):  $Bi = D_{inv} K \ll 1$  and  $\varphi^2 = D_{inv} (R / \omega) = O(Bi)$ 
  - Closest regime to “standard”,  $D_{inv} = 0$
  - 1<sup>st</sup> and 3<sup>rd</sup> rows are included sublimits of 2<sup>nd</sup> row
- Mass transport limitation achieved even while  $\varphi^2 \ll O(1)$
- **Solution in washcoat does not affect reactor output ( $\omega_g$ ) for  $\omega_g \gg \omega_s$**



## $D_{inv} \ll 1$ for large nonlinear systems

- Review from asymptotic solution (e.g. single layer)

$$K \left[ \omega_s(\bar{\omega}, \bar{R}) - \omega_g \right] = \bar{R}, \quad \bar{R} = R(\bar{\omega})$$

- used in determining  $\bar{\omega}$
- Solution:  $\omega(x) = \bar{\omega} + D_{inv} \bar{R} \left[ 1/6 - (1-x)^2 / 2 \right]$
- Consider reactant,  $i$ ,  $\bar{R}_i < 0$ ,  $\phi_i^2 = -D_{inv,i} \bar{R}_i / \bar{\omega}_i = O(D_{inv})$ 
  - If we increase  $\phi_i^2$  greater than  $O(D_{inv})$ :
    - “Simplest problem”  $\rightarrow$  mass transfer limit before  $O(1)$
    - In general problem, cannot make rate more negative than  $-K_i \omega_{gi}$
    - Instead, decrease  $\bar{\omega}_i \rightarrow 0$
    - Flat profiles, ( $D_{inv} \ll 1$ ,  $\bar{R}$  bounded,  $O(1)$ )  $\rightarrow \omega_s \rightarrow 0$
    - Transport limitation. Do not need detailed washcoat solution.
- Asymptotic solution depends on approximately flat profiles
  - Breakdown with increasing  $\phi_i^2$  manifests as  $\omega(x) < 0$

# Small concentration problem

- Can't get, don't need (mass transport) accurate asymptotic solution for  $\varphi_i^2 = O(1)$  or larger
- Can't tolerate negative concentrations
- Several strategies attempted
  - Dual layer hardest, especially layer 1 reactant, layer 2 product
  - Must respect asymptotic solution for  $\varphi_i^2 \ll 1$ , where needed and applicable
  - Can introduce/manipulate higher-order terms:  $D_{inv}^2$  and higher
- Best strategy so far – hyperbolic functions from “simplest problem”

# Maintain positive washcoat profiles

- Each species handled individually (suppress subscript)
- For products, rates positive, no changes required:
  - Layer 1:  $\omega(x) = \bar{\omega}^{(1)} + D_{inv}^{(1)} \bar{R}^{(1)} [1/6 - (1-x)^2/2] + D_{inv}^{(1)} \bar{R}^{(2)} (x - 1/2)$
  - Layer 2:  $\omega(x) = \bar{\omega}^{(2)} + D_{inv}^{(2)} \bar{R}^{(2)} [1/6 - (2-x)^2/2]$
- Positivity requires arguments from algebraic equations for  $\bar{\omega}^{(1)}$  and  $\bar{\omega}^{(2)}$
- For reactants,  $\bar{R} < 0$ 
  - Layer 1:  $\omega(x) = \bar{\omega}^{(1)} \varphi^{(1)} \frac{\cosh(\varphi^{(1)}(1-x))}{\sinh \varphi^{(1)}} + D_{inv}^{(1)} \bar{R}^{(2)} \frac{\sinh(\varphi^{(1)}(x-1/2))}{\varphi^{(1)} \cosh(\varphi^{(1)}/2)}$
  - Layer 2:  $\omega(x) = \bar{\omega}^{(2)} \varphi^{(2)} \frac{\cosh(\varphi^{(2)}(2-x))}{\sinh \varphi^{(2)}}$
  - When expanded for small  $\varphi$ , these **agree with original formulas**.
  - Maintains  $\omega(x) \geq 0$  for all  $\varphi$
  - Downsides: hyperbolic evaluations and increased nonlinearity of profiles

# Review and Conclusions

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- Considerable experience in complex, challenging problems since last year. Current release of GT-Suite.
- Increasing Thiele modulus cannot not make the rate larger than the finite external mass transfer limit. It makes the washcoat concentrations small.
- Clarified how mass transport limit and small Biot number allows us to finesse large concentration gradients of large Thiele modulus
- Avoid negative concentrations for large Thiele modulus by adding higher-order terms that convert washcoat profiles from simpler linear functions of the rates to hyperbolic functions.
- Plan a research note to archive hyperbolic function modification