

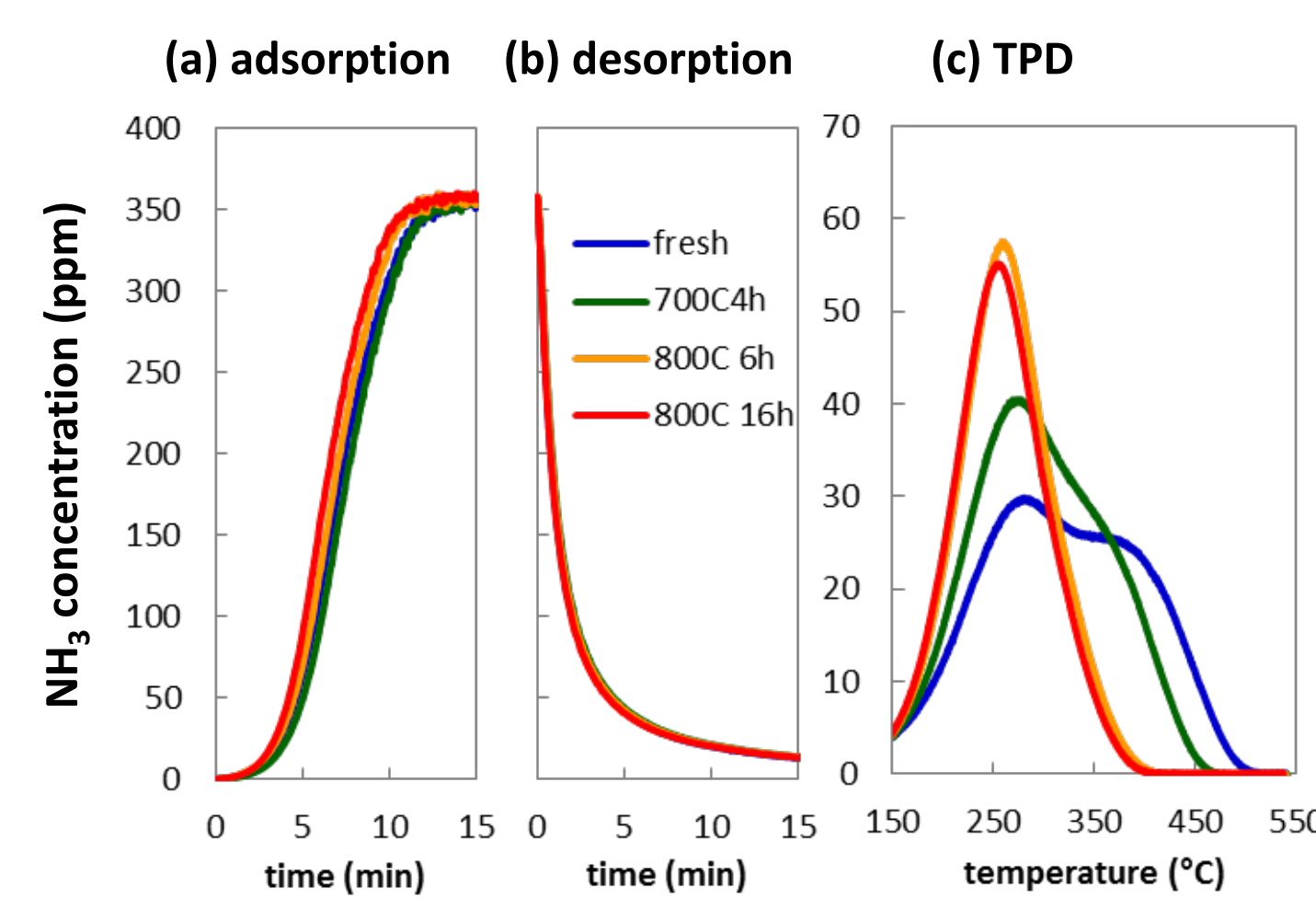
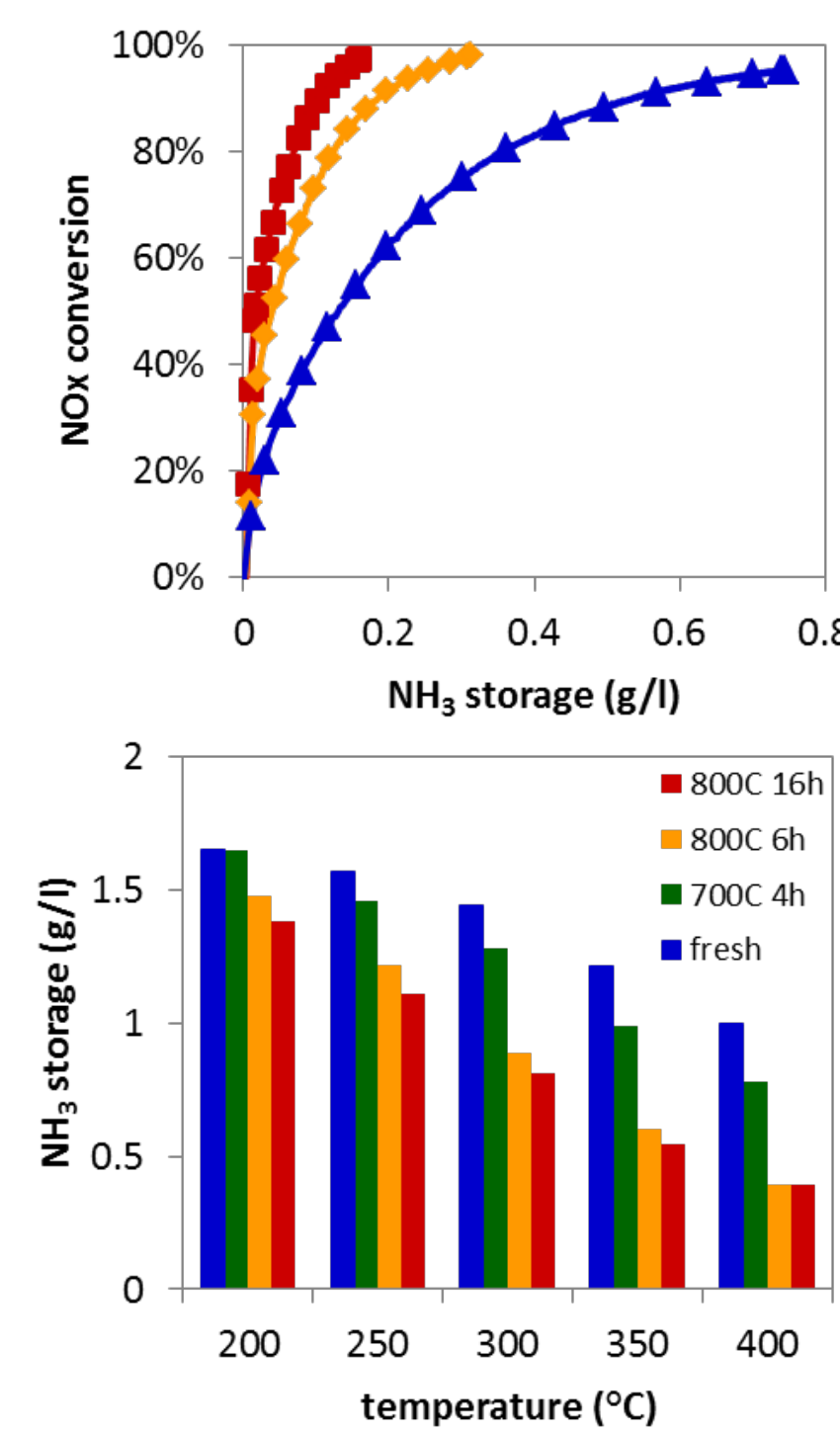
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Motivation

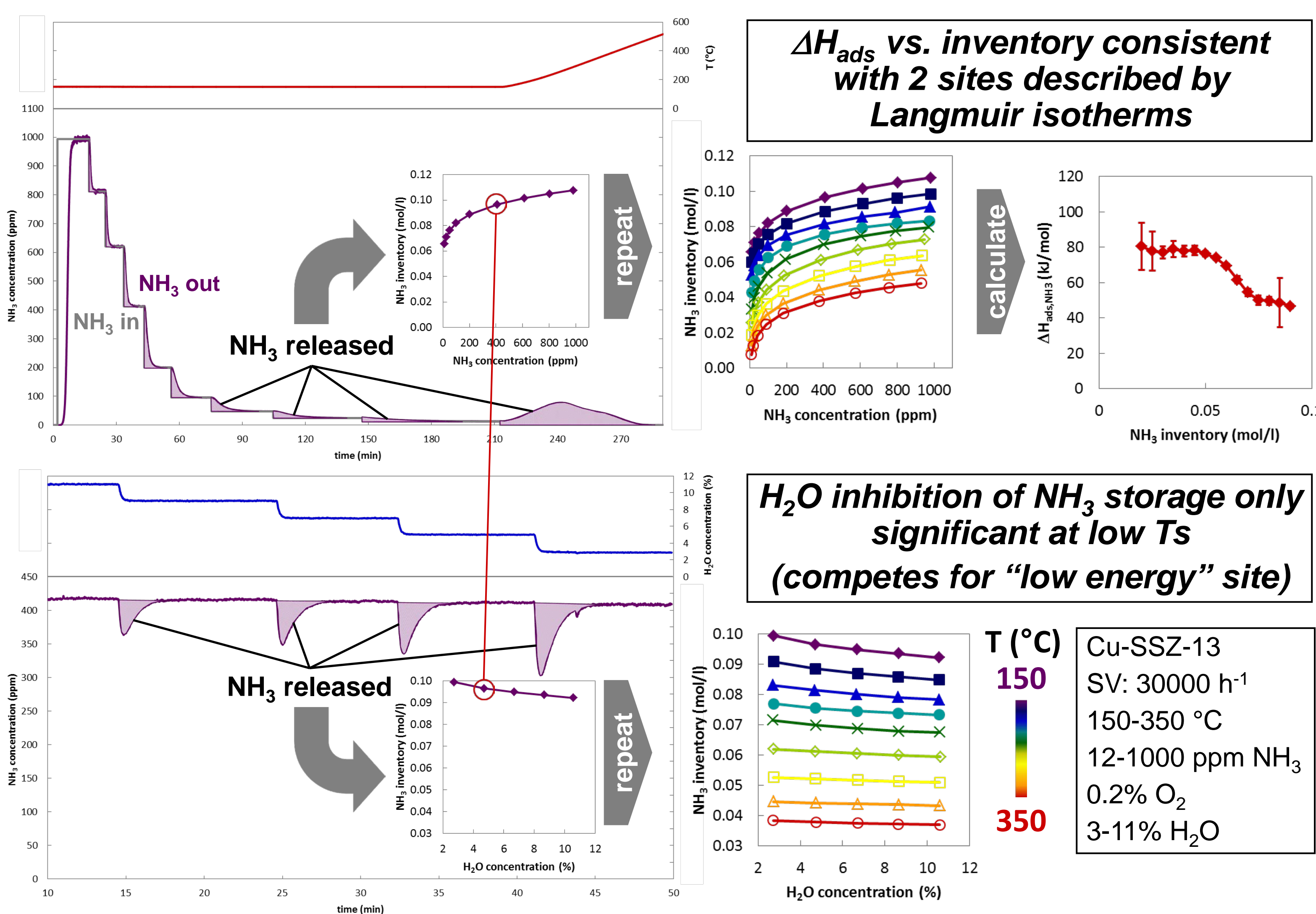
- SCR NH₃ inventory must be managed to:
 - maintain high NOx conversion
 - avoid NH₃ slip and wasted reductant
- NH₃ inventory is controlled through reductant dosing
- Dosing strategies are often developed with simulations
- Simulation tools require NH₃ storage models that accurately capture the effects of:
 - catalyst temperature
 - exhaust composition
 - catalyst age
- Typical NH₃ storage measurements [1] rely on transient operating conditions, confounding effects of:
 - thermodynamics
 - adsorption/desorption kinetics
 - transport processes
- SCR catalyst structure/properties and modeling strategies remain uncertain:
 - multiplicity, quantity of storage sites
 - energetics of adsorption at each site
 - Langmuir, Temkin, etc.
 - role of competitive adsorption
 - aging impacts
- Confounded experimental data sets and uncertain model structures create too many degrees of freedom for unique parameter estimation
- Better measurement and modeling strategies are needed



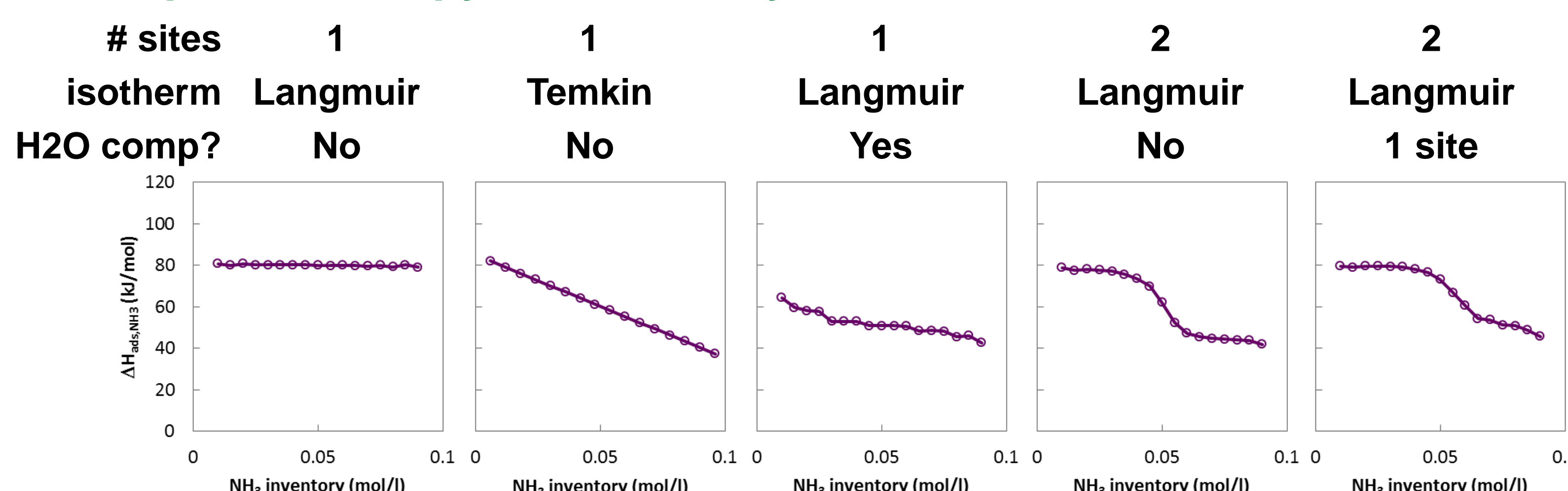
Approach

- Use an automated flow reactor to measure steady state NH₃ inventories on core samples cut from commercial SCR catalysts
 - vary NH₃ concentration (isotherms), temperature, H₂O concentration
 - isolates energetics from kinetics and transport
- Extract adsorption enthalpies from isotherms with thermodynamic relation:

$$\text{Clausius-Clapeyron equation: } \frac{\partial(\ln P_{NH_3})}{\partial(1/T)} = \frac{\Delta H_{ads}}{R}$$



Adsorption enthalpy vs. inventory for model isotherms



Adsorption enthalpy vs. inventory curve guides selection of modeling strategies by providing insights into site multiplicity, adsorption energetics

References

1. E. Tronconi et. al, Chem. Eng. Sci. 51, 2965, 1996
2. S. Schmiege et. al, Catal. Today, 184, 252-261, 2011

Equilibrium storage model equations

$$I_{NH_3} = \omega_1 \theta_{1,NH_3} + \omega_2 \theta_{2,NH_3}$$

$$\theta_{1,NH_3} = \frac{K_{1,NH_3} P_{NH_3}}{1 + K_{1,NH_3} P_{NH_3}}$$

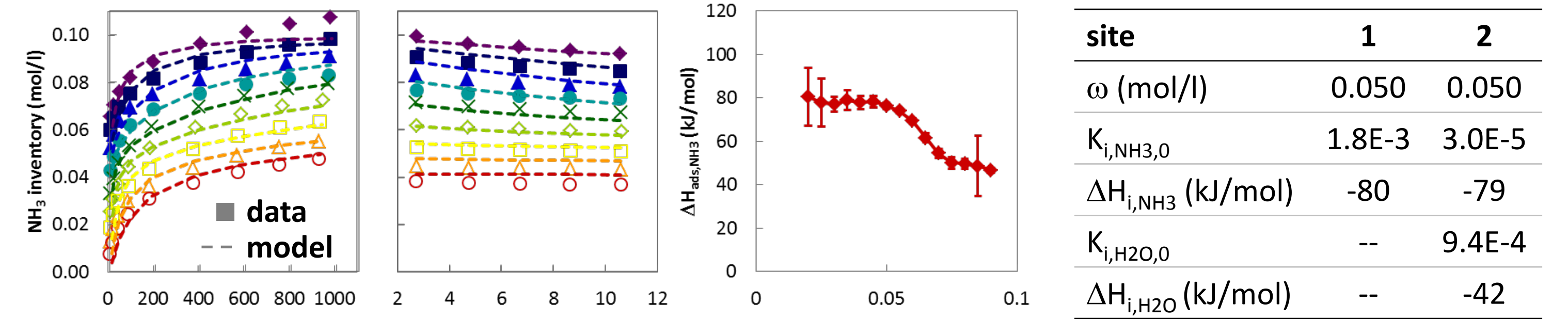
$$\theta_{2,NH_3} = \frac{K_{2,NH_3} P_{NH_3}}{1 + K_{2,NH_3} P_{NH_3} + K_{2,H_2O} P_{H_2O}}$$

$$K_{i,a} = K_{i,a,0} e^{-\Delta H_{i,a}/RT}$$

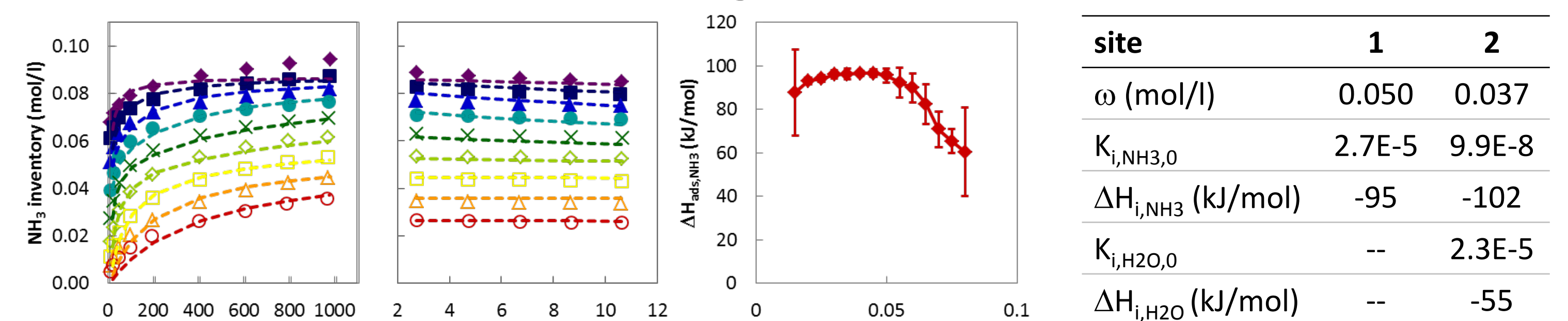
- two distinct storage sites
- site 1: Langmuir isotherm
- site 2: Langmuir isotherm with H₂O competitive adsorption
- both sites: constant adsorption enthalpies (no coverage dependence)

Zeolite composition effects on NH₃ storage

Cu-SSZ-13 (2010 GM pickup truck)

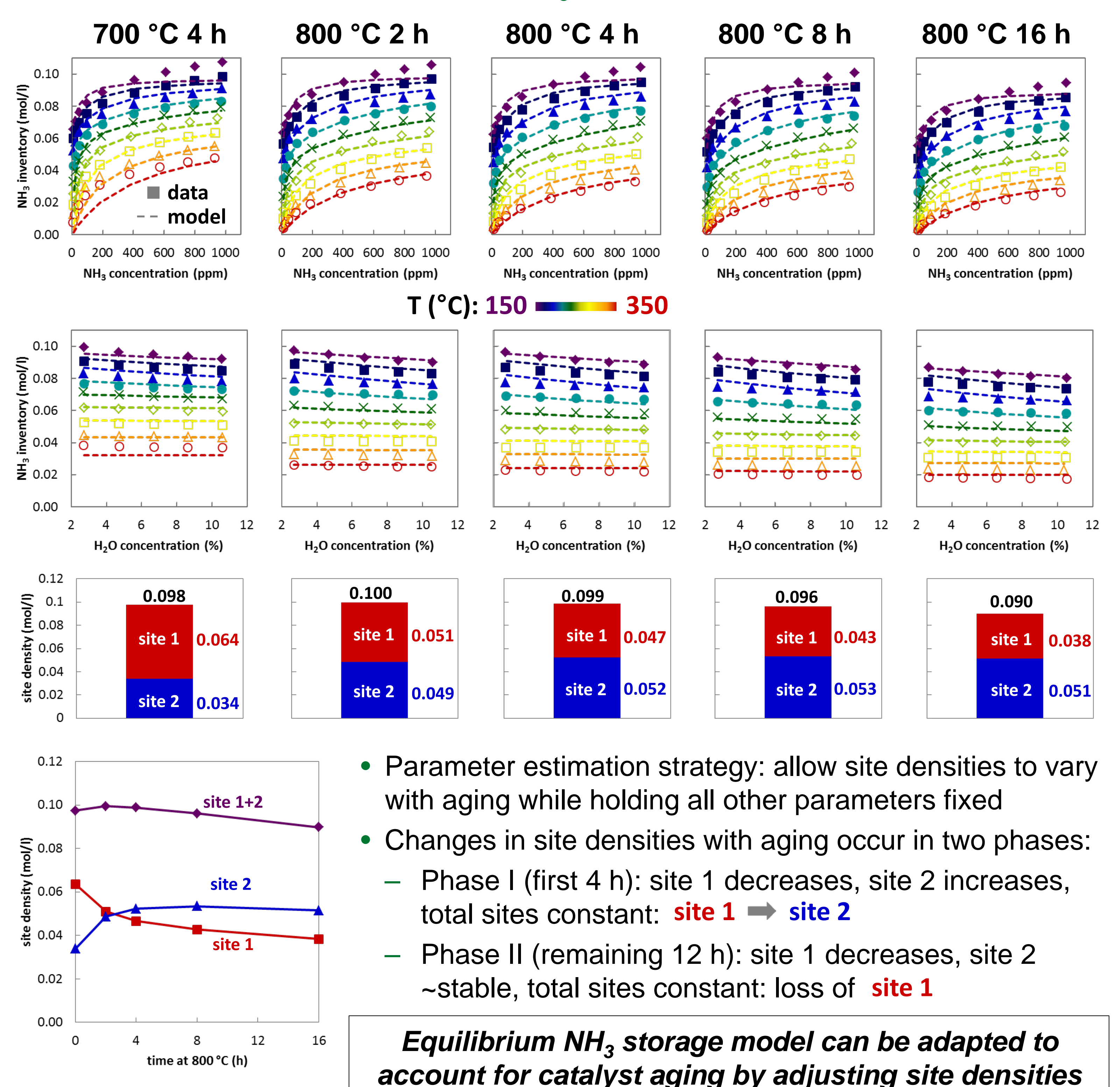


Cu-SAPO-34 (2010 Cummins ISB engine)



2 site model with constant adsorption enthalpies and H₂O competition at one site effectively captures NH₃ storage behavior on two commercial small pore copper zeolites with very different compositions

Hydrothermal aging effects on NH₃ storage over Cu-SSZ-13



Equilibrium NH₃ storage model can be adapted to account for catalyst aging by adjusting site densities

Conclusions

- Measuring NH₃ adsorption isotherms and calculating adsorption enthalpy as a function of NH₃ inventory provides unique insights that guide model strategy development
- A two site adsorption equilibrium model with constant adsorption enthalpies and H₂O competitive adsorption at one site accurately captures the NH₃ storage behavior of commercial Cu-SSZ-13 and Cu-SAPO-34 SCR catalyst formulations
- Hydrothermal aging impact on NH₃ storage over anticipated light duty vehicle life can be modeled by adjusting only site densities

Future Work

- Implement model structure and parameters in fully transient SCR model
- Extend approach to model catalysts to identify physical sites corresponding to sites 1, 2