



Experimental Study and Numerical Interpretation on the Temperature Field of DPF during Active Regeneration with Hydrocarbon Injection

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- **Experimental Study**
- Numerical Interpretation (CFD Modeling)
- **Summary**
- Acknowledgements



Diesel particulate filter (DPF) is indispensable for diesel engines to meet the increasingly stringent emission regulations.

Regeneration is needed for the DPF to burn off the accumulated soot in the DPF.





□ The active regeneration process of the DPF.





Both the peak temperature and the maximum temperature gradient of the DPF during active regeneration should be well controlled in order to enhance the reliability and durability of the filter.

Too high temperature (>1100°C for cordierite DPF)



Too high temperature gradient (>350°C/cm for cordierite DPF)



Experiment Setup

Engine and catalysts specifications

Engine type	Diesel, 4-strokes, 6- cylinders in line
Air intake system	Inter-cooled, turbocharged
Fuel metering system	High pressure common rail
Bore	110 mm
Stroke	132 mm
Displacement	7.5 L
Compression ratio	17.4
Rated power	248 kW @ 2300 rpm
Maximum torque	1350 N·m @ 1200- 1700 rpm



Catalysts	Specifications
DOC	Ф10.5"x6 "
	400 cpsi/4 mil
CDPF	Ф10.5"x11 "
	200 cpsi/12 mil

- 24 thermocouples were inserted into the DPF channels to measure the inner temperature of the filter.
- The temperature circumferential uniformity of three different sections at the DPF length direction was analyzed.



Case 1: no soot loading in DPF, no HC injection.

The temperature circumferential distribution of the three sections is very homogeneous.



Temperature: °C



Case 2: no soot loading in DPF, with HC injection.

The temperature at the left-bottom region is higher than that of the right-top region in all the three sections, which should be caused by the nonuniform distribution of the HC at the DOC inlet.
Temperature: °C





Case 3: DPF soot loading = 3 g/L, with HC injection.

■ The temperature circumferential distribution of the three sections is highly similar with case 2, which indicates that the HC spray is the primary contributor of the circumferential nonuniformity. _{Temperature: °C}



75 IN C 11 7 75 IN

A new thermocouple layout configuration was adopted to evaluate the axial and radial uniformity of the DPF temperature field during active regeneration.





The DPF temperature field was visualized using cubic interpolation based on the measured temperature data.

Regeneration conditions:

exhaust mass flow = 440 kg/h DPF soot loading = 4 g/L DPF inlet temperature = 600 °C



Temperature gradient (°C/cm)



- The DPF temperature field was visualized using cubic interpolation based on the measured temperature data.
- The peak temperature occurred at the center of the DPF rear end.
- The maximum temperature gradient occurred at the DPF outer edge.

Regeneration conditions:

exhaust mass flow = 440 kg/h DPF soot loading = 4 g/LDPF inlet temperature = 600 °C



Temperature ($^{\circ}C$)





The DPF inlet temperature during regeneration has a significant effect on the peak temperature and maximum temperature gradient, and it should be accurately controlled during active regeneration.



 $SV = 20,000 h^{-1}$, DPF soot loading = 4 g/L



The soot loading level for DPF regeneration triggering is an important parameter for DPF regeneration control calibration.

The more soot loading in the DPF, the higher peak temperature and maximum temperature gradient during regeneration.



SV = 20,000 h⁻¹, DPF inlet temperature = 600 °C

The peak temperature and the maximum temperature gradient are both decreased at high space velocity condition due to the enhancement of the heat transfer.



DPF soot loading = 4 g/L, DPF inlet temperature = 600 $^{\circ}$ C

Numerical Interpretation (CFD Modeling)



Modeling platform: AVL FIRE

Calculation domain and mesh generation



Soot Loading Process Simulation

The soot distribution in the DPF is very homogeneous, because:

- The flow distribution after DOC is very homogeneous.
- The soot accumulation in the DPF tends to be homogeneous, because the flow rate will be reduced due to the high flow restriction if somewhere has more soot, and then less soot will be trapped at this region.



Diesel Spray Simulation

HC injector parameters and spray model selection

Number of nozzle holes	1
Nozzle hole diameter	0.5 mm
Spray cone angle	25 °
Diesel injection rate	3.1 kg/h
Wall interaction model	Kuhnke model
Evaporation model	Dukowicz model
Breakup model	Wave model

Exhaust conditions

Exhaust mass flow	440 kg/h
Exhaust temperature	300 ℃
Environment temperature	25 ℃



Diesel Spray Simulation



The HC distribution at DOC inlet is nonuniform due to the short evaporation distance and mixing time of the diesel spray.

The HC distribution at DOC inlet will influence the temperature distribution at the DPF inlet, thus the temperature field of the DPF during active regeneration. 300C HC:TI 0.57:Species:Mole Fraction C3H6[-]



0.0080284

0.0075704

0.0071124

0.0066544

0.0061965

0.0057385

0.0052805

0.0048225

0.0043645

0.0039066

0.0034486

How to take the soot distribution and HC nonuniformity effects into consideration?

Diesel spray simulation

Soot loading simulation

HC distribution calculated from diesel spray simulation **DPF** regeneration simulation

soot distribution calculated from soot loading simulation

DPF regeneration reactions calibration

 NO2 regeneration was ignored due to the low NO2 concentration during active regeneration, which has been mostly converted into NO at high temperature because of chemical equilibrium.

$$C(\mathbf{s}) + \frac{1}{2}O_2 \xrightarrow{k_1} CO$$
$$C(\mathbf{s}) + O_2 \xrightarrow{k_2} CO_2$$

$$\begin{split} \dot{r}_1 &= f_{\rm CO} \cdot \mathbf{K}_1 \cdot T_{\rm s} \cdot \mathrm{e}^{\left(\frac{-\mathbf{E}_1}{\mathbf{R} \cdot T_{\rm s}}\right)} \cdot y_{\rm O_2} \\ \dot{r}_2 &= (1 - f_{\rm CO}) \cdot \mathbf{K}_1 \cdot T_{\rm s} \cdot \mathrm{e}^{\left(\frac{-\mathbf{E}_1}{\mathbf{R} \cdot T_{\rm s}}\right)} \cdot y_{\rm O_2} \\ f_{\rm CO} &= \frac{1}{1 + \mathbf{k}_{\rm f} \cdot y_{\rm O_2}^{\rm Q_{\rm f}} \cdot \mathrm{e}^{\left(\frac{\mathbf{E}_{\rm f}}{\mathbf{R} \cdot T_{\rm s}}\right)} \end{split}$$







DPF regeneration simulation results

Temperature



539.94

Peak temperature

Simulation: 804 °C

Experiment: 732 °C







Both the peak temperature and the maximum temperature gradient of the DPF during active regeneration can be significantly decreased with the optimization of the HC distribution at the DOC inlet.



Summary



- The DPF temperature field during active regeneration was well studied in order to enhance the reliability and durability of the filter.
- A 3D CFD simulation, which takes the soot distribution and HC nonuniformity effect into consideration, was conducted to interpret the DPF temperature field during regeneration.
- The HC distribution at the DOC inlet has a significant effect on the DPF temperature filed during regeneration, and it should be well optimized.
- The DPF temperature field during DTI (drop to idle) regeneration should be studied in the future work, which is much more critical for the DPF reliability and durability than the steady state regeneration.

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Back up

Soot Loading Process Simulation



The soot loading process



Diesel Spray Simulation

Diesel spray





· 1510 - 14158



Temperature



 Case_6:TI_5.0:Cat:GradSolidTemperature[K/m]

 5312.1

 4867.2

 4422.4

 3977.6

 3532.8

 3087.9

 2643.1

2198.3

