## An Analysis of DISI Particle Morphology

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## **DISI Vehicle Particle Emissions**

### DISI particle number concentration emissions greater than that for PFI and CI-DPF vehicles (Mathis et al., 2005)



Soot and volatile nanoparticles present in DISI exhaust (Mathis et al., 2004)



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### Background: Conventional Diesel & PCCI

 Primary particle diameter range: 20 – 25 nm



mode	mobility diameter (nm)	d <sub>pp</sub> (nm)
conven- tional	50	$24\pm3$
	100	$22\pm 4$
	150	$25\pm4$
PCCI	50	$23\pm 4$
	100	$20\pm2$
150 nm	150	$21\pm 3$

*Energy & Fuels* Barone et al. (2011)

1500 rpm, 2.6 bar



### **Comparison of Conventional Diesel Particle Studies**

• Neer and Koylu (2006)

Comparison of diesel soot properties from TEM measurements

Study	Diesel engine type	Method	d̄p (nm)
Present study	6-cylinder engine, various loads and speeds	TEM	20–35
Zhu et al. [13]	Light-duty engine, various loads and speeds	TEM	19–33
Park et al. [11] <sup>a</sup>	4-cylinder engine, single operating condition	TEM	32
Wentzel et al. [8] <sup>b</sup>	Unknown engine, single operating condition	TEM	23
Lee et al. [12]	Heavy-duty engine, four operating conditions	TEM	28–34



19 – 35 nm



# **Sampling and Analysis Methods**



- Early Fuel Injection 320 DBTDC
- Fuel Injection for Low PN 280 DBTDC



## **Particle Collection for TEM Analysis**



Fierz, Kaegi and Burtcher (2007) University of Applied Sciences Northwestern Switzerland

Uniform collection across substrate Optimized sampling time Sampling efficiency vs. particle size





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# Aggregate Image Analysis

• Xiong and Friedlander (2001)



Atmospheric, 2006, *J. Nanoparticle Research* Diesel & PCCI, 2011, *Energy and Fuels* 





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### DISI and Conventional Diesel Size Distributions





## Early Injection Particle Morphology

- E20, DI320 BTDC, 1500 rpm/8 bar, Engine-out
- 2-stage dilution with evaporator tube, DR=30





Large variation primary particle diameter – Greater range than for diesel aggregates

– Heterogeneous fuel/air mixing



## Early Injection Particle Morphology

- Liquid droplets abundant
  - Condensation of unburned fuel and lube
  - Possible fuel impingement from early injection





Scale bar 200 nm

E20, DI320 BTDC, 1500 rpm/8 bar, Engine-out 2-stage dilution with evaporator tube, DR=30

# **Fuel Injection for Minimum PN**

- Peak primary diameters smaller than early injection but still wide range
- Fewer unburned fuel/oil droplets
  - Less impingement on cylinder since later injection





# **Fuel Injection for Minimum PN**

 Presence of large and small primary particles indicates heterogeneous mixing



#### Both images have same magnification

12 Managed by UT-Battelle for the U.S. Department of Energy E20, DI280 BTDC, 1500 rpm/8 bar, Engine-out 2-stage dilution with evaporator tube, DR=30



# **Fuel Injection for Minimum PN**

 Single solid nanoparticles (~10 nm) smaller than E.U. particle number regulation limit (23 nm)



13 Managed by UT-Battelle for the U.S. Department of Energy E20, DI280 BTDC, 1500 rpm/8 bar, Engine-out 2-stage dilution with evaporator tube, DR=30



### Nanoparticles Can Penetrate to Alveolar Region





Adapted from Heyder (2004)

International Commission on Radiological Protection Model



# Toxicity of 15, 30 & 55 nm Silver Particles

• Rat alveolar macrophages exposed for 24 hr to agglomerates

Carlson et al. (2008)

**Mitochondrial Function** 

**Reactive Oxygen Species** 



Inner membrane damage,\* permeability transition (PT) pore opening,\* energy failure,\* apoptosis,\* apo-necrosis, cytotoxicity Phase II enzyme induction, inflammation, mitochondrial perturbation\*

National Laboratory

### **Relative Number of Surface Molecules Inversely Related to Particle Size**



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## Morphology Comparison for Injection Strategies

	Early – DI 320	Minimum PN – DI 280
Single Spheres	8%	21%
Aggregates	67%	78%
Droplets	25%	1%
Irregular	1%	-

- Injection for minimum PN generated fewer droplets and more single solid spheres than early injection
- Dependence of collection efficiency on particle size not reflected in this data



# **Idealized Aggregate Theory**

- Derived by equating migration velocity of an aggregate and sphere
- Relates primary particle diameter  $(d_{pp})$  and number of primary particles  $(N_p)$  to mobility diameter  $(d_m)$

- Lall and Friedlander (2006)

$$\frac{d_m}{C(d_m)} = \frac{c^* N_p d_{pp}^2}{12 \pi \lambda}$$

- $d_m$  = Mobility diameter
- $d_{pp}$  = Primary particle diameter
- $N_p$  = Number of primary particles
- $\dot{\lambda}$  = Gas mean free path
- $C(d_m) =$ Slip correction factor
  - c\* = Dimensionless drag force that depends on aggregate orientation
- Assumes most primary particles exposed to collisions with surrounding gas molecules ( $D_f < -2$ )



## **Projected Area Equivalent Diameter**

Direct-injection spark-ignition



Projected area



Rogak, Flagan & Nguyen (1993)



4-cylinder, 1.9 L engine E20 fuel 280 DBTDC injection

Other supporting studies Park et al. (2004) Ku & Maynard (2005) Chakrabarty et al. (2007)



### **Charging Efficiency for Aggregates and Spheres**

- Unipolar diffusion charger (Shin et al., 2010)
  - Difference between aggregate and sphere charging efficiency increases with increasing electrical mobility diameter.





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# **Particle Collection Efficiency**

- Aerosol concentration calculation
  - Analyzed 112 particles at 81K magnification
  - Estimated aggregate mobility diameter using IA theory and projected area
  - Extrapolated to area of TEM grid (3.05 mm diameter)
  - Calculated collection efficiency from power law calibration curve





## SMPS & TEM Size Distributions: 10 - 50nm



# Conclusions

- Wide primary particle diameter range
  - 7 to 60 nm
  - Indicative of heterogeneous fuel and air mixing
  - Other speed and load points should be examined
- Small primary size relative to diesel for minimum PN injection point
  - 10 to 15 nm
  - Fuel and air mixing enhanced in some zones
- Presence of single solid particles smaller than 23 nm
  - TEM number concentration data consistent with SMPS for this size range
  - May be of health concern since can deposit in alveolar region and have greater percent surface area

