

Modeling Studies of the Dual-Layer LNT/SCR Monolithic Catalyst

Mike Harold

Acknowledgements:

**Bijesh Shakya, Yi Liu, Yang Zheng,
Vemuri Balakotaiah, Dan Luss**



Funding:





Motivation



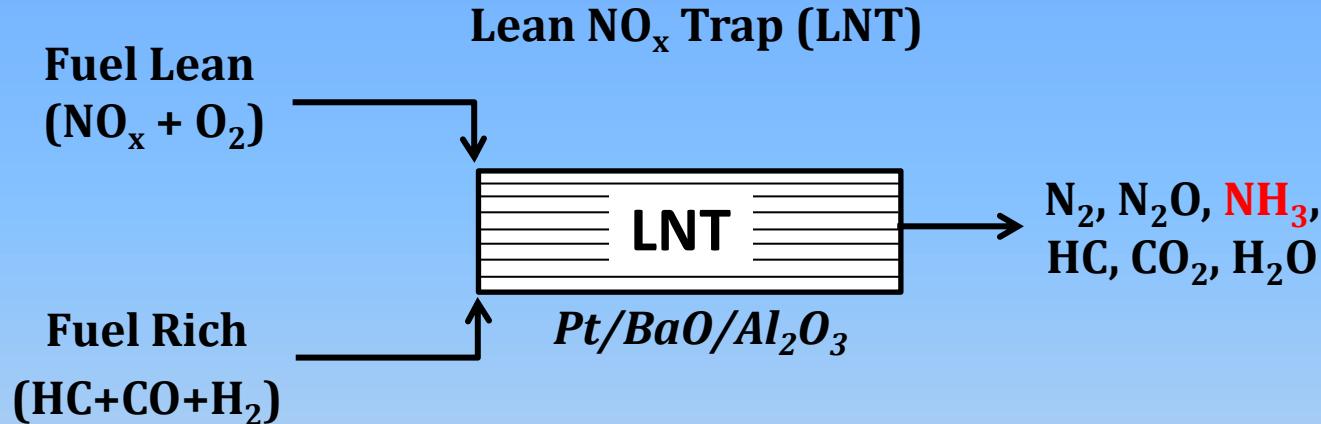
<http://solar.calfinder.com/blog/wp-content/uploads/2009/12/toxic-city-houston.jpg>

http://images.google.com/imgres?imgurl=http://www.utexas.edu/research/ceer/texaqs/images/downtown_view2

Background

Technologies for Lean NO_x Reduction

NO_x Storage and Reduction (NSR)



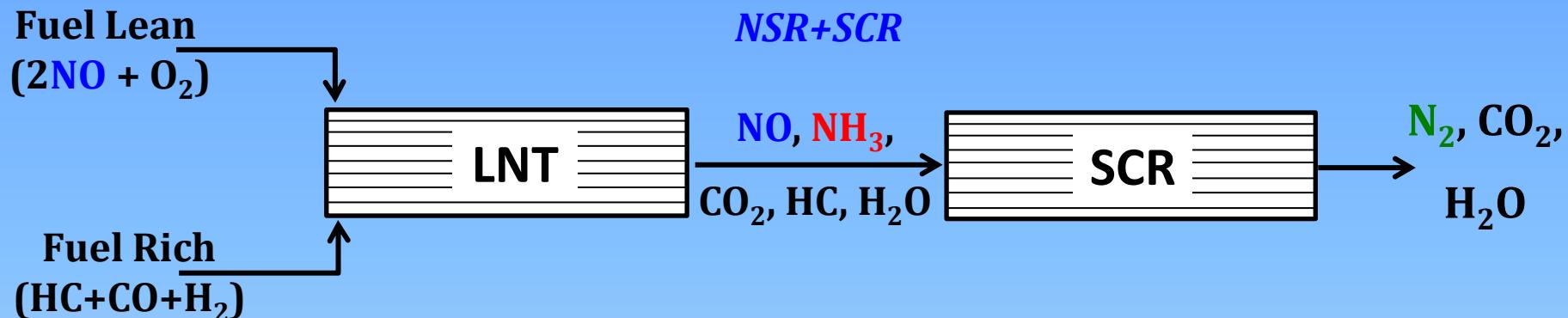
Selective Catalytic Reduction (SCR)



Fe- or Cu- Zeolite

Background

Technologies for Lean NO_x Reduction

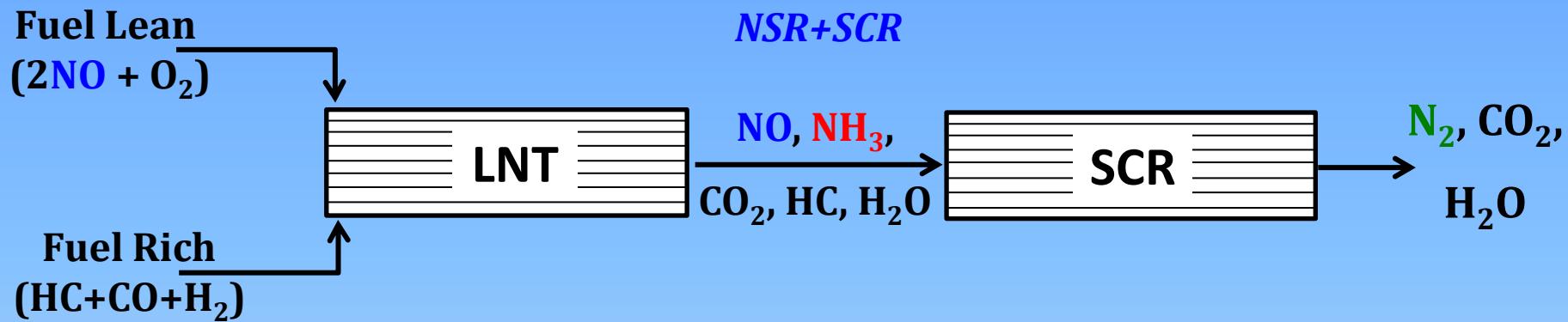


$$X_{\text{NOx}}=0.5 \quad S_{\text{NH3}}=1$$

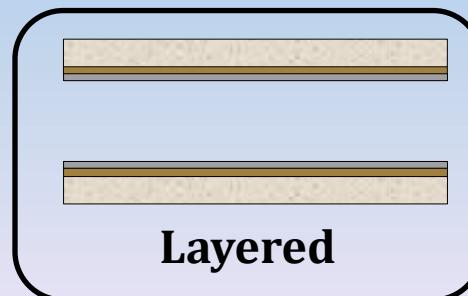
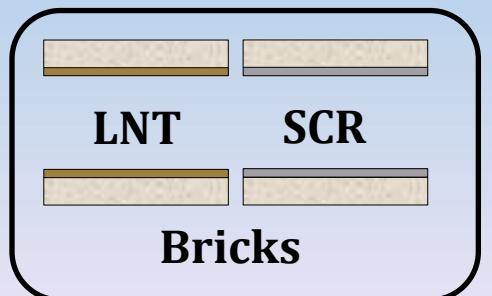
LNT does not need a highly effective NSR catalyst in the combined NSR/SCR application

Background

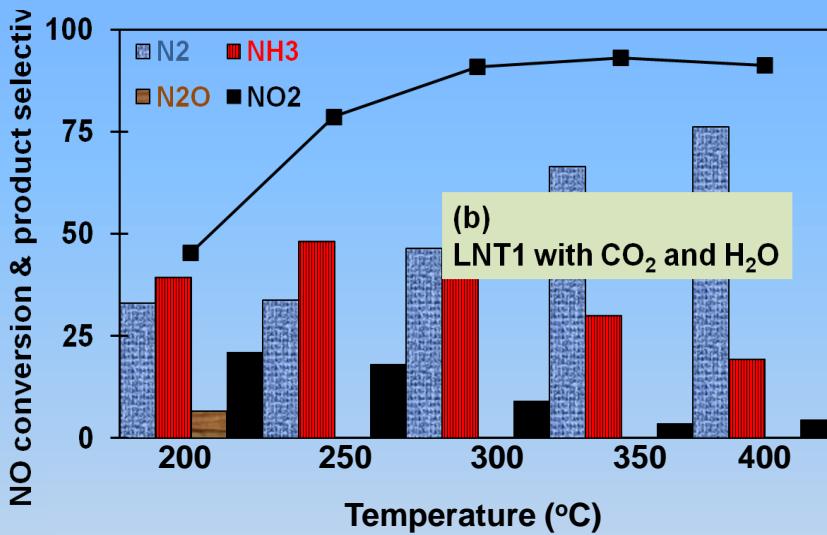
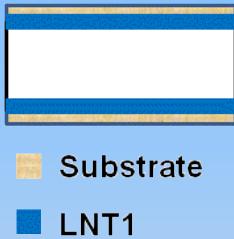
Technologies for Lean NO_x Reduction



Compare:



LNT/SCR: H₂ Reductant With CO₂ & H₂O



LNT/SCR: H₂ Reductant With CO₂ & H₂O



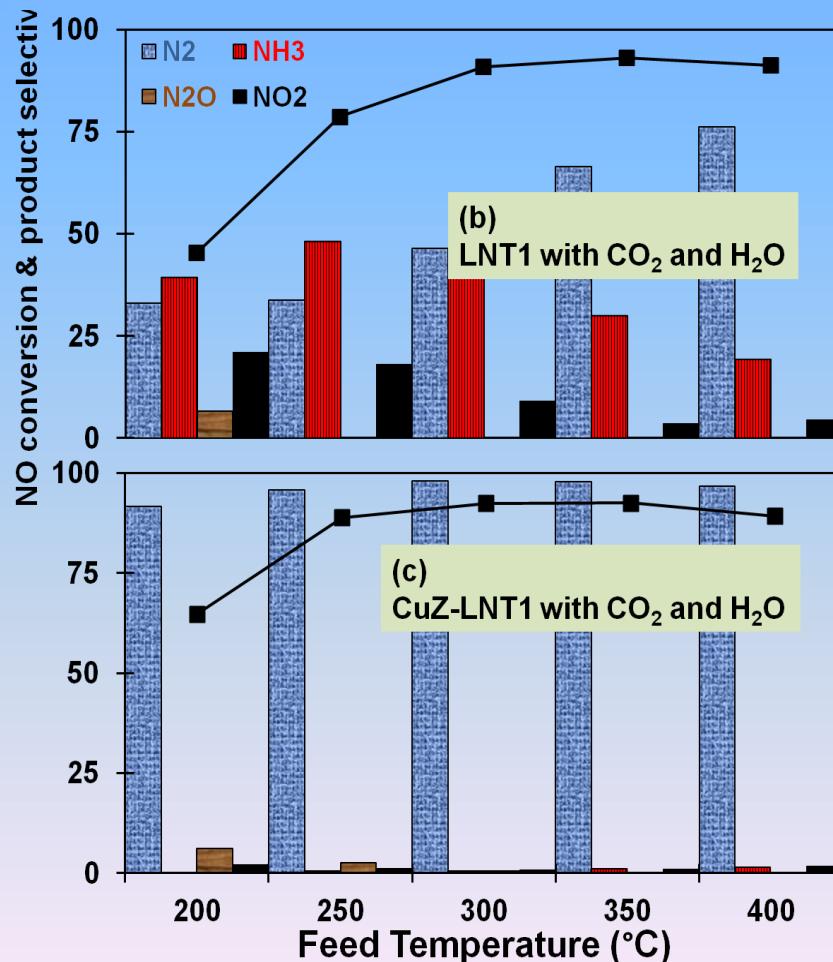
Substrate
LNT1



Substrate
LNT1
Cu/ZSM-5

Conditions:

Lean: 500 ppm NO, 5% O₂; 60s
Rich: 2.5% H₂; 5s
(Both: 2.5% H₂O, 2% CO₂)





Objective of Current Study

Conduct simulation studies of dual-layer LNT/SCR monolithic catalyst using global kinetics to

- (i) elucidate the reactor behavior**

- (ii) identify optimal catalyst design & reactor operating strategies**

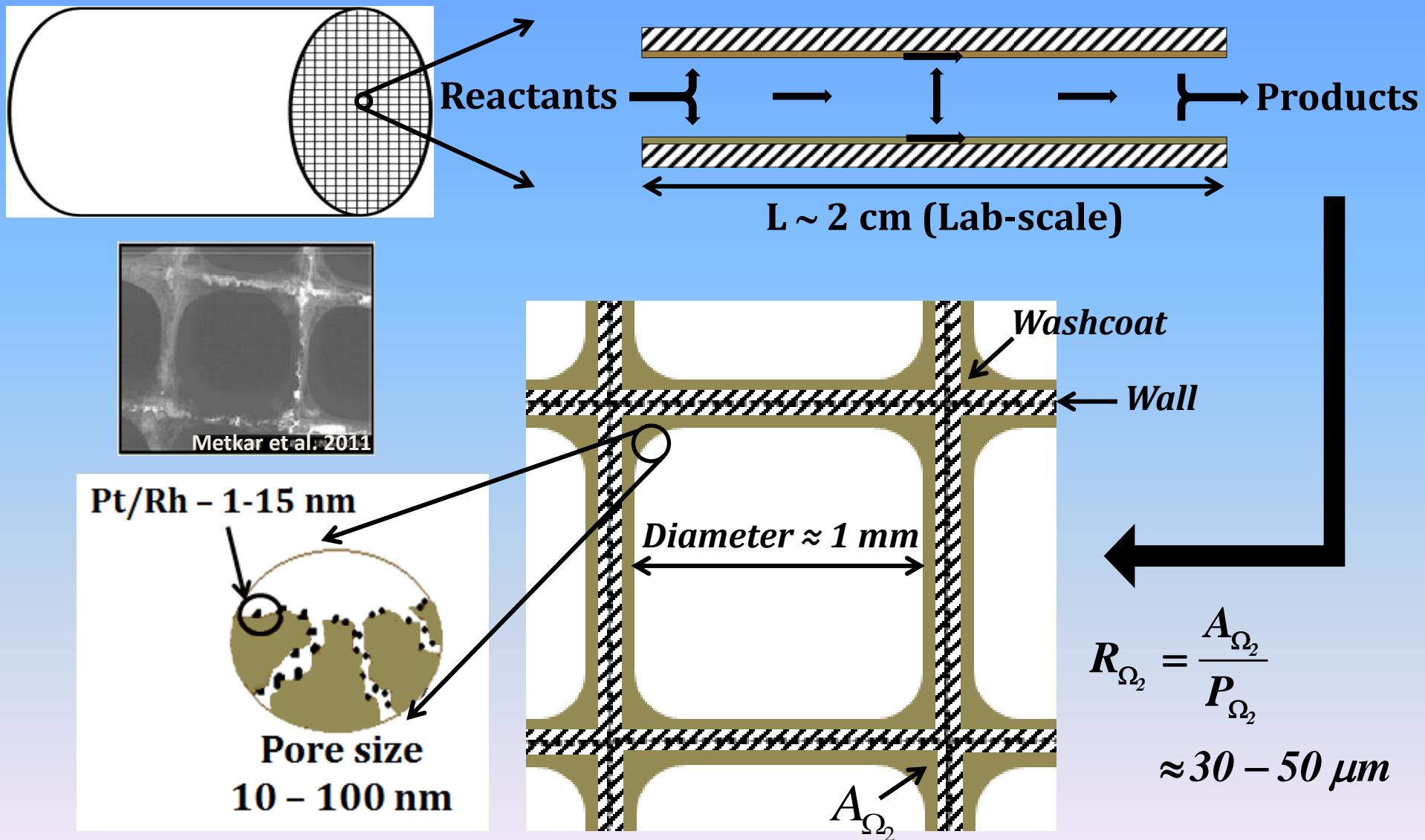
- Develop & validate global kinetic model for low dispersion LNT catalysts
- Adopt kinetic model for SCR from the literature ‡
- Use LNT/SCR dual layer reactor model to study:
 - ❖ Effect of washcoat loading
 - ❖ Effect of temperature
 - ❖ Compare dual layer design to dual brick design



Outline

- ❖ Model development (Multiple length-time scales, model equations)
- ❖ Model tuning and validation for LNT (LNT reactions, compare with experiments)
- ❖ Review SCR model[‡] (SCR reactions, validations)
- ❖ Simulation results of dual layer LNT/SCR (concentration profiles, effect of washcoat/catalyst loading, effect of temperature, compare with brick config)
- ❖ Conclusions

Multiple Length/Time Scales

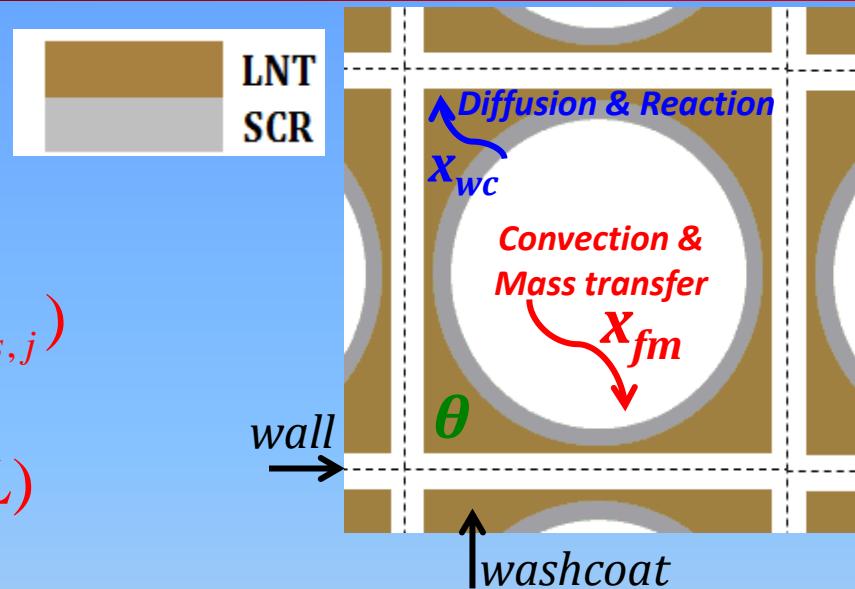


Model Development

Model equations

Fluid phase equation

$$\frac{\partial x_{fm,j}}{\partial t} = -u \frac{\partial x_{fm,j}}{\partial z} - \frac{k_{me,j}(z)}{R_{\Omega_1}} (x_{fm,j} - x_{s,j}) \quad (0 < z < L)$$



Washcoat equation

$$\varepsilon_{wc} \frac{\partial x_{wc,j}}{\partial t} = \frac{\partial}{\partial y} \left(D_{e,j} \frac{\partial x_{wc,j}}{\partial y} \right) + \frac{1}{C_{tm}} \sum_{r=1}^{rxn} g_{jr} R_r (\underline{x}_{wc}, \underline{\theta}, T)$$

Site balance

$$\frac{\partial \theta_k}{\partial t} = \frac{1}{C^o} \sum_{r=1}^{rxn} g_{kr} R_r (\underline{x}_{wc}, \underline{\theta}, T)$$

Outline

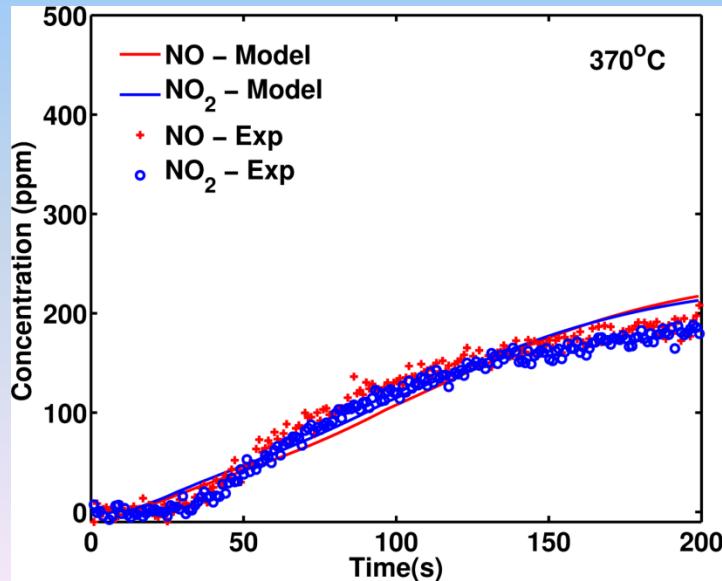
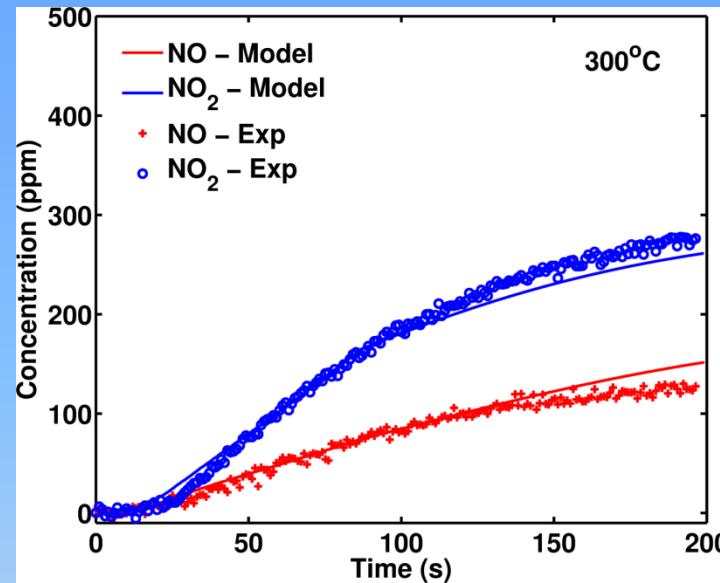
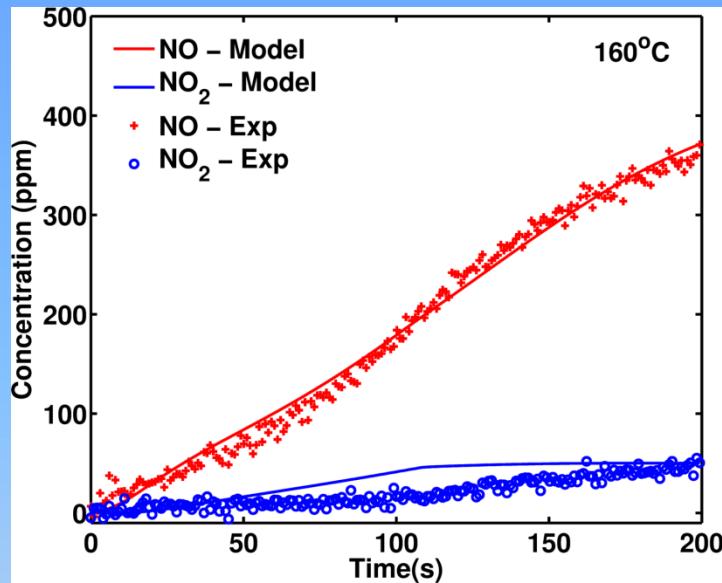
- ❖ Model development (Multiple length-time scales, model equations) ✓
- ❖ Model tuning and validation for LNT
- ❖ Review SCR model[‡] (SCR reactions)
- ❖ Simulation results of dual layer LNT/SCR (concentration profiles, effect of washcoat/catalyst loading, effect of temperature)
- ❖ Summary and conclusions

LNT – Reactions and Catalyst

<i>NO oxidation</i>	1.	$\text{NO} + 0.5 \text{O}_2 \rightarrow \text{NO}_2$
<i>NO storage in the presence of O₂</i>	2.	$2 \text{NO} + 1.5 \text{O}_2 + \text{BaO}_{(\text{f})} \rightarrow \text{Ba}(\text{NO}_3)_2 \text{ (f)}$
	3.	$2 \text{NO} + 1.5 \text{O}_2 + \text{BaO}_{(\text{s})} \rightarrow \text{Ba}(\text{NO}_3)_2 \text{ (s)}$
<i>NO₂ Storage</i>	4.	$2 \text{NO}_2 + 0.5 \text{O}_2 + \text{BaO}_{(\text{f})} \rightarrow \text{Ba}(\text{NO}_3)_2 \text{ (f)}$
	5.	$3 \text{NO}_2 + \text{BaO}_{(\text{s})} \rightarrow \text{Ba}(\text{NO}_3)_2 \text{ (s)} + \text{NO}$
<i>Nitrate reduction by H₂</i>	6.	$\text{Ba}(\text{NO}_3)_{2(\text{f})} + 3 \text{H}_2 \rightarrow \text{BaO}_{(\text{f})} + 2 \text{NO} + 3 \text{H}_2\text{O}$
	7.	$\text{Ba}(\text{NO}_3)_{2(\text{s})} + 3 \text{H}_2 \rightarrow \text{BaO}_{(\text{s})} + 2 \text{NO} + 3 \text{H}_2\text{O}$
<i>Nitrate reduction by NH₃</i>	8.	$\text{Ba}(\text{NO}_3)_{2(\text{f})} + 10/3 \text{NH}_3 \rightarrow \text{BaO}_{(\text{f})} + 8/3 \text{N}_2 + 5 \text{H}_2\text{O}$
	9.	$\text{Ba}(\text{NO}_3)_{2(\text{s})} + 10/3 \text{NH}_3 \rightarrow \text{BaO}_{(\text{s})} + 8/3 \text{N}_2 + 5 \text{H}_2\text{O}$
<i>Pt catalyzed NO reduction</i>	10.	$2 \text{NO} + \text{H}_2 \rightarrow \text{N}_2\text{O} + \text{H}_2\text{O}$
	11.	$\text{NO} + 5/2 \text{H}_2 \rightarrow \text{NH}_3 + \text{H}_2\text{O}$
	12.	$3/2 \text{NO} + \text{NH}_3 \rightarrow 5/4 \text{N}_2 + 3/2 \text{H}_2\text{O}$
<i>NH₃ adsorption and consumption</i>	13.	$\text{NH}_3 + \text{X} \rightarrow \text{NH}_3\text{-X}$
	14.	$\text{NH}_3\text{-X} + 3/4 \text{O}_2 \rightarrow 1/2 \text{N}_2 + 3/2 \text{H}_2\text{O} + \text{X}$

Sample	Pt (%)	Pt dispersion%	BaO (%)
Pt/BaO/Al ₂ O ₃	2.48	8	13.0

LNT – Model vs Exp [‡] - Storage



Conditions:

Lean inlet: 500 ppm NO + 5% O₂

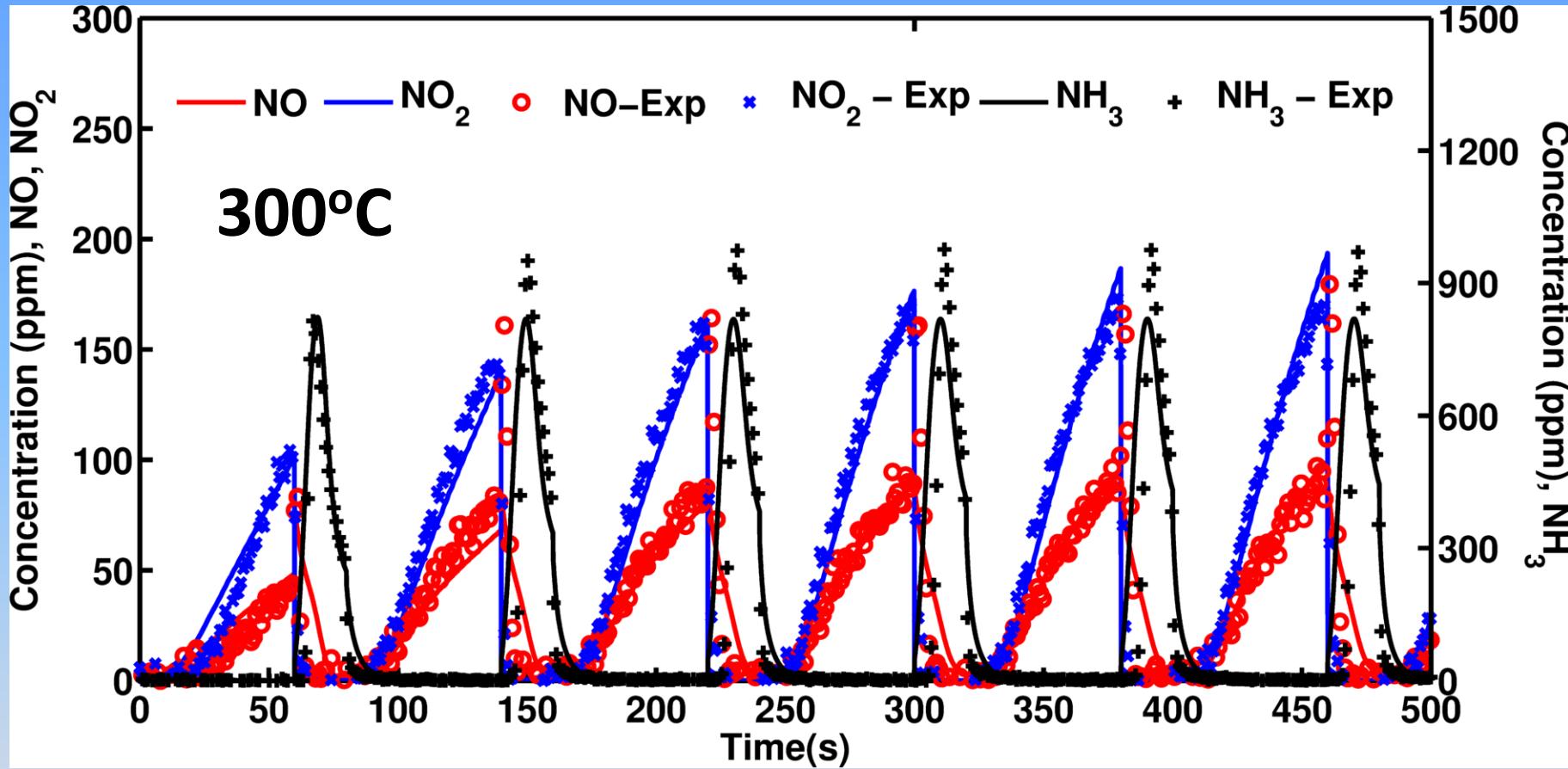
GHSV: 60,000 hr⁻¹ (based on monolith volume) (20 ms @ 300°C)

Catalyst:

2 cm long; 28 channels

400 cpsi; 30 µm washcoat

LNT – Model vs Exp \ddagger – Cycling



Conditions:

Lean inlet: 500 ppm NO + 5% O₂ in bal Ar / Duration: 60s

Rich inlet: 5000 ppm H₂ in bal Ar / Duration: 20s

Temperature: 300°C

GHSV: 60,000 hr⁻¹ (based on monolith volume)

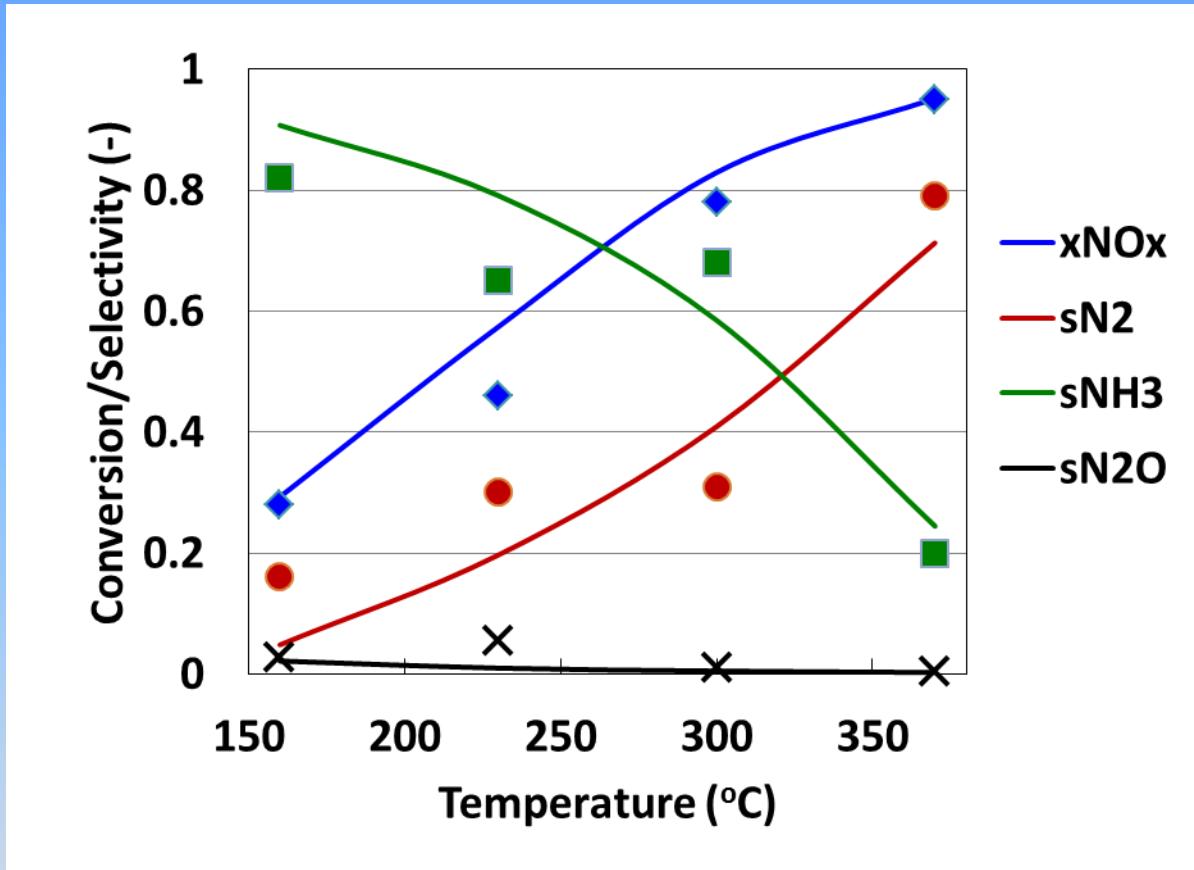
Catalyst:

2 cm long

28 channels

400 cpsl

30 μm washcoat

**Conditions:**

NOx stored: 1.5×10^{-5} moles

Rich inlet: 1500 ppm H₂ – 200s

GHSV: 60,000 hr⁻¹ (based on monolith volume)

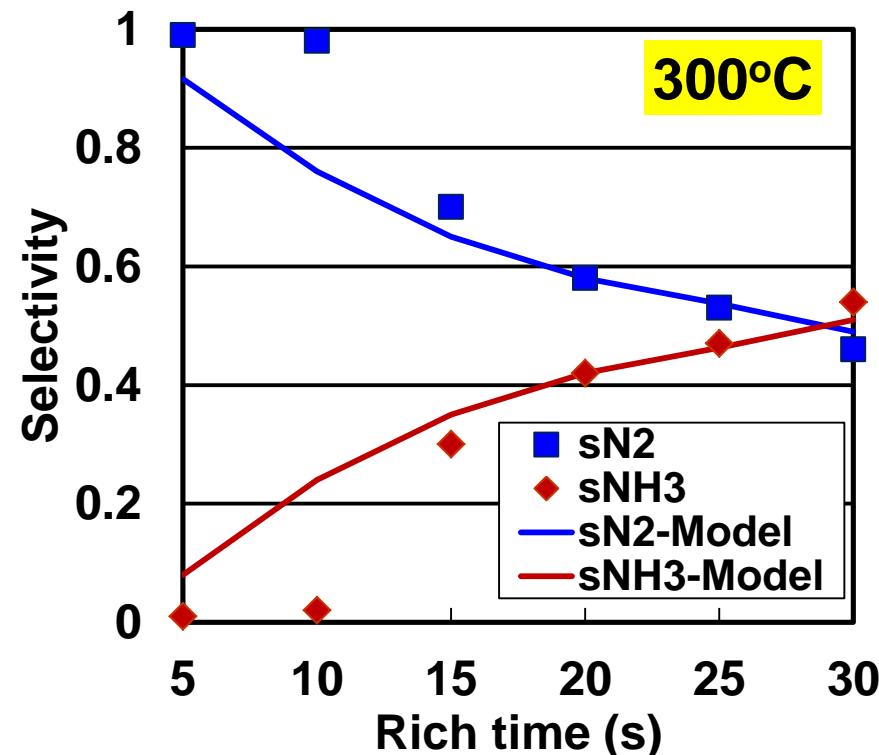
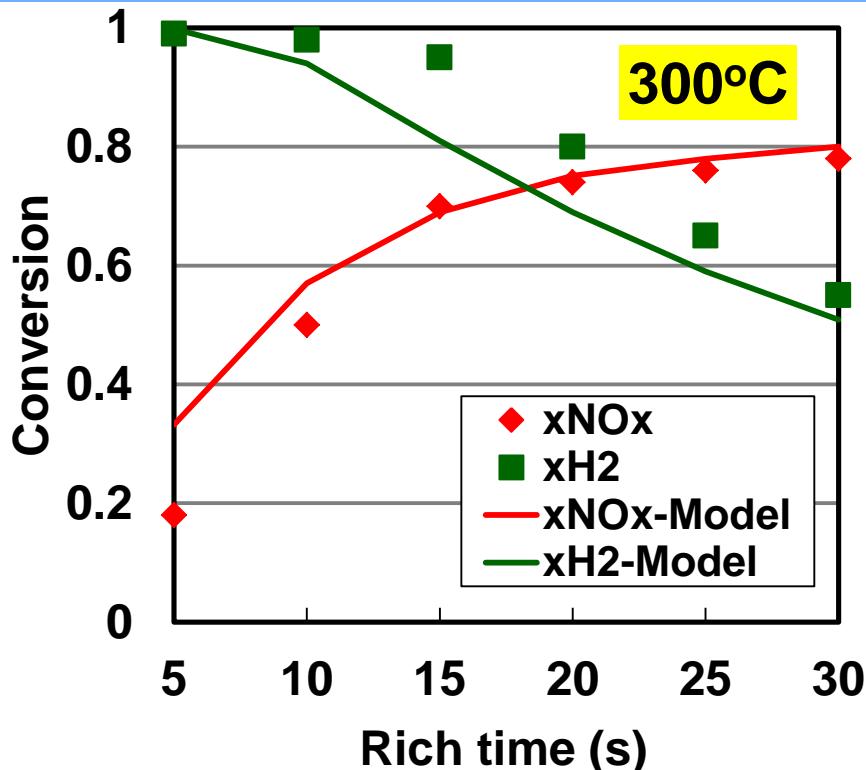
Catalyst:

2 cm long; 28 channels

400 cpsi; 30 μm washcoat

LNT – Model vs Exp [‡]

Effect of Rich phase duration



Conditions: Lean inlet: 500 ppm NO + 5% O₂ in bal Ar / Duration: 60s

Rich inlet: 5000 ppm H₂ in bal Ar / Duration: 5-30s

Model accurately predicts the effect of rich phase duration on conversion and selectivity



Outline

- ❖ Model development (Multiple length-time scales, model equations) ✓
- ❖ Model tuning and validation for LNT (review of experimental results, LNT reactions) ✓
- ❖ Review SCR model[‡] (SCR reactions)
- ❖ Simulation results of dual layer LNT/SCR (concentration profiles, effect of washcoat/catalyst loading)
- ❖ Summary and conclusions

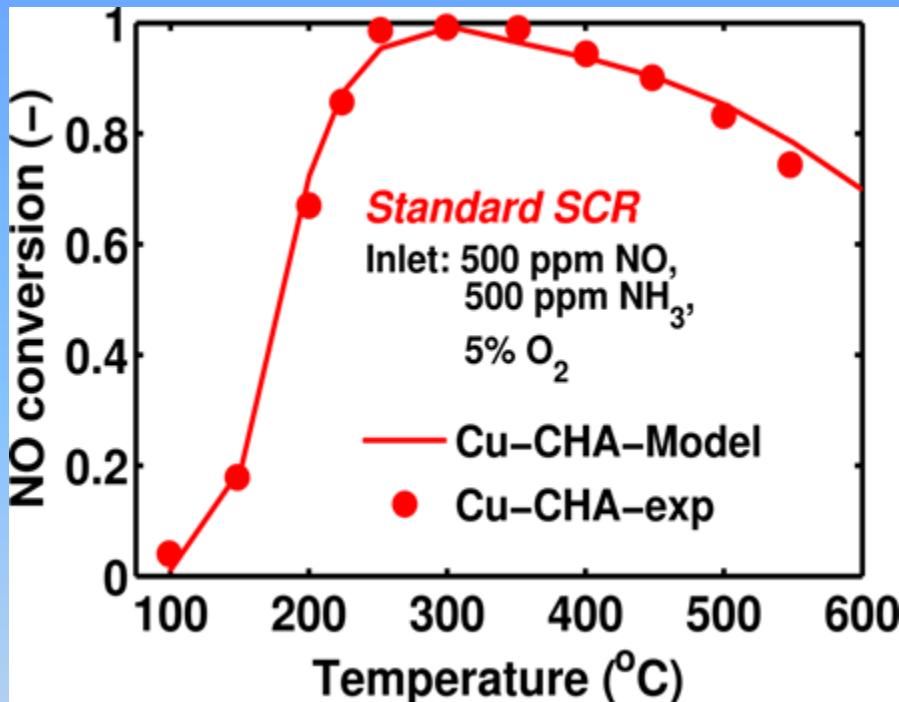
[‡] Metkar et. al. 2012 / Chem. Eng. Sci. / doi: <http://dx.doi.org/10.1016/j.ces.2012.09.008>

SCR[‡] – Reactions and Catalyst

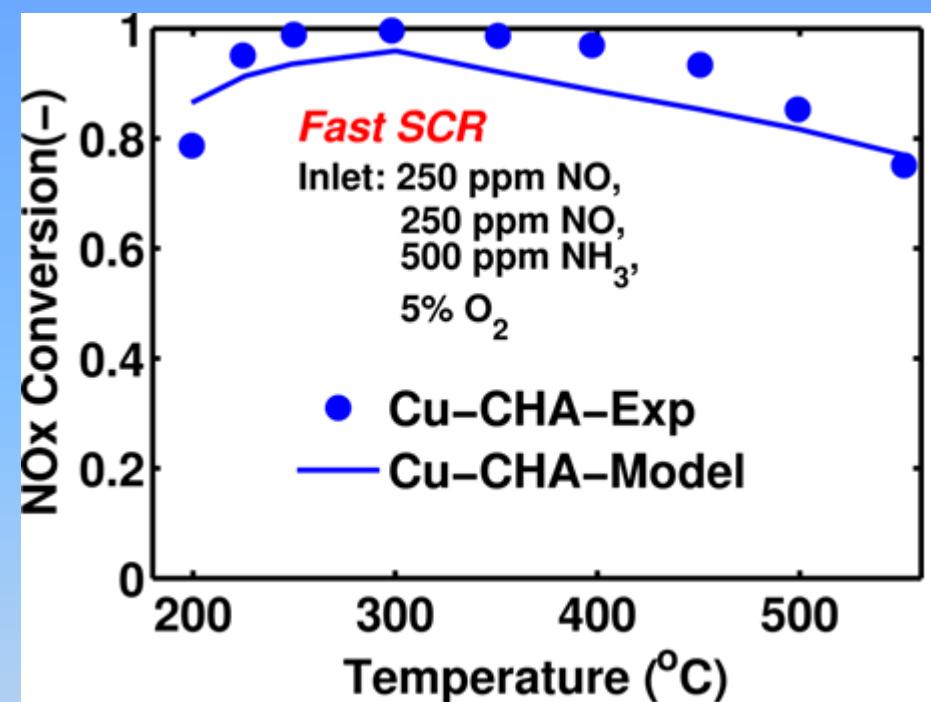
<i>NH₃ adsorption / desorption</i>	1.	NH ₃ + S → NH ₃ -S	
<i>NH₃ oxidation</i>	2.	2NH ₃ -S + 1.5O ₂ → N ₂ + 3H ₂ O + 2S	
<i>NO oxidation</i>	3.	NO + ½ O ₂ → NO ₂	
<i>Standard SCR</i>	4.	4NH ₃ -S + 4NO + O ₂ → 4N ₂ + 6H ₂ O + 4S	
<i>Fast SCR</i>	5.	2NH ₃ -S + NO + NO ₂ → 2N ₂ + 3H ₂ O + 2S	
<i>NO₂-SCR</i>	6.	4NH ₃ -S + 3NO ₂ → 3.5N ₂ + 6H ₂ O + 4S	
<i>Ammonium nitrate formation</i>	7.	2NH ₃ -S + 2NO ₂ → N ₂ + NH ₄ NO ₃ + H ₂ O + 2S	
<i>Ammonium nitrate decomposition</i>	8.	NH ₄ NO ₃ → N ₂ O + 2H ₂ O	

Sample	Cu (%)
Cu-Chabazite	2.48

SCR Results[‡]



“Standard” SCR



“Fast” SCR



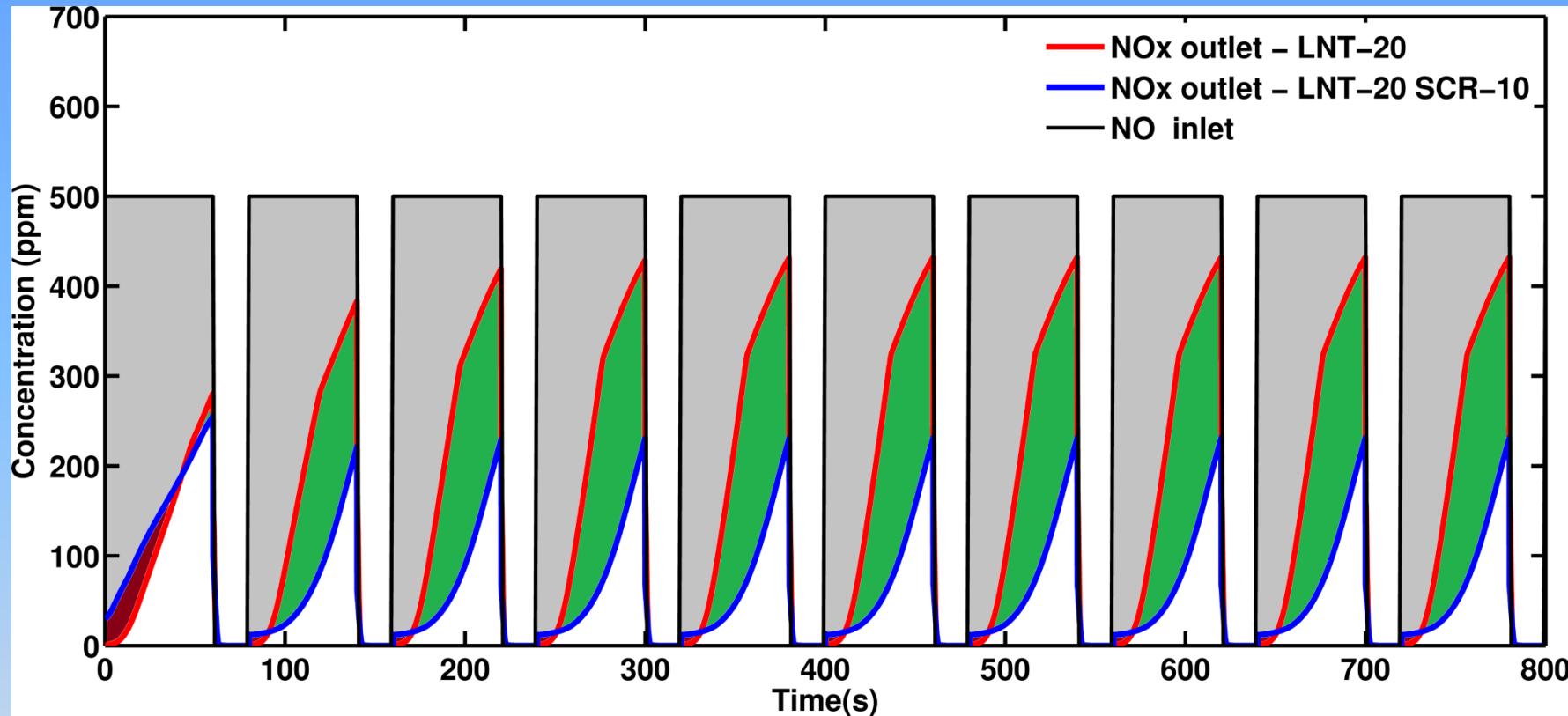
Cu-Chabazite gives high NO_x conversion activity over wide range of operating temperature and feed composition



Outline

- ❖ Model development (Multiple length-time scales, model equations) ✓
- ❖ Model tuning and validation for LNT (review of experimental results, LNT reactions) ✓
- ❖ Review SCR model[‡] (SCR reactions) ✓
- ❖ Simulation results of dual layer LNT/SCR (concentration profiles, effect of washcoat/catalyst loading)
- ❖ Summary and conclusions

LNT/SCR – Effluent NO_x Profile



Washcoat thickness: LNT = 20 μm / SCR = 10 μm

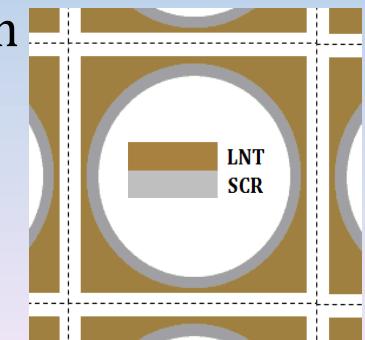
Conditions:

Lean inlet: 500 ppm NO + 5% O₂ in bal Ar / Duration: 60s

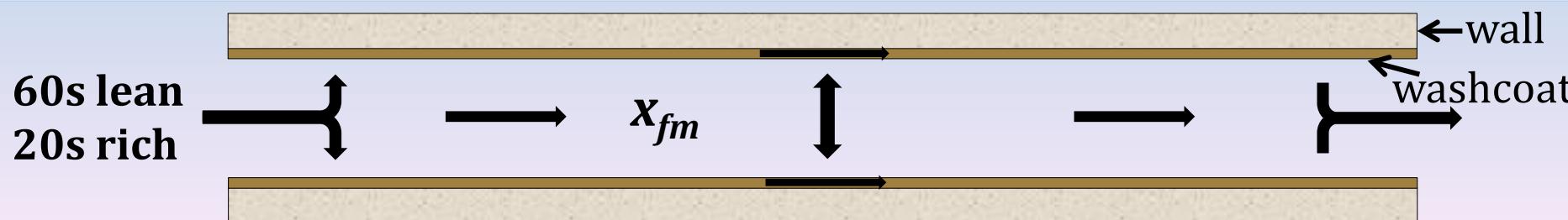
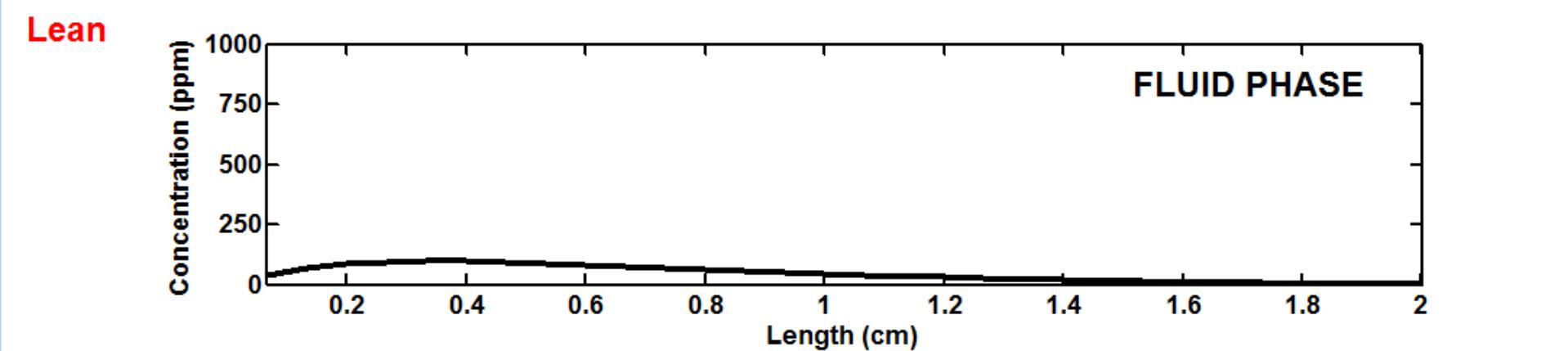
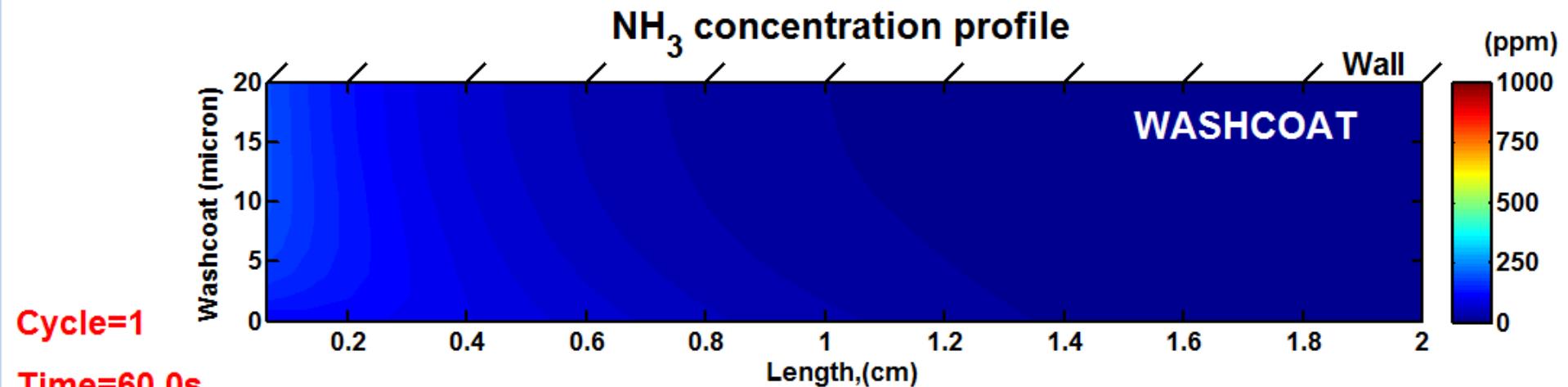
Rich inlet: 5000 ppm H₂ in bal Ar / Duration: 20s

Temperature: 300°C

GHSV: 60,000 hr⁻¹ (based on monolith volume); $\tau_c \approx 20\text{ms}$

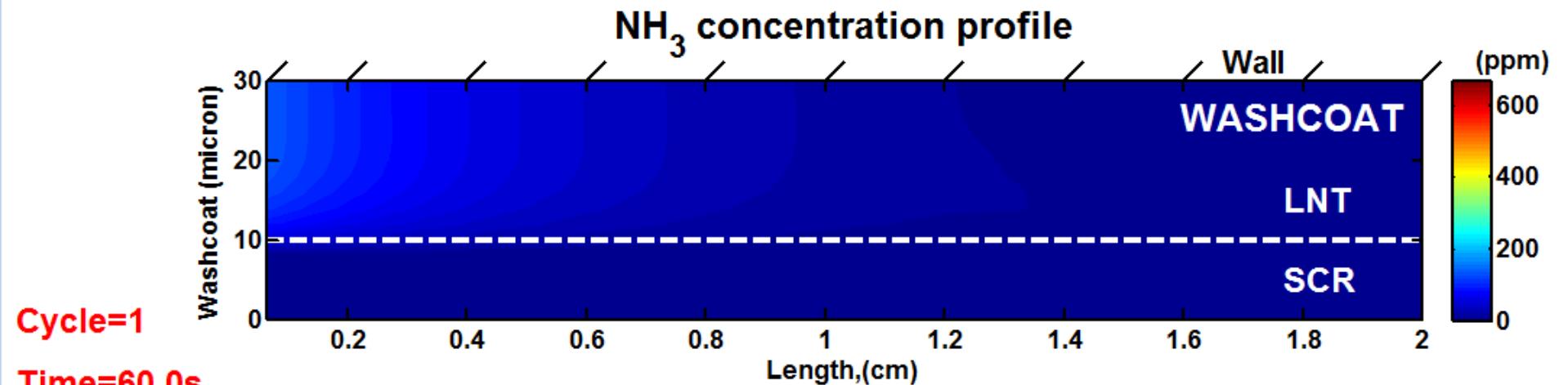


NH₃ Profile in LNT @ 300°C

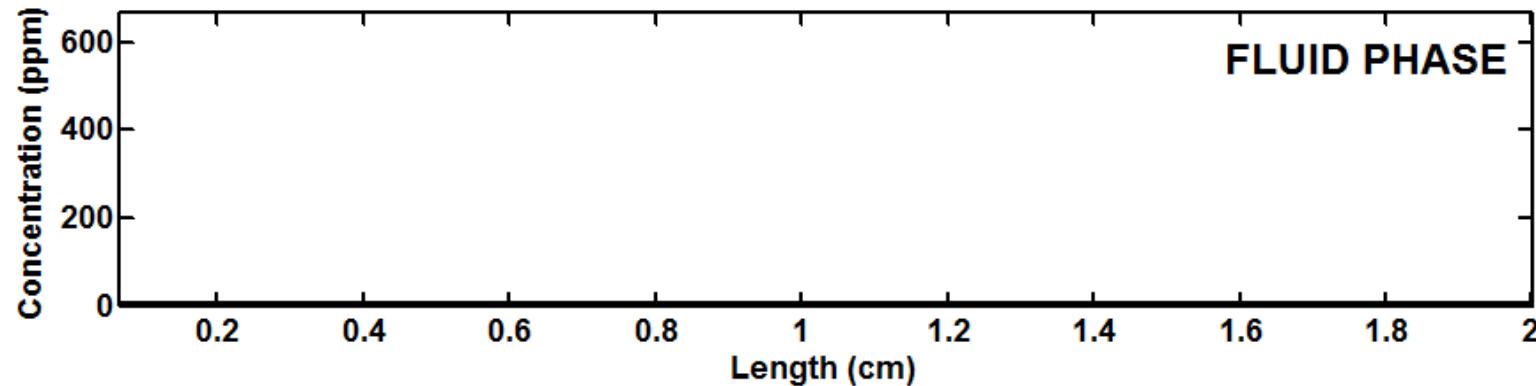




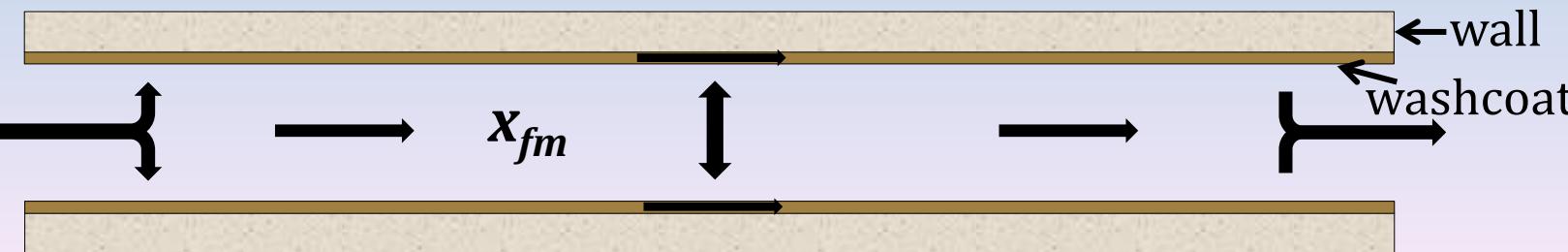
NH₃ Profile in LNT/SCR @ 300°C



Lean



60s lean
20s rich



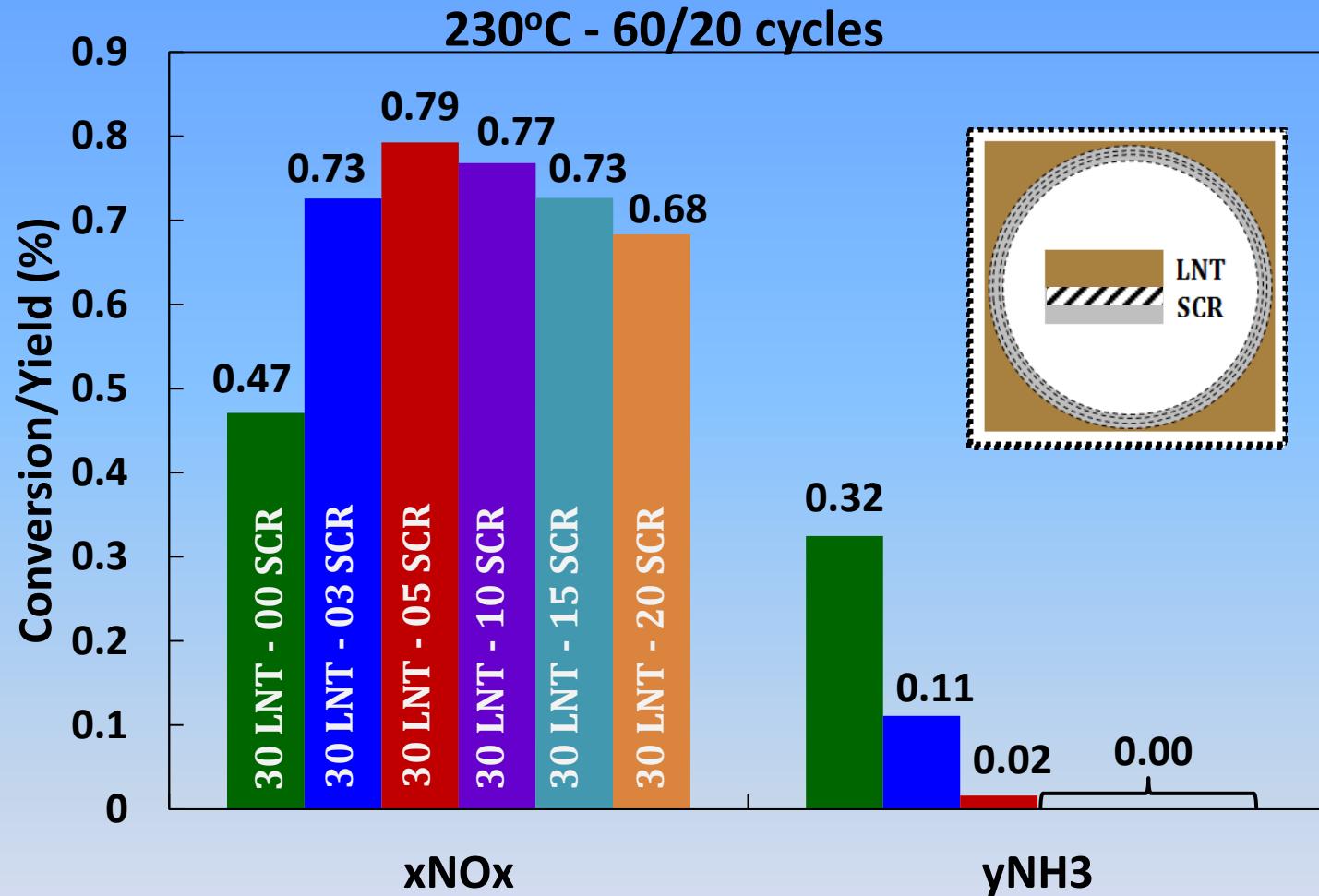
Effect of SCR Washcoat Loading

Conditions:

Lean: 60s
500 ppm NO
5% O₂
Rich: 20s
5000 ppm H₂
230°C

Washcoat Thickness:

LNT = 30 μm
SCR = 0-20μm



Excessive SCR loading leads to lower NOx conversion because of undesired diffusional limitation

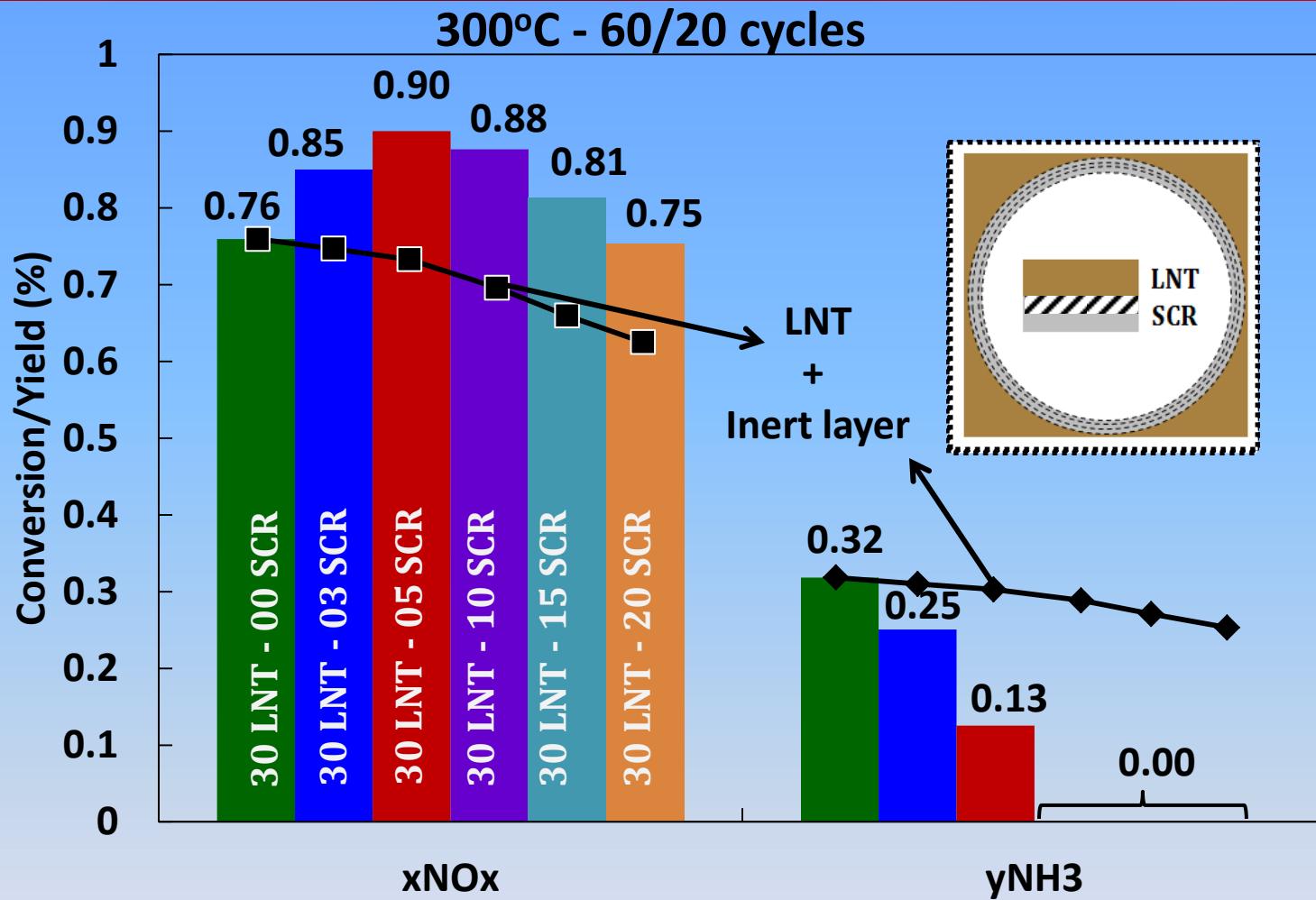
Effect of SCR Washcoat Loading

Conditions:

Lean: 60s
 500 ppm NO
 5% O₂
 Rich: 20s
 5000 ppm H₂
 300°C

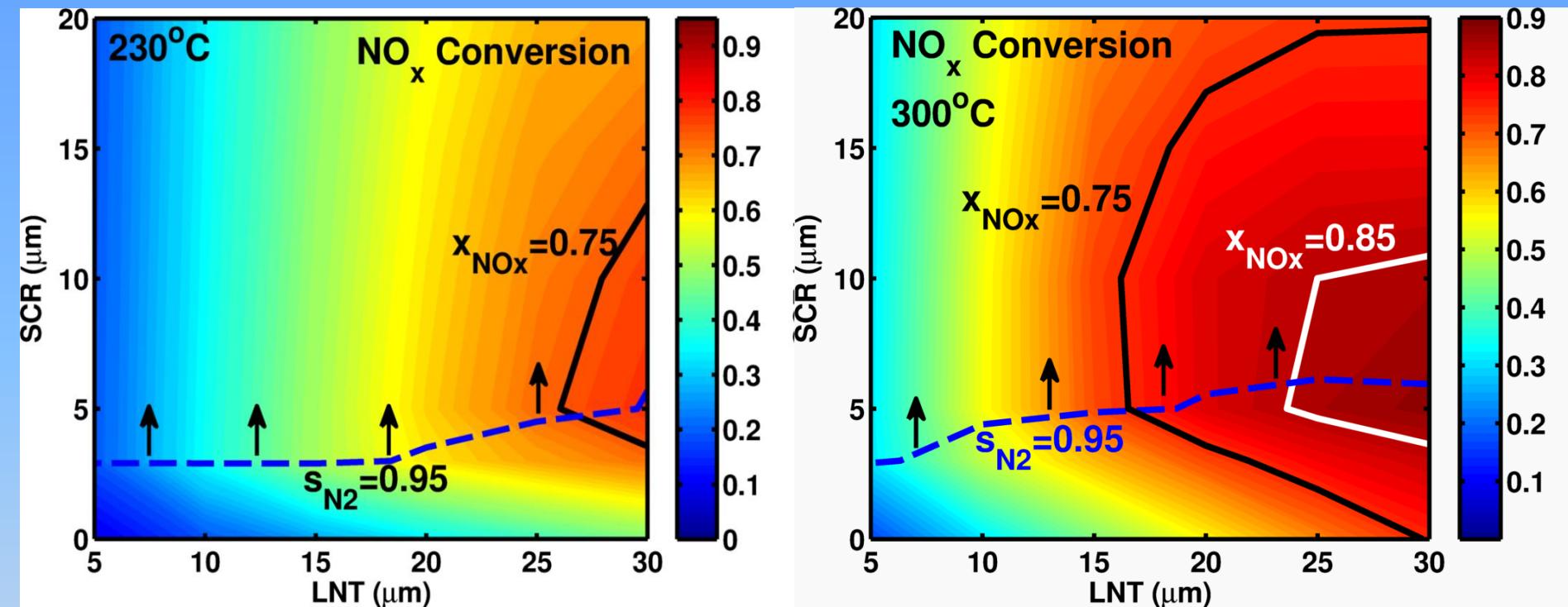
Washcoat Thickness:

LNT = 30 μm
 SCR = 0-15 μm



Inert layer shows effect of diffusion w/o reaction

Effect of LNT/SCR Washcoat Loading



Conditions:

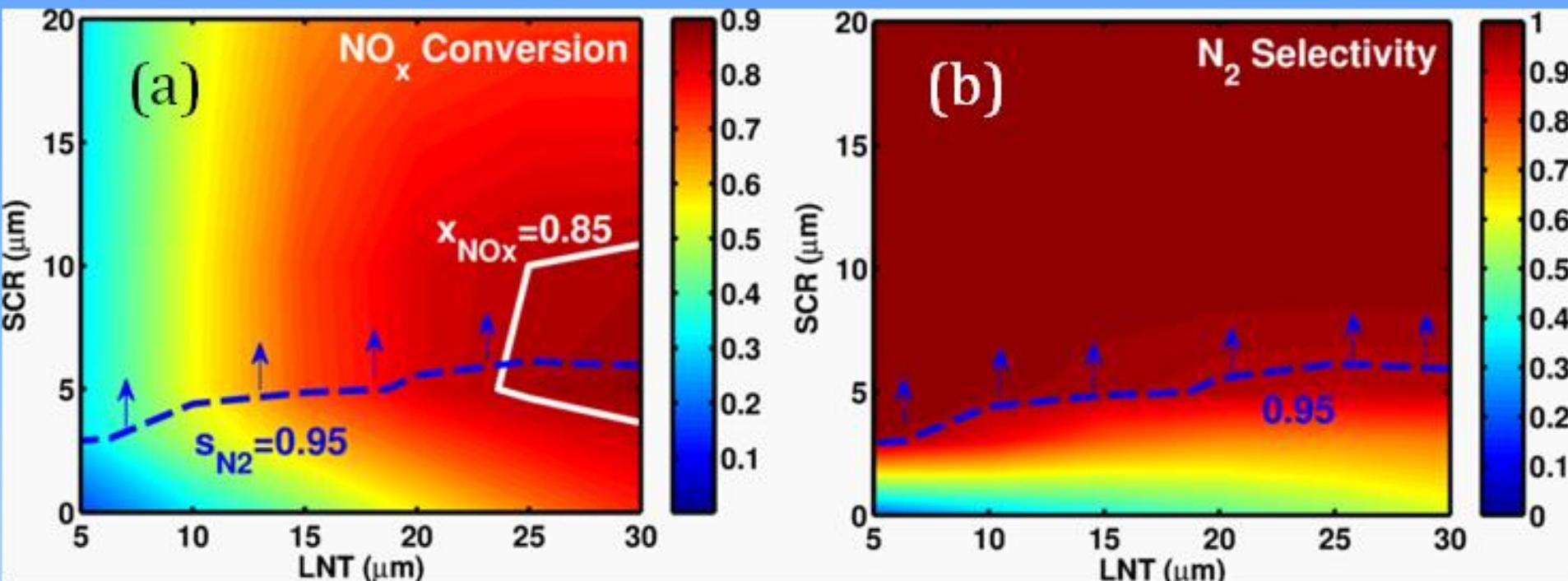
Lean inlet: 500 ppm NO + 5% O₂ in bal Ar / Duration: 60s

Rich inlet: 5000 ppm H₂ in bal Ar / Duration: 20s

Temperature: 230°C **GHSV:** 60,000 hr⁻¹ (based on monolith volume)

Several combinations of LNT/SCR are possible to attain the same conversion

Effect of LNT/SCR Washcoat Loading



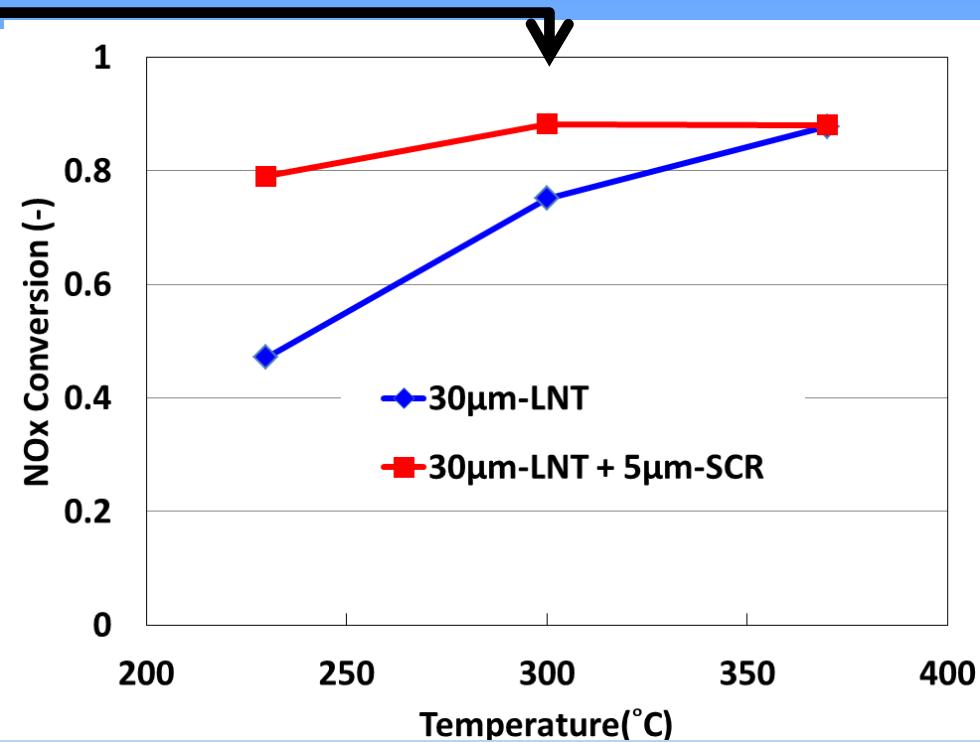
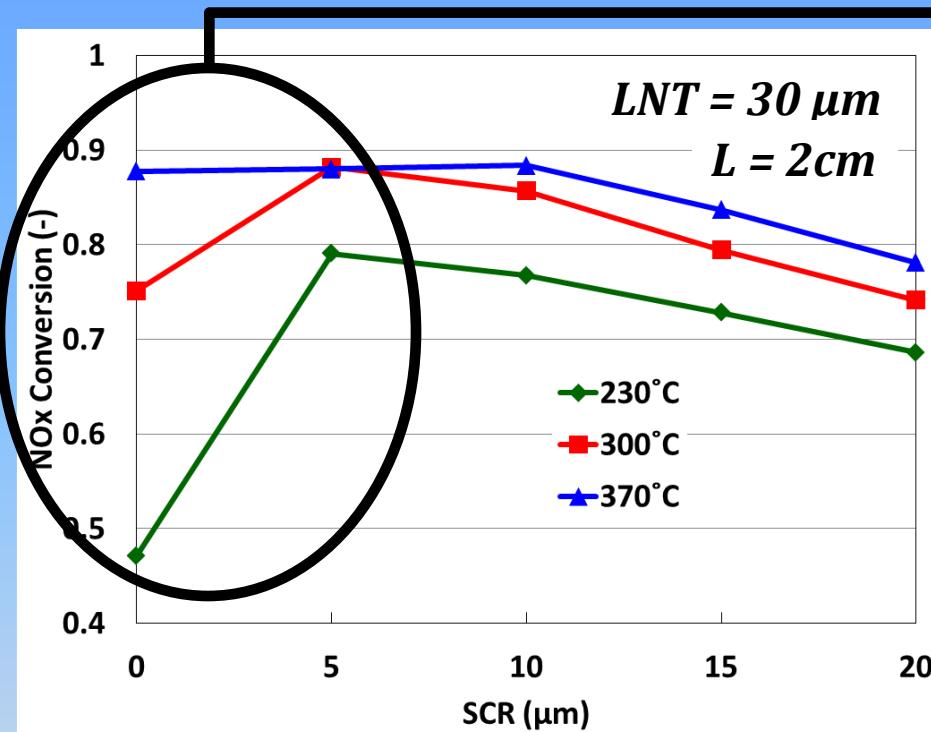
Conditions:

Lean inlet: 500 ppm NO + 5% O₂ in bal Ar / Duration: 60s

Rich inlet: 5000 ppm H₂ in bal Ar / Duration: 20s

Temperature: 300°C **GHSV:** 60,000 hr⁻¹ (based on monolith volume)

Effect of Temperature

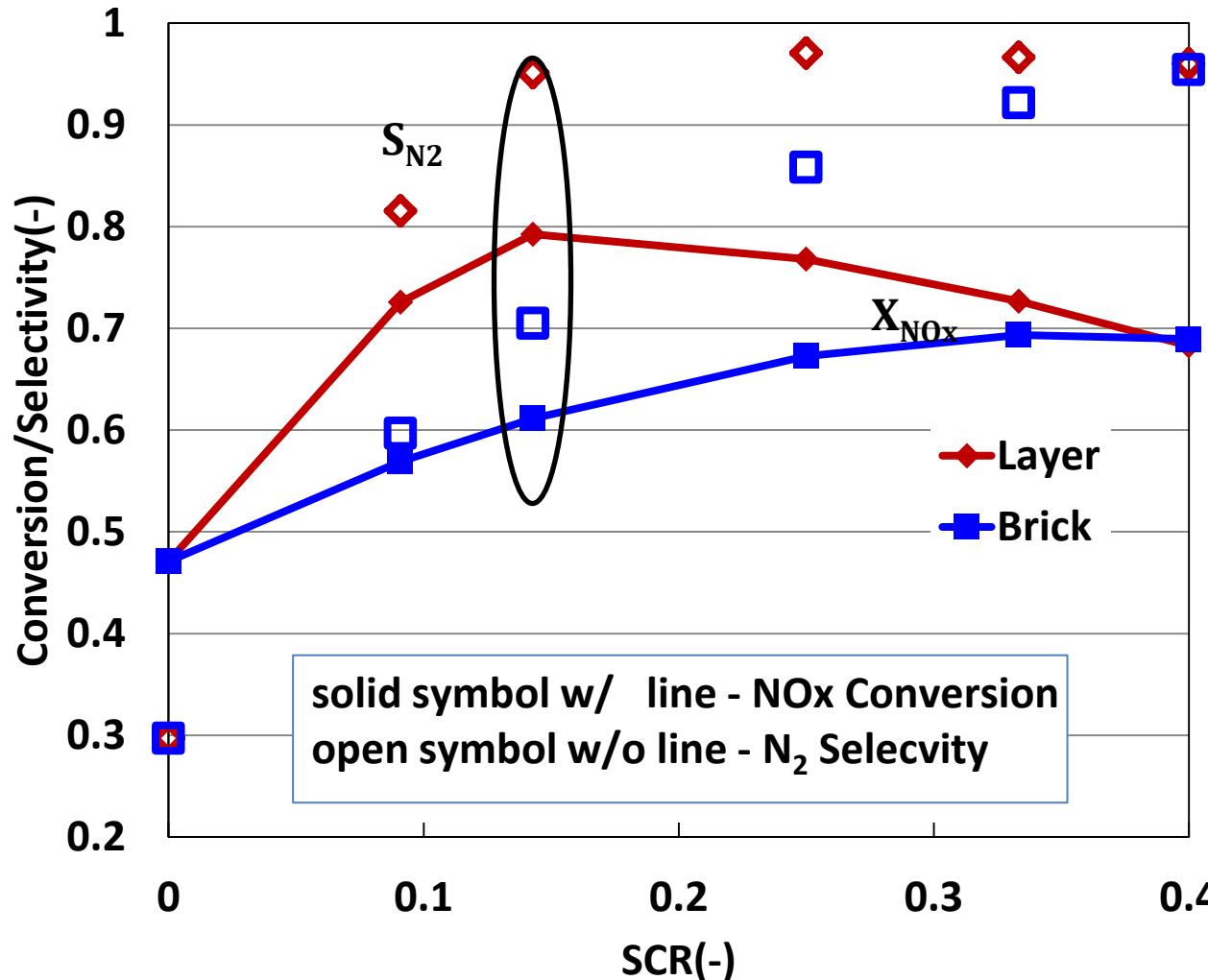


Conditions: Lean: 60s 500 ppm NO + 5% O₂
Rich: 20s 5000 ppm H₂

Impact of SCR becomes less significant at higher temperature → significant NH₃ consumption in LNT

Layered vs Brick

230°C - 60/20 cycles



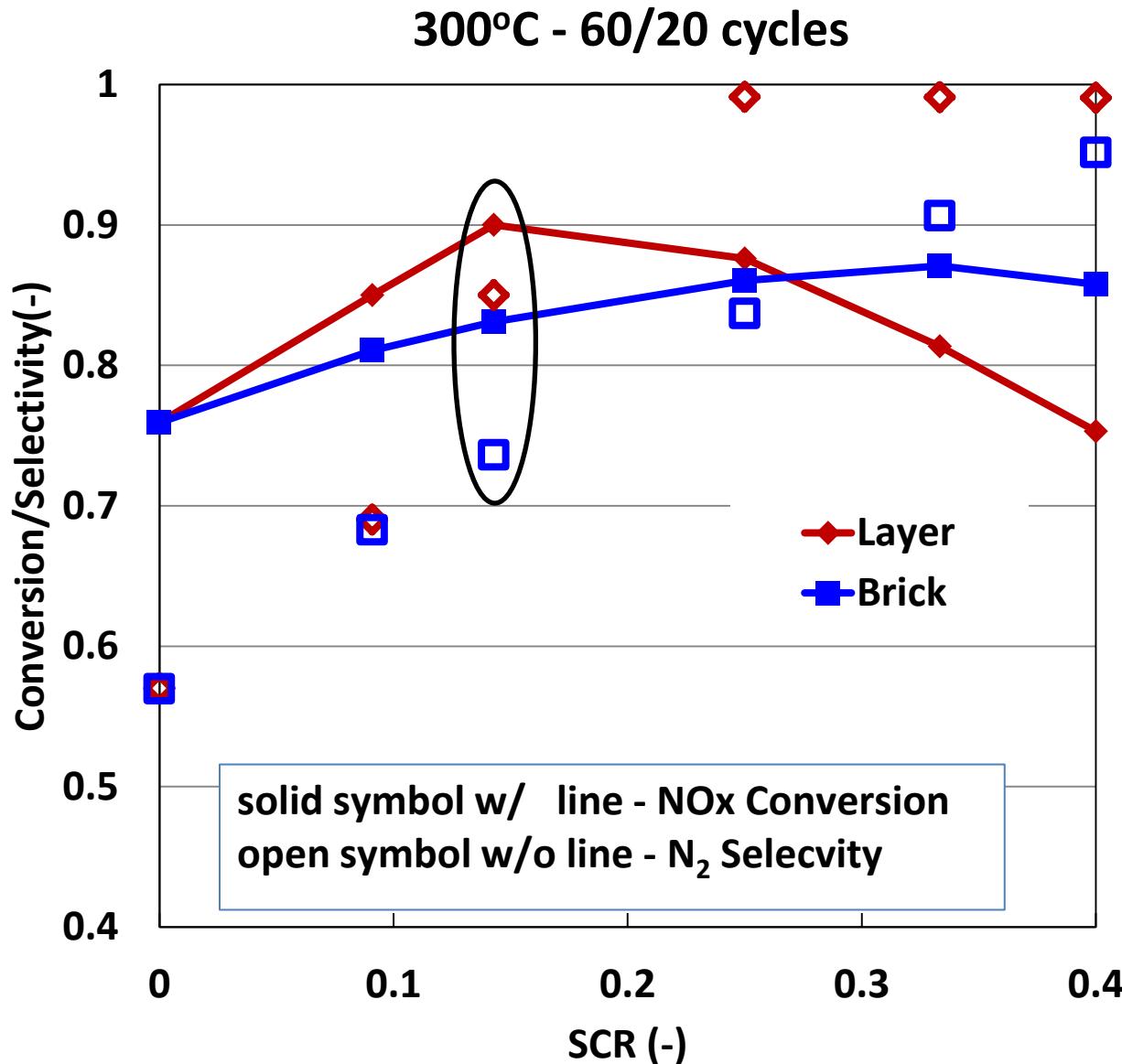
$L = 2\text{ cm}$
 $LNT = 30 \mu\text{m}$

SCR	Layer (μm)	Brick (cm)	R _{Ω₂} (μm)
0.00	0	0.00	30
0.09	3	0.18	33
0.14	5	0.28	35
0.25	10	0.50	40
0.33	15	0.66	45
0.40	20	0.80	50

Conditions:
 Lean: 60s 500
 ppm NO + 5% O₂

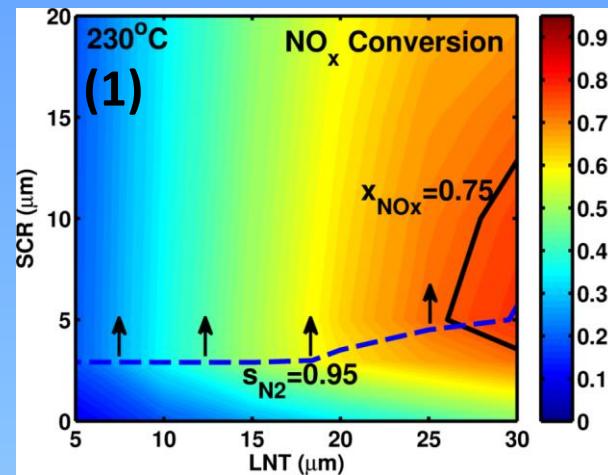
Rich: 20s 5000
 ppm H₂

Layered vs Brick



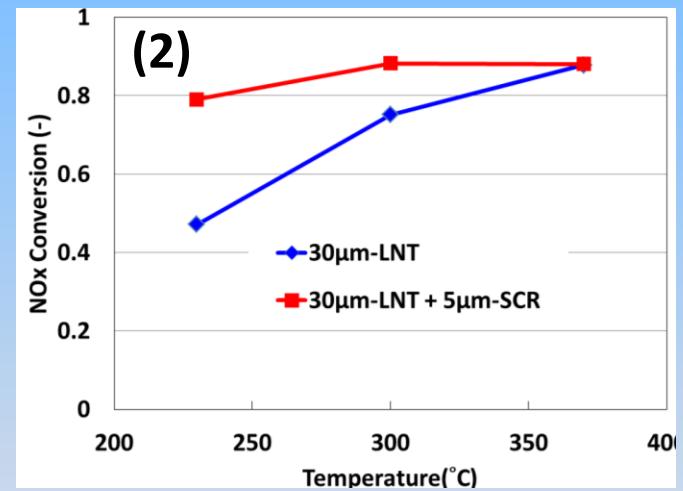
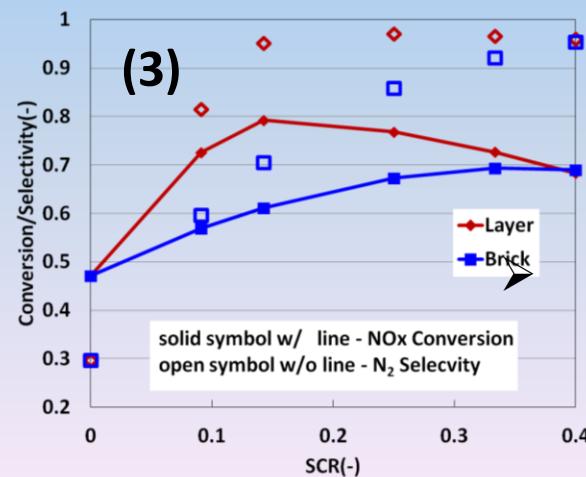
$L = 2\text{ cm}$
 $LNT = 30 \mu\text{m}$

Summary and Conclusions



- Multiple combination of LNT and SCR can give same NO_x conversion
- For a given LNT loading and temperature, there exists an SCR loading that gives max NO_x conversion

- SCR function is diminished at higher temperature



Better storage and utilization of generated NH₃ in dual layer configuration compared to brick

THANK YOU FOR YOUR ATTENTION!

Acknowledgements:

