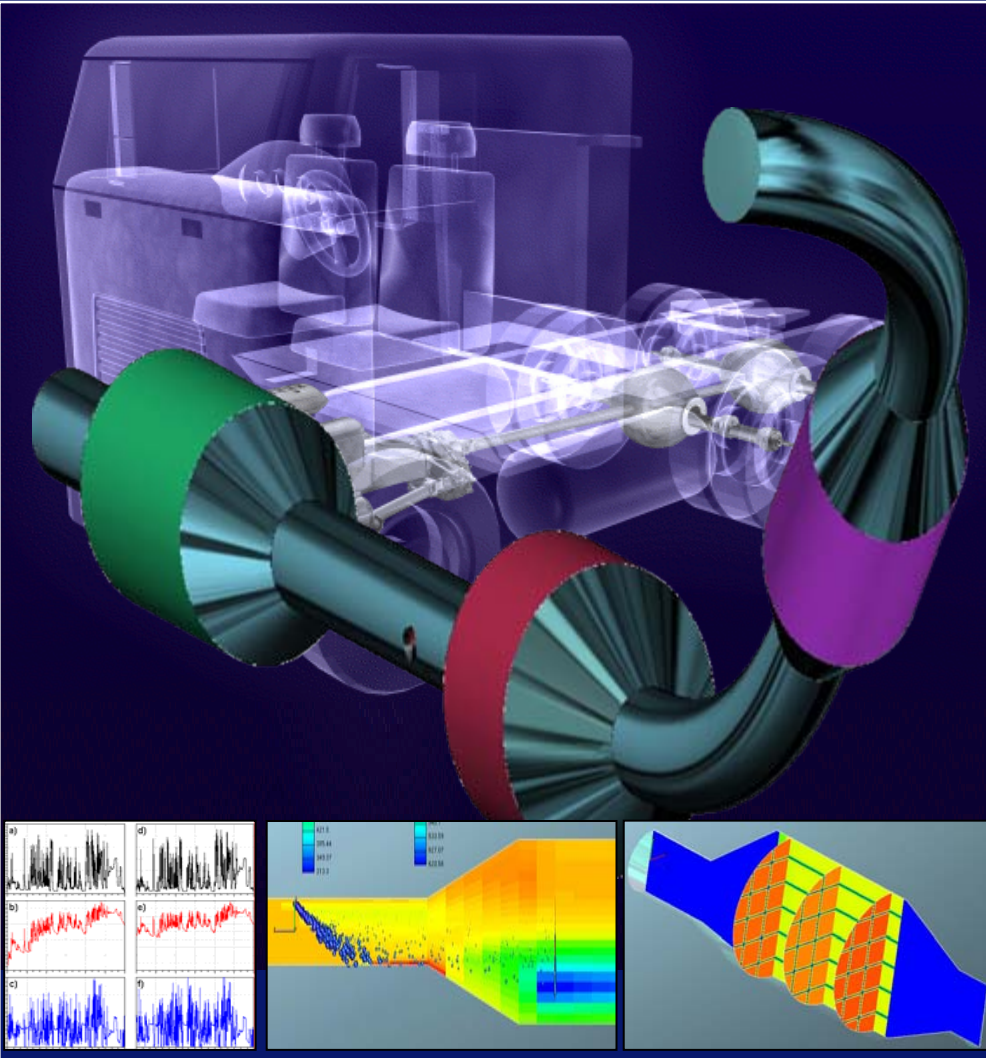


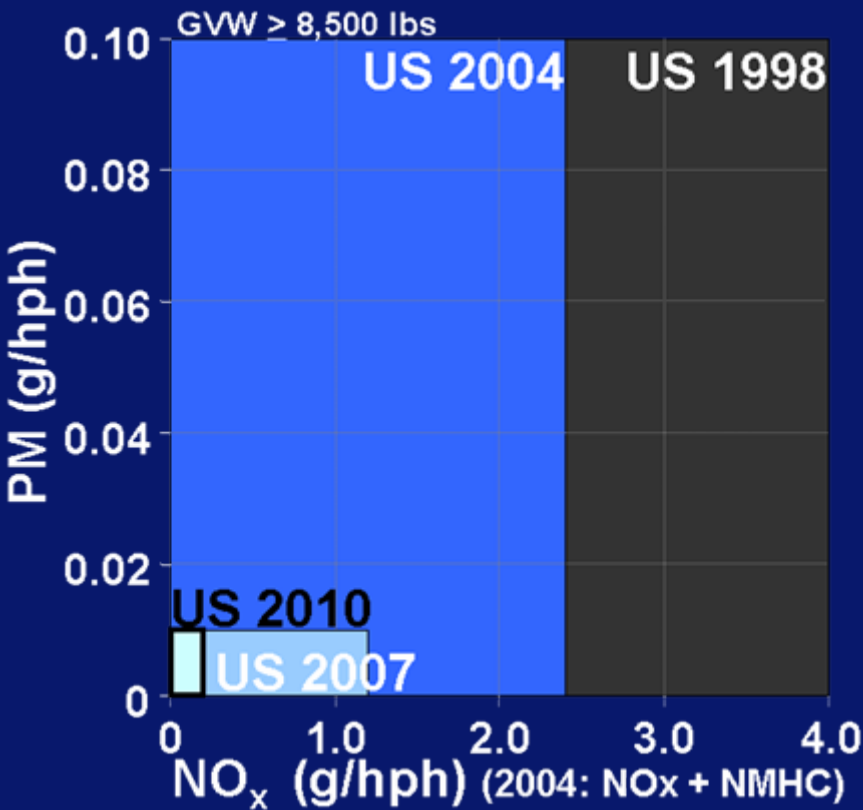
1D/3D Simulation in the Development of DeNOx Aftertreatment Systems for US 2010 Heavy Duty Applications

Johann C. Wurzenberger

Roland Wanker
Martin Schüßler
Wilfried Edelbauer
Eberhard von Berg
Klaus Pachler
Bernd Breitschädel
Clemens Fink
Ruppert Scheucher
Alex Raulot
Moritz Frobenius
Reinhard Tatschl



- **Introduction**
- **System Model and Simulation Workflow**
- **Models and Results**
 - **DOC**
 - **DPF**
 - **Injector**
 - **SCR**
 - **Pipes**
- **DeNOx Performance during WHTC**
- **Conclusion**



Growing importance of exhaust aftertreatment due to emissions legislation needs more effort for

- Component and system layout
- System application

1D/3D Simulation Workflow

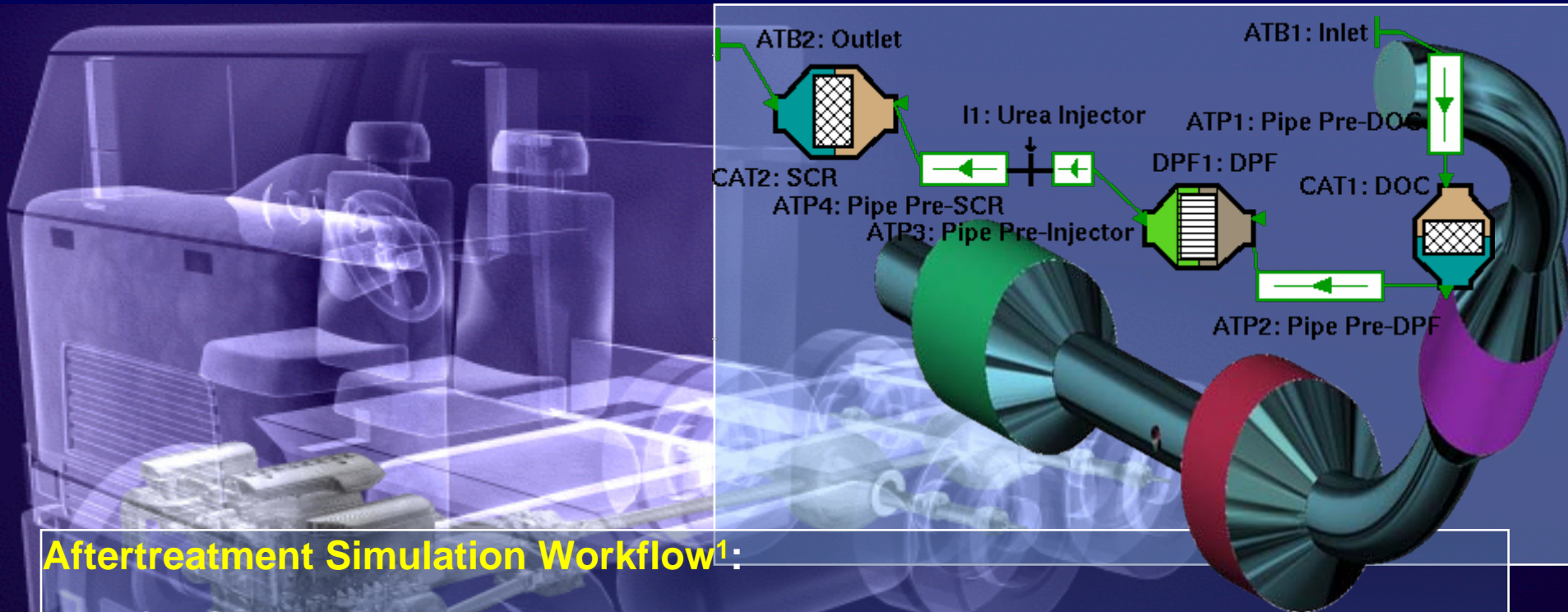
for efficient integration of simulation in development process using

- 1D model alibration system analysis and optimization
- 3D detail analysis

→ Example:

1D/3D analysis of heavy-duty exhaust system

Exhaust Gas Aftertreatment System

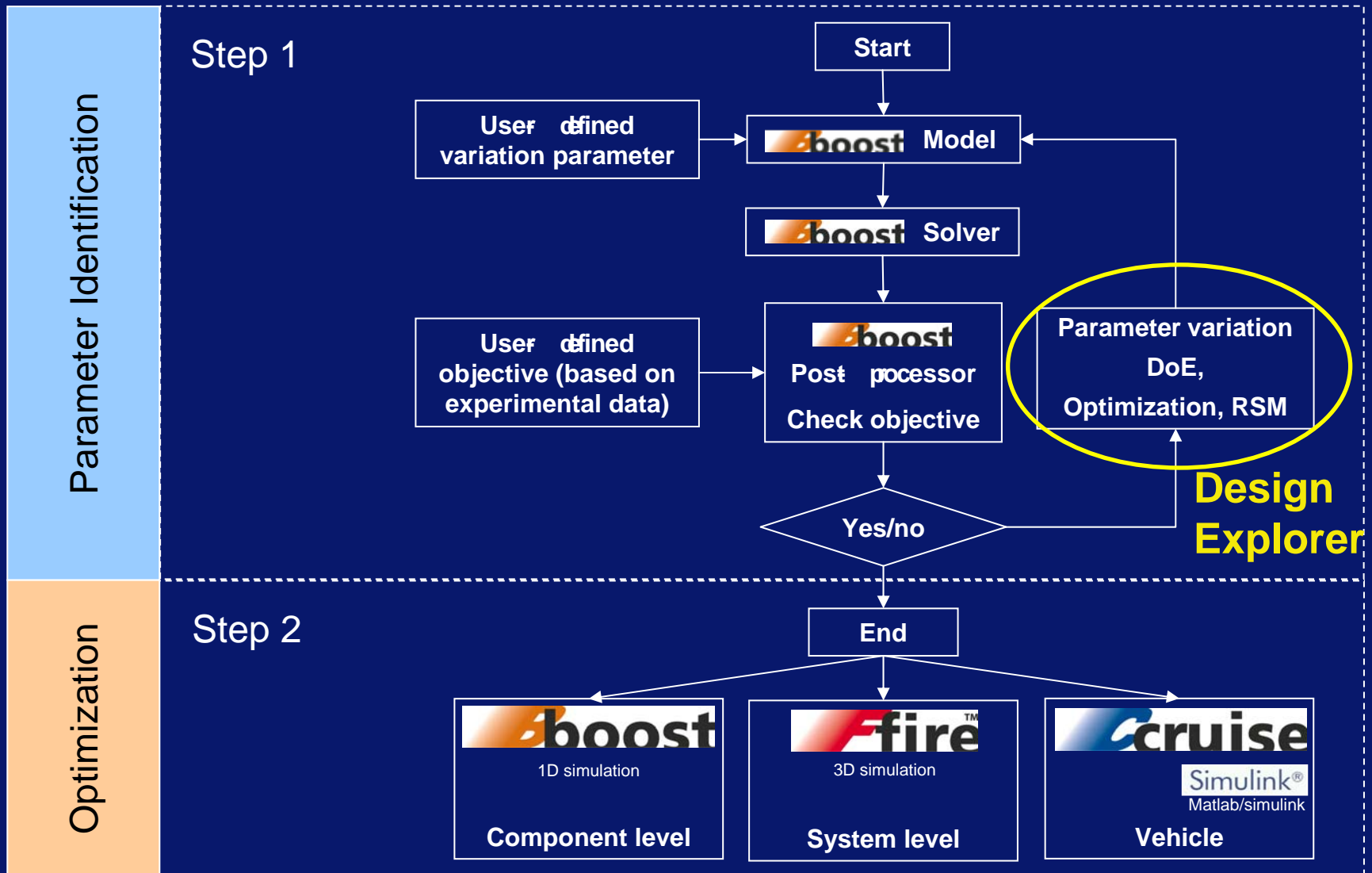


Aftertreatment Simulation Workflow¹:

- 1) Calibrate individual components with experimental data in an automatic parameter optimization process (AVL Design Explorer)
- 2) Investigate 3D effects with FIRE
- 3) Build up 1D BOOST model of overall system
- 4) Calculate the performance of the system during drive cycle

1: see ATZ 7/8 2004

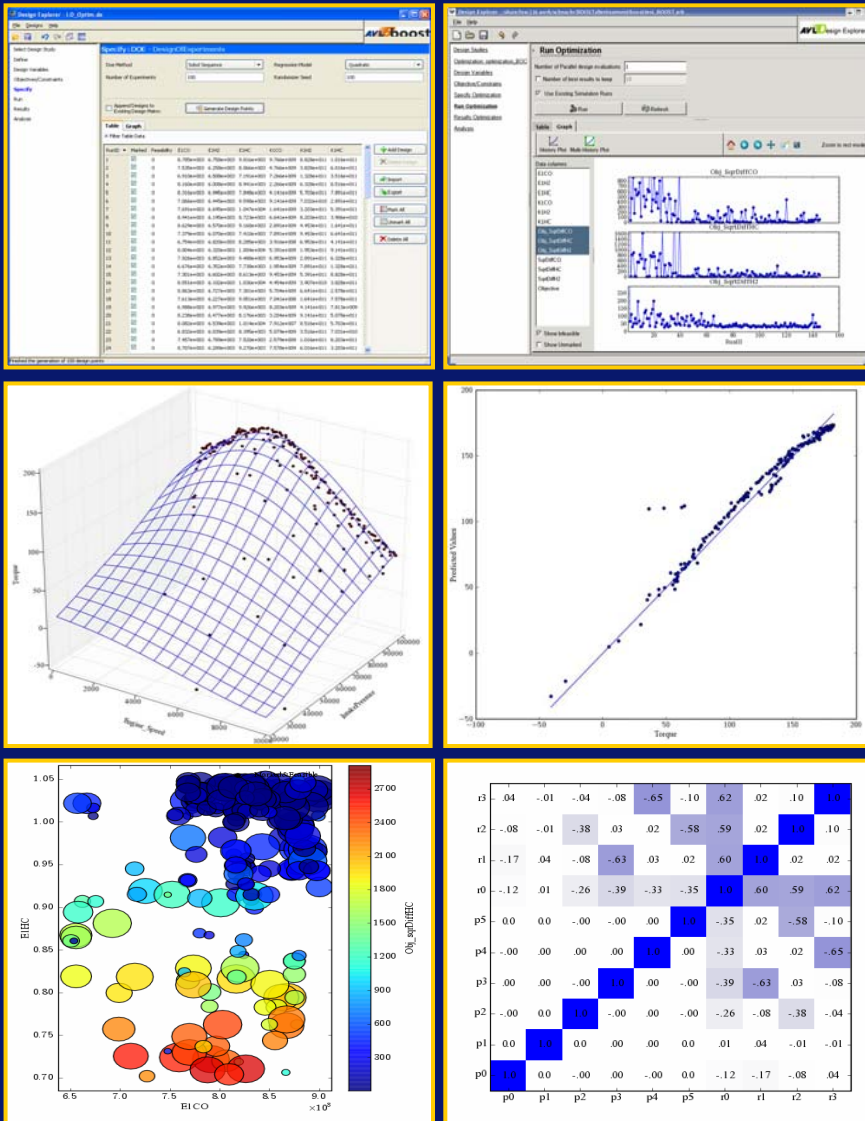
Aftertreatment Simulation Workflow

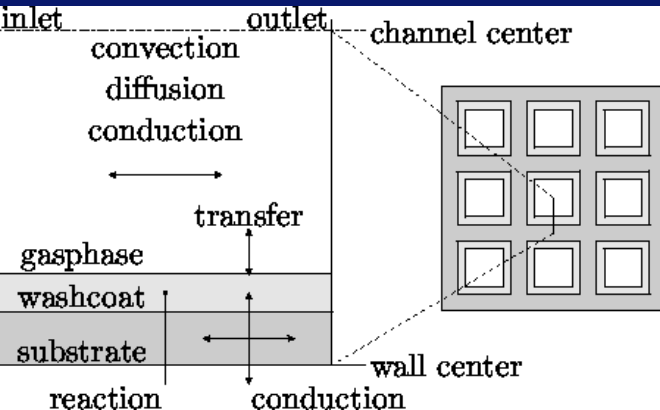
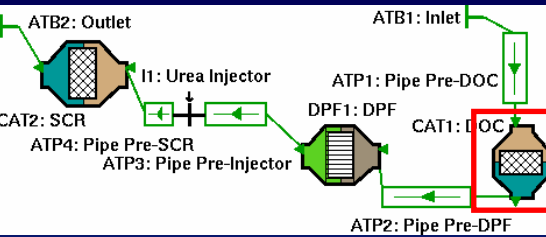


- **Design Explorer**
- **Environment for**
 - Design optimization
 - Sensitivity analysis
 - Parameter identification

Using

- **DoE** (Full Factorial Design, Sobol Sequence, Latin Hypercube Sampling, Orthogonal Arrays)
- **Optimization** (NSGA, Nelder-Mead, NLPQL,...)
- **Response Surface Methods** (NN, SVM)

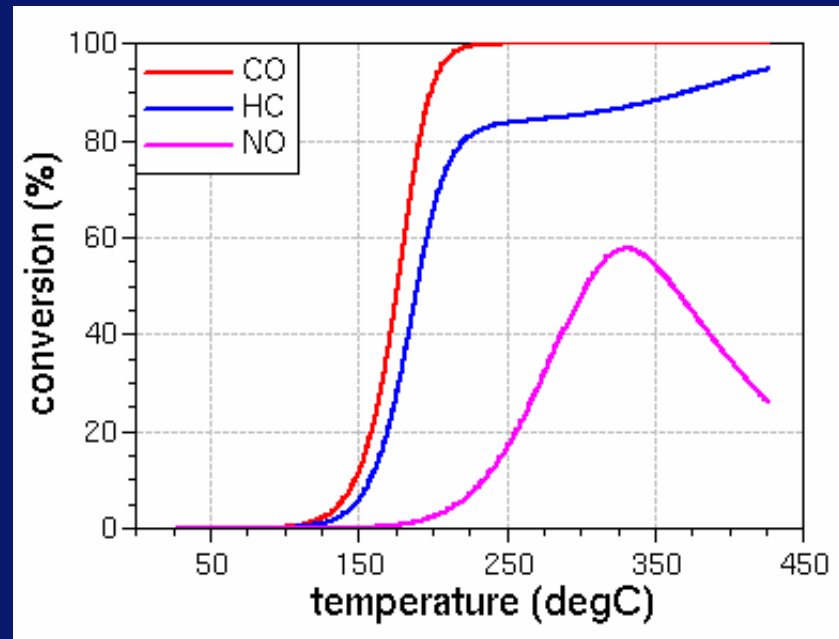




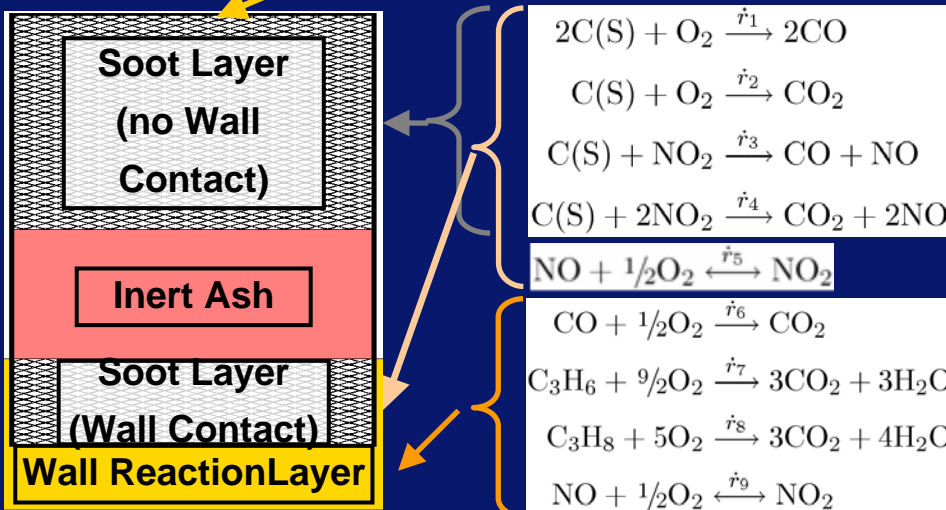
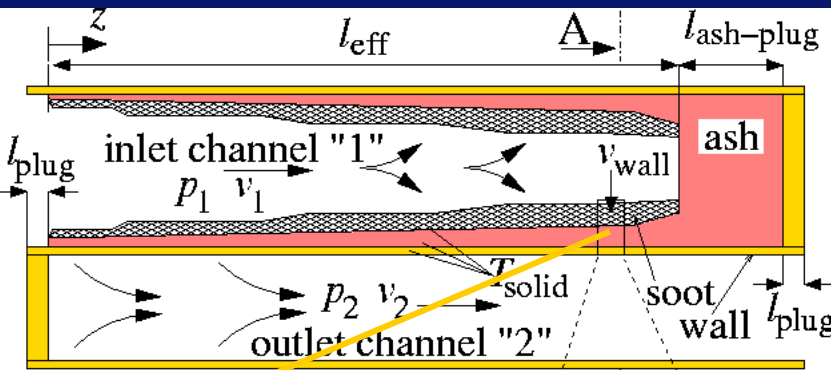
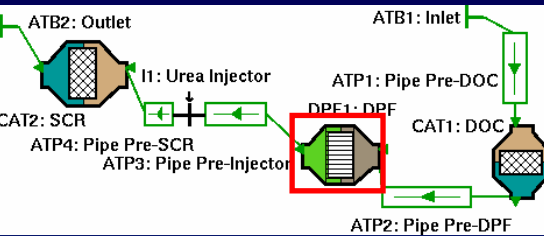
<input checked="" type="checkbox"/>	R1:	$\text{CO} + \frac{1}{2}\text{O}_2 \rightarrow \text{CO}_2$
<input checked="" type="checkbox"/>	R2:	$\text{C}_3\text{H}_6 + \frac{9}{2}\text{O}_2 \rightarrow 3\text{CO}_2 + 3\text{H}_2\text{O}$
<input type="checkbox"/>	R3:	$2\text{CO} + 2\text{NO} \rightarrow 2\text{CO}_2 + \text{N}_2$
<input type="checkbox"/>	R4:	$\text{H}_2 + \frac{1}{2}\text{O}_2 \rightarrow \text{H}_2\text{O}$
<input checked="" type="checkbox"/>	R5:	$2\text{NO} + \text{O}_2 \leftrightarrow 2\text{NO}_2$
<input type="checkbox"/>	R6:	$\text{CO} + \text{H}_2\text{O} \leftrightarrow \text{CO}_2 + \text{H}_2$
<input checked="" type="checkbox"/>	R7:	$\text{C}_3\text{H}_8 + 5\text{O}_2 \rightarrow 3\text{CO}_2 + 4\text{H}_2\text{O}$

Transient 1D 2-Phase model for an arbitrary number of gas and surface species¹

- 4 Oxidation reactions are enabled
- Light-off simulation shows typical behavior for CO, HC and NO

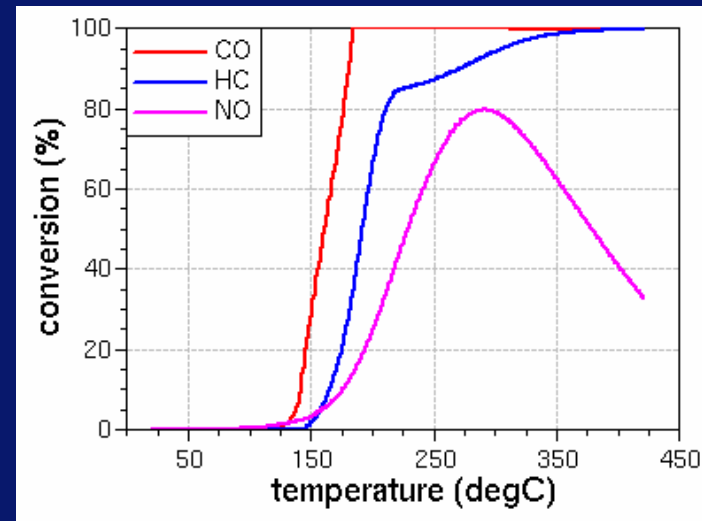


1: see SAE 2003-01-1003



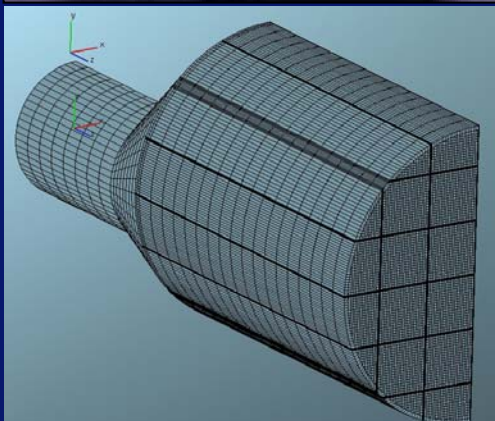
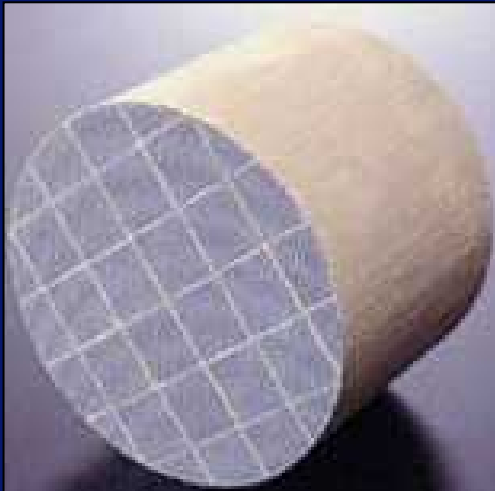
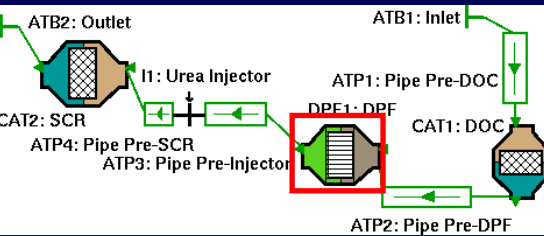
Wall flow DPF model¹:

- Asymmetric channel geometries
- Ash and soot loading
- Soot depth and cake layer filtration
- Active and passive soot regeneration w/o catalytic support
- Catalytic wall reactions



1: see SAE 2007-01-1137

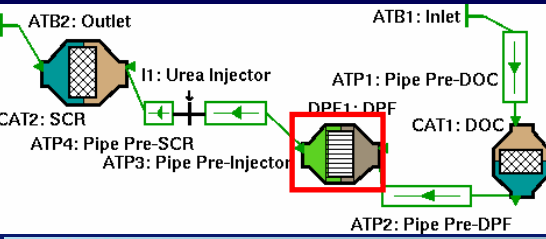
SiC Filter with Segmentation



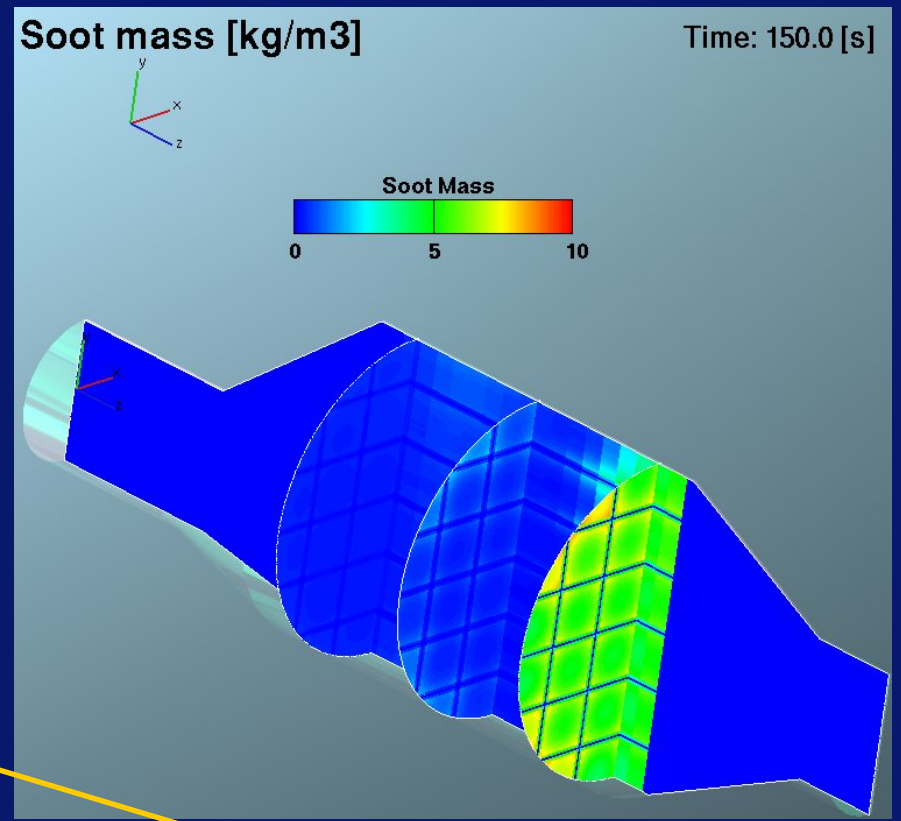
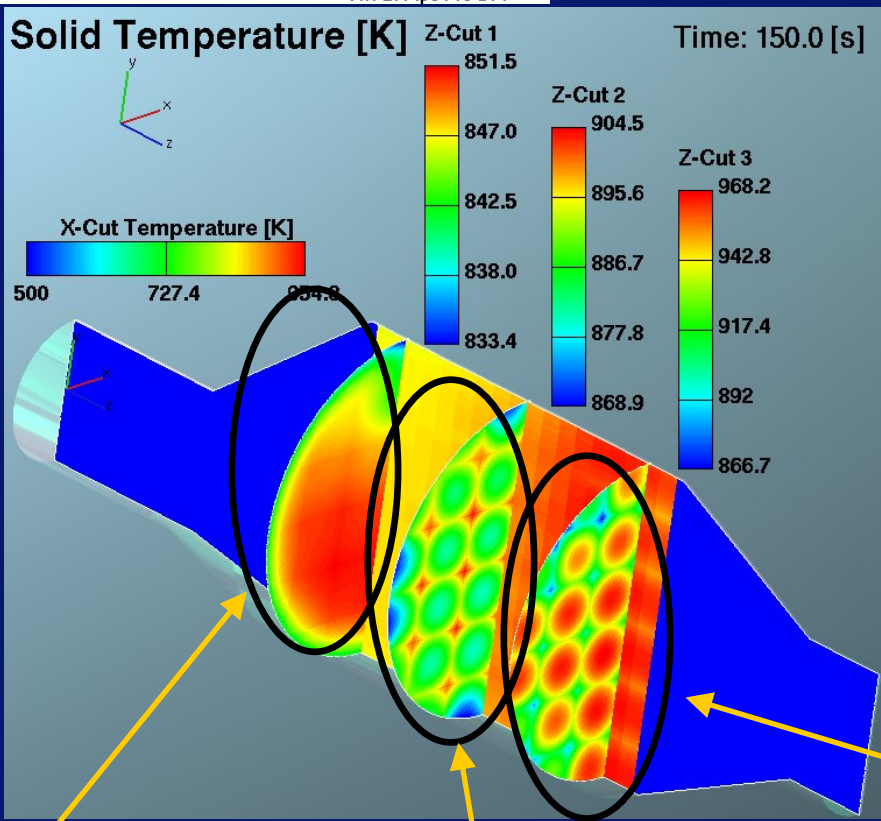
- **Gluing zones**
- **Impact on pressure drop**
 - Reduced effective flow area
 - Different number of active filtration sides near gluing zones (2/3/4 Sides)
- **Impact on regeneration**
 - Different thermal inertia
 - Different heat transfer behavior

Active Regeneration of Segmented SiC DPF

Snapshots of Movies

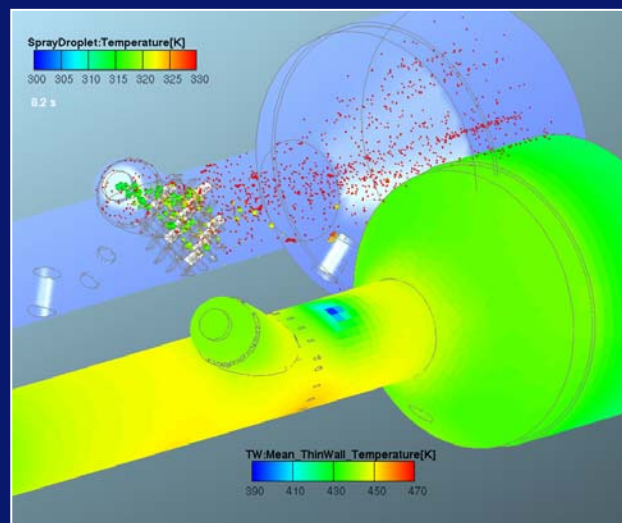
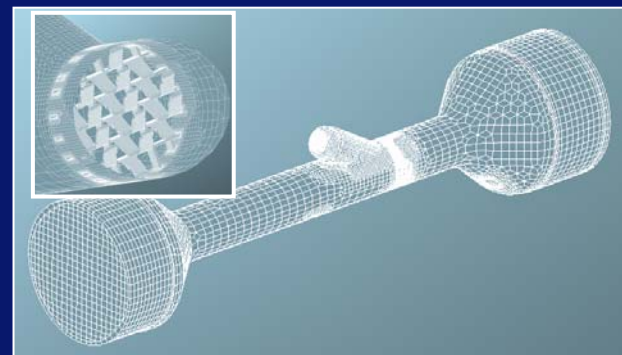
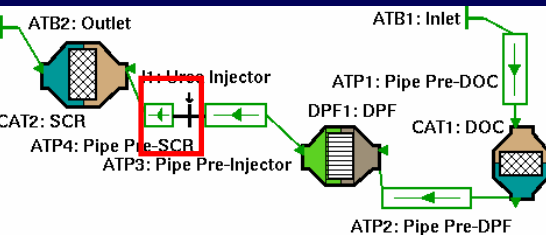


Solid temperature and soot mass at the of forced regeneration (t=150s)



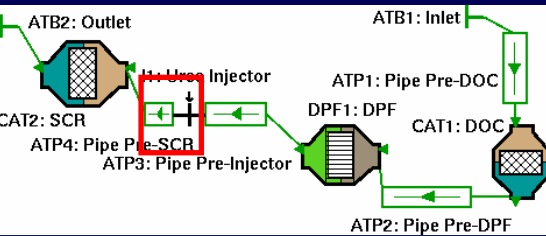
- Uniform temperature
- Gluing zones show highest temperatures
- Gluing zones show lowest temperatures

Urea Injector Model

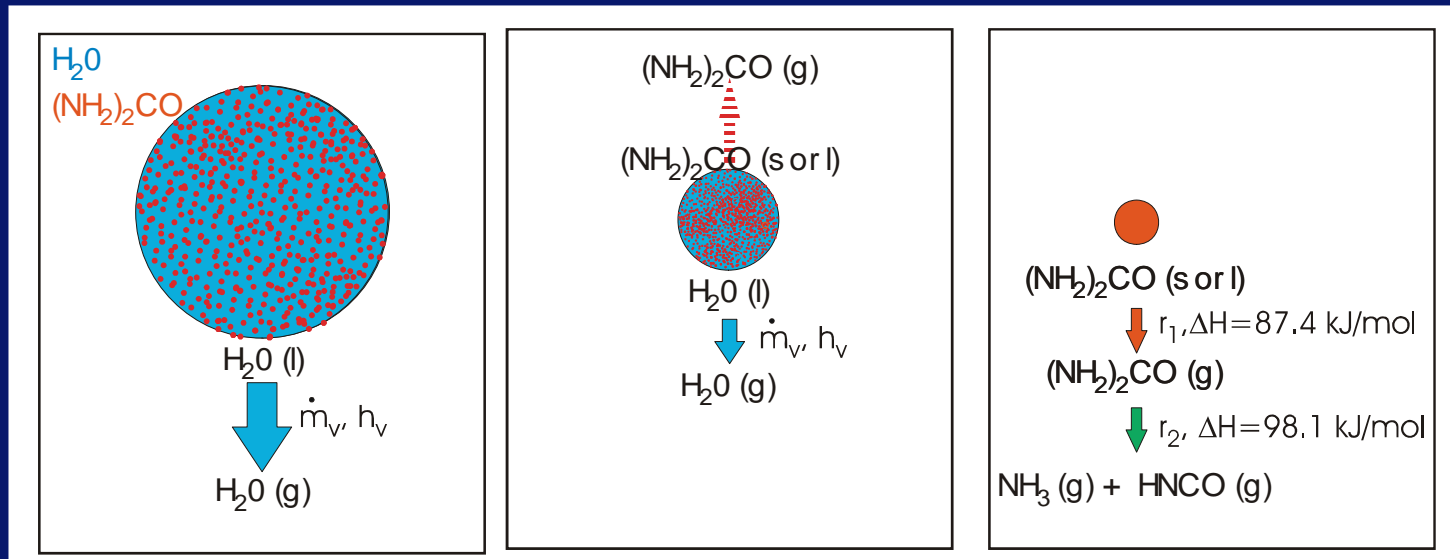


- **Injection of urea-water solution**
- **Spray / gas interaction**
 - Liquid / gaseous momentum exchange
 - Droplet / gas heat transfer
 - Water evaporation / urea thermolysis
- **Spray / wall / wallfilm interaction**
 - Spray impingement
 - Droplet / wall heat transfer
 - Wallfilm formation
 - Wallfilm evaporation / thermolysis
- **Cooling of walls**
 - Lateral heat conduction
- **Hydrolysis**
- **Catalytic reactions**

Evaporation / Thermolysis / Hydrolysis - Model



Droplet Mass transfer model

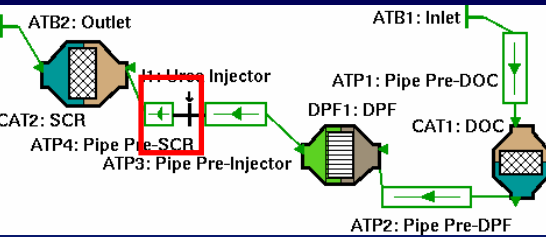


Evaporation of water: $\text{H}_2\text{O} (\text{l}) \rightarrow \text{H}_2\text{O} (\text{g})$

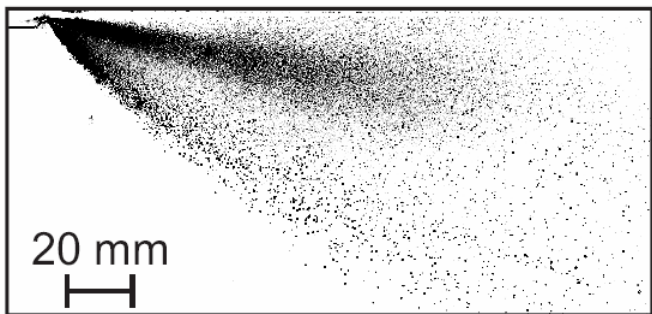
Thermolysis: $(\text{NH}_2)_2\text{CO} (\text{s or l}) \rightarrow \text{NH}_3 (\text{g}) + \text{HNCO} (\text{g})$

Hydrolysis: $\text{HNCO} (\text{g}) + \text{H}_2\text{O} (\text{g}) \rightarrow \text{NH}_3 (\text{g}) + \text{CO}_2 (\text{g})$

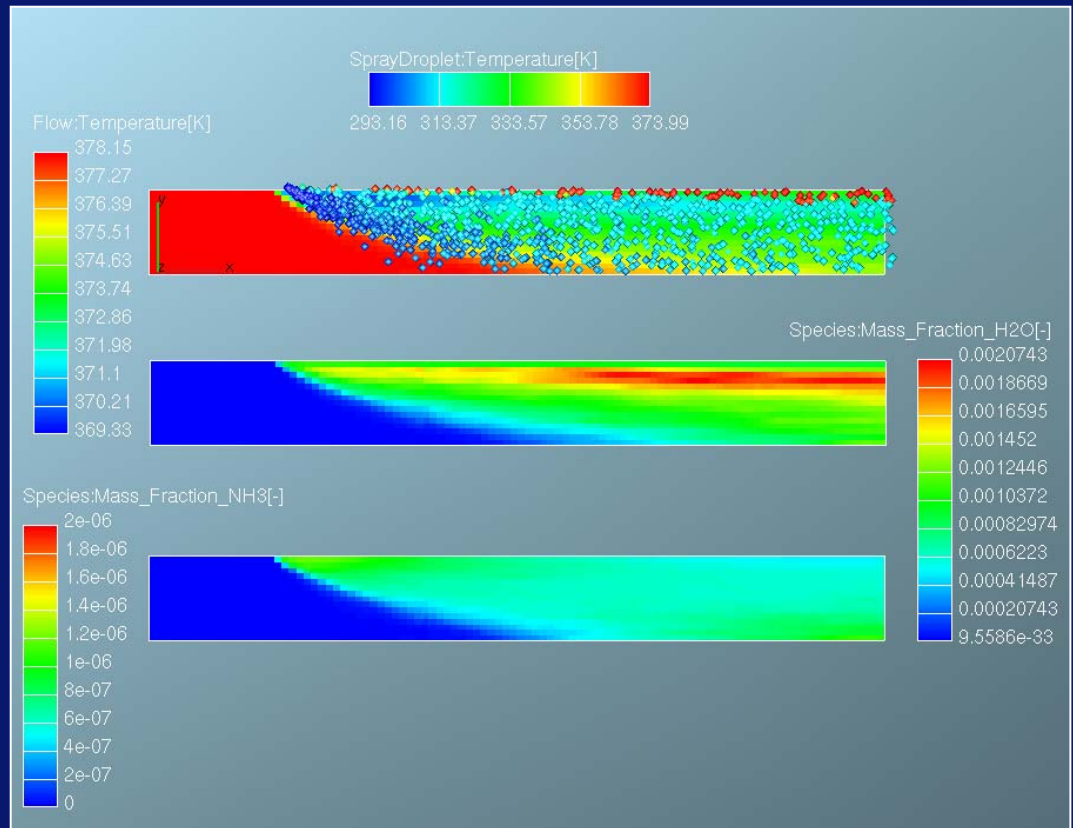
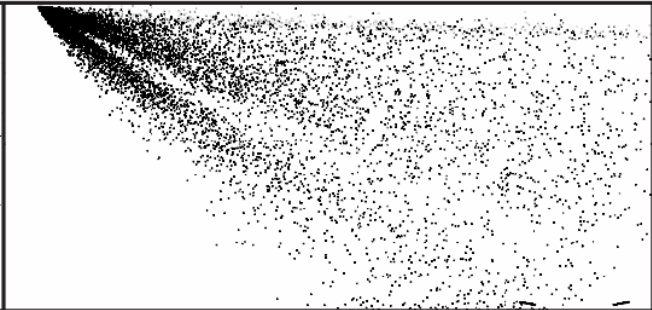
Spray in Cross-Flow - Validation



Measurement

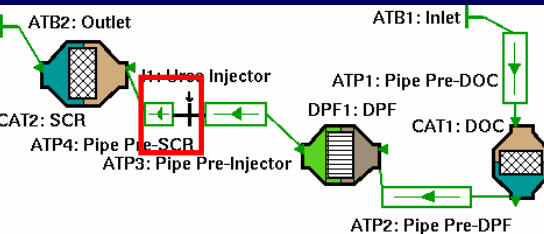


Simulation



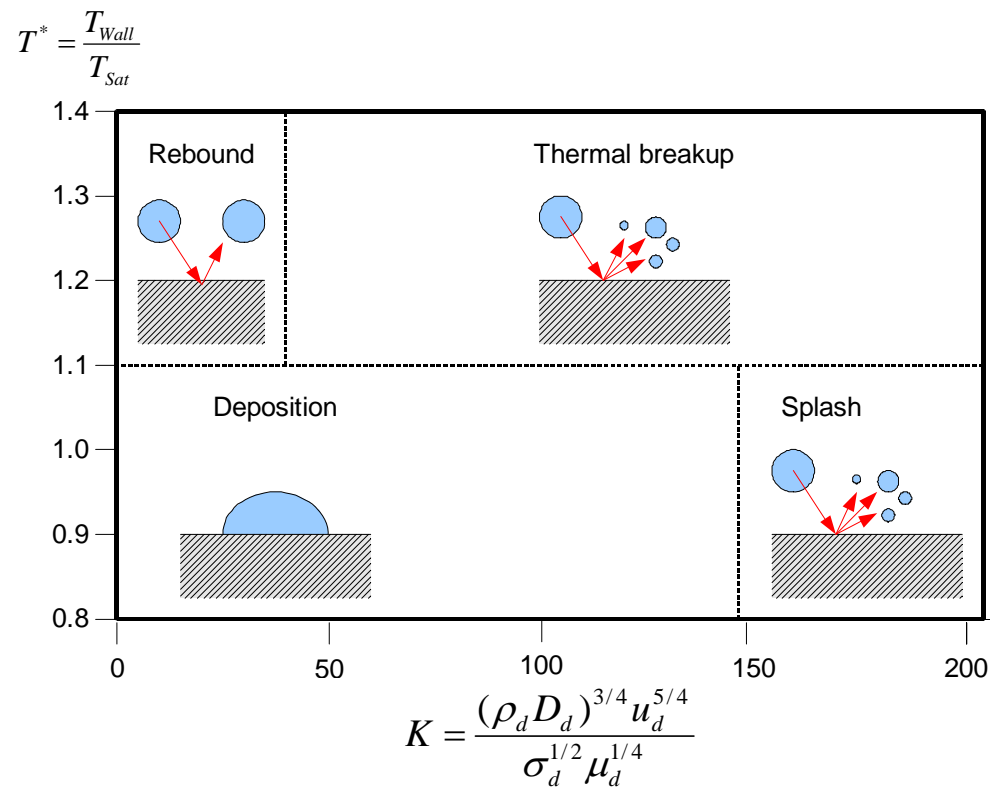
Schwarzenberg, M. Untersuchung von Spraykonzepten zur Dosierung von Harnstoff-Wasser-Lösung beim Einsatz eines SCR-Verfahrens. Diplomarbeit, RWTH Aachen, 2005

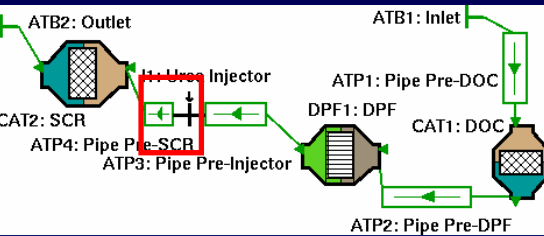
Spray Wall Interaction Model



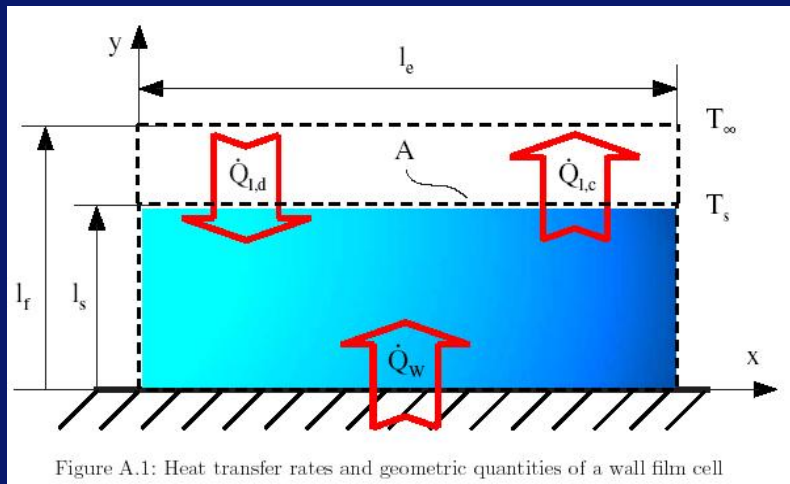
Wall Impingement depends on

- Droplet velocity
- Droplet temperature
- Wall temperature
- Droplet properties (size, viscosity,...)





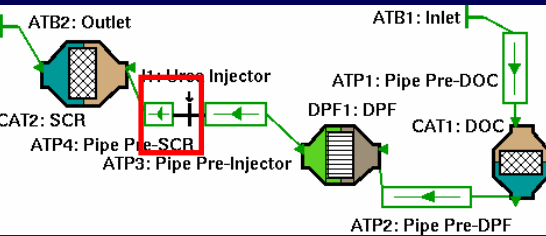
Sketch of Film Element



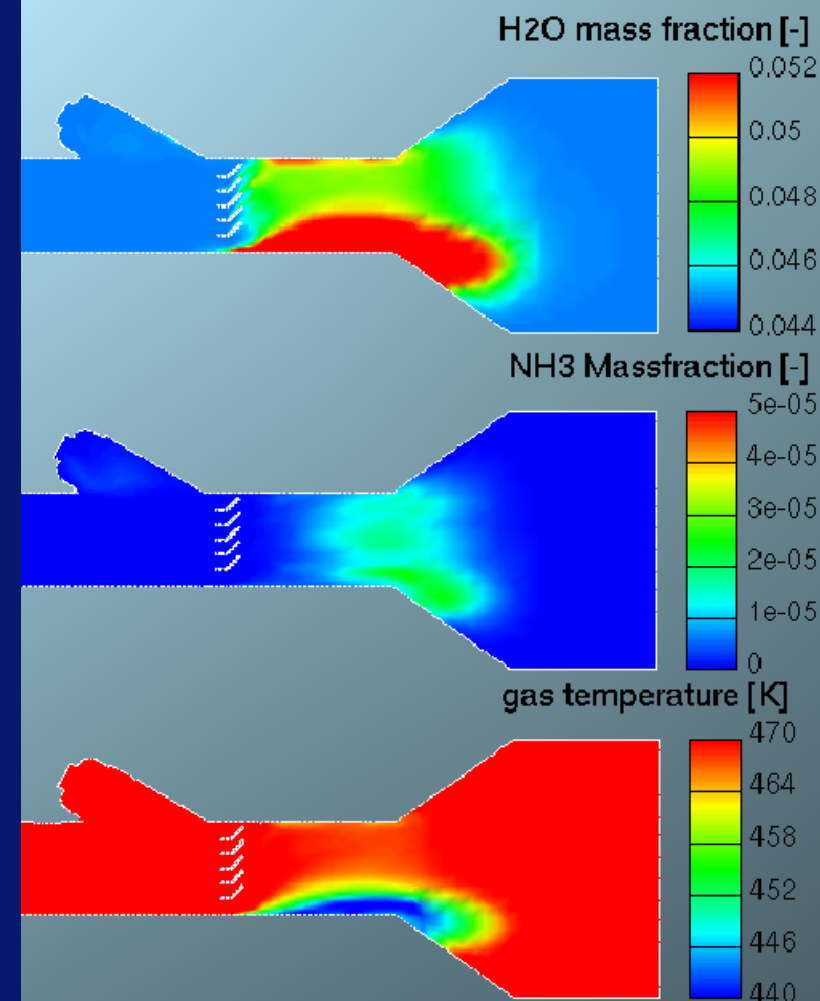
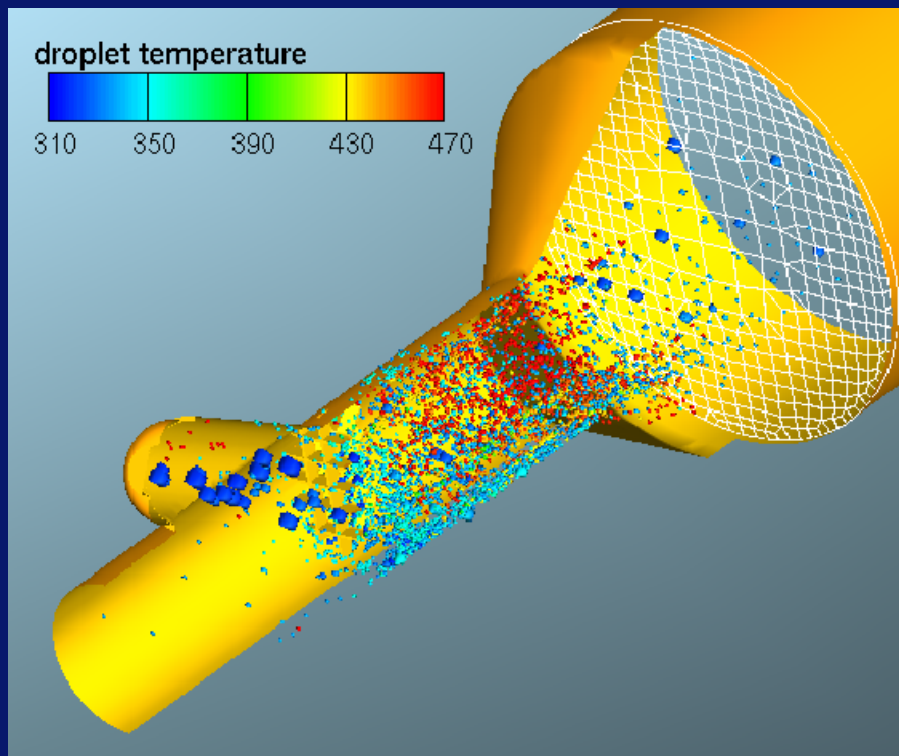
Modeled Effects:

- Film formation and transport
- Temperature dependent splashing models
- Heat transfer between film, droplets and wall
- Multi-component species transport and evaporation / thermolysis

Urea-Injection and NH3 Formation

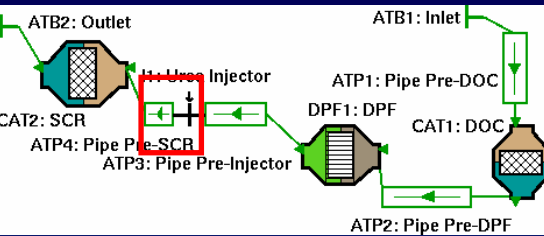


Snapshot of Movies

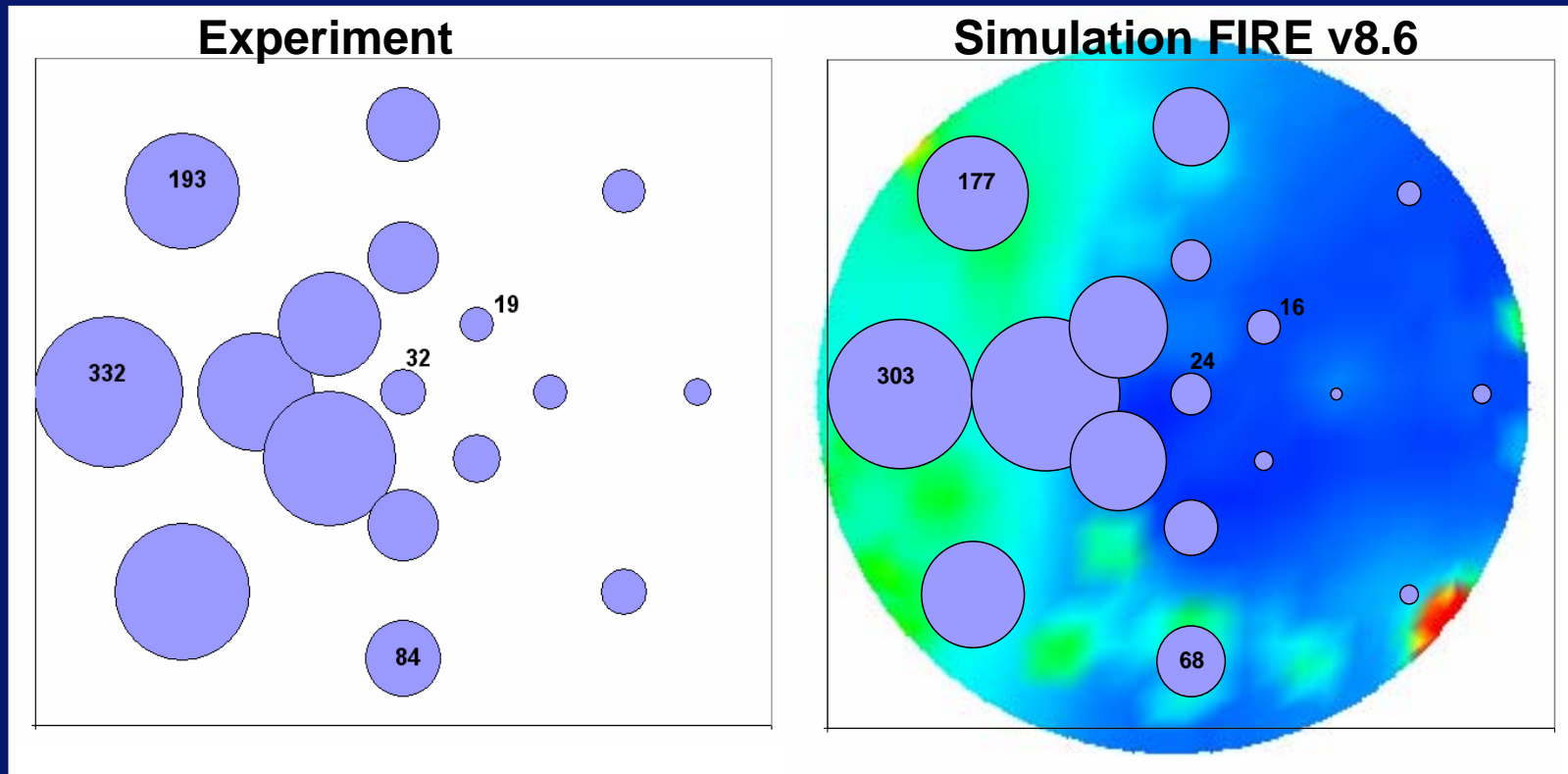


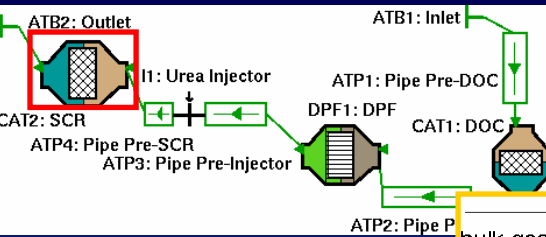
Detailed modeling of spray, evaporation, wall interaction,... is basis to predict NH3 formation and uniformity

NH3 Distribution

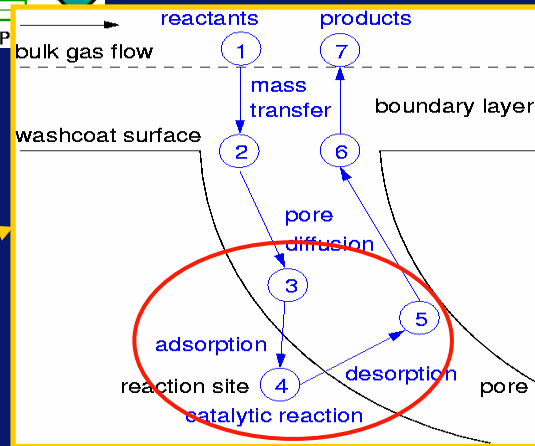
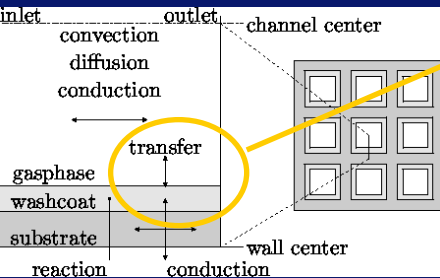


NH3-Concentration past the hydrolysis-catalyst (ppm), application example without mixer





Transient 1D 2-Phase model for an arbitrary number of gas and surface species¹



- Storage and desorption of NH₃ is explicitly taken into account
- The reaction model is reduced to 4 major reactions

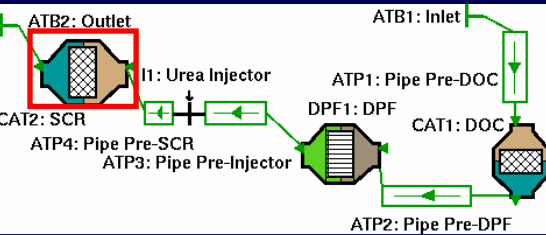
Transient SCR Mechanism

Select: SCR HSO_SCR All None

	Sec1	Sec2	Sec3	Chemical Reaction
R1:	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	$\text{HCNO} + \text{H}_2\text{O} \rightarrow \text{NH}_3 + \text{CO}_2$
R2:	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	$\text{NH}_3 + \text{S} \rightarrow \text{NH}_3(\text{S})$
R3:	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	$\text{NH}_3(\text{S}) \rightarrow \text{NH}_3 + \text{S}$
R4:	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	$4\text{NH}_3 + 4\text{NO} + \text{O}_2 \rightarrow 4\text{N}_2 + 6\text{H}_2\text{O}$
R5:	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	$4\text{NH}_3 + 2\text{NO} + 2\text{NO}_2 \rightarrow 4\text{N}_2 + 6\text{H}_2\text{O}$
R6:	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	$8\text{NH}_3 + 6\text{NO}_2 \rightarrow 7\text{N}_2 + 12\text{H}_2\text{O}$
R7:	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	$4\text{NH}_3 + 3\text{O}_2 \rightarrow 2\text{N}_2 + 6\text{H}_2\text{O}$
R8:	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	$4\text{NH}_3 + 3\text{O}_2 \rightarrow 2\text{N}_2 + 6\text{H}_2\text{O}$
R9:	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	$2\text{NO} + \text{O}_2 \leftrightarrow 2\text{NO}_2$

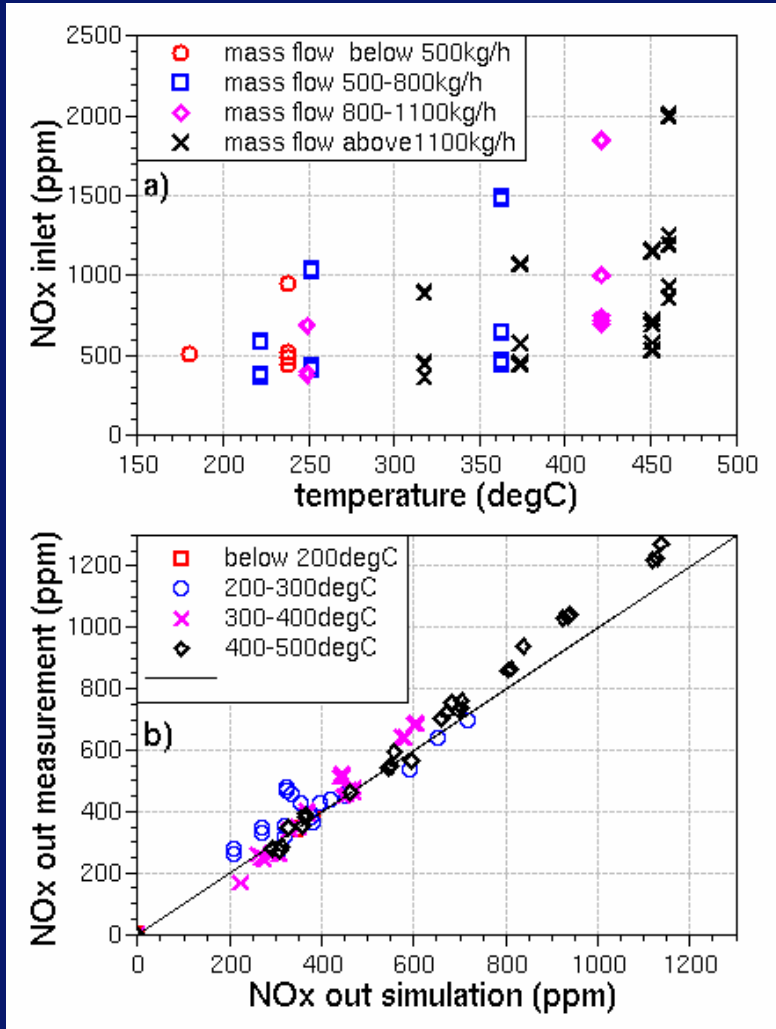
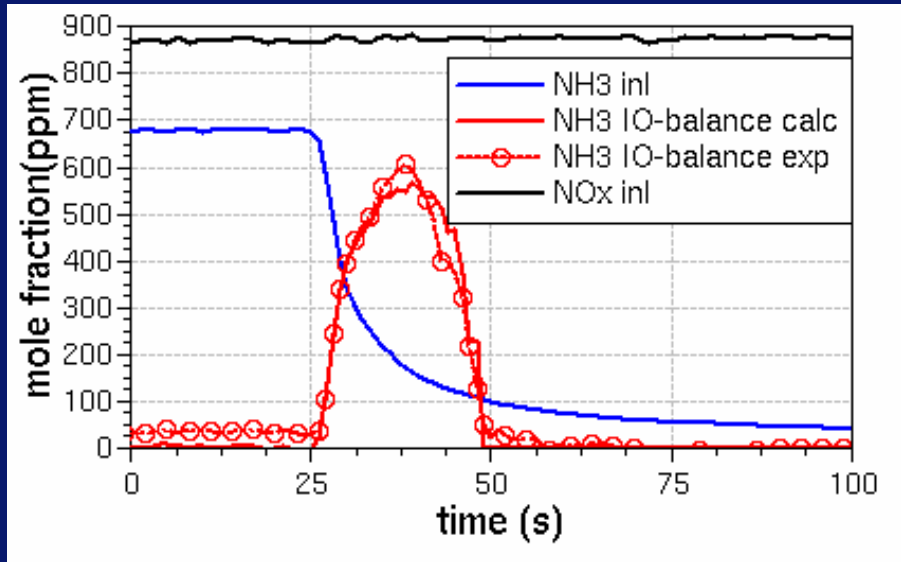
1: see SAE 2005-01-0948

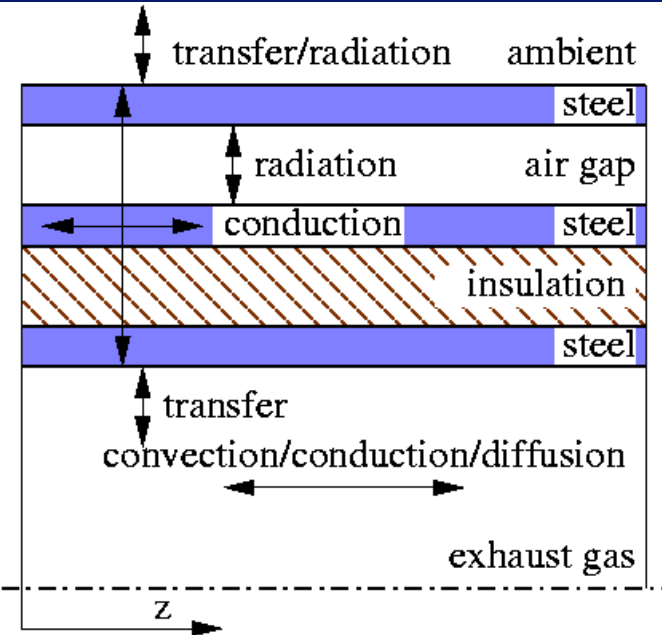
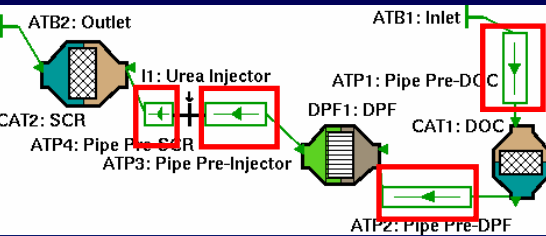
SCR, NO_x-Conversion Performance



Simulation/experiment for 108 load points

Simulation/experiment for NH₃-desorption during dosing-step





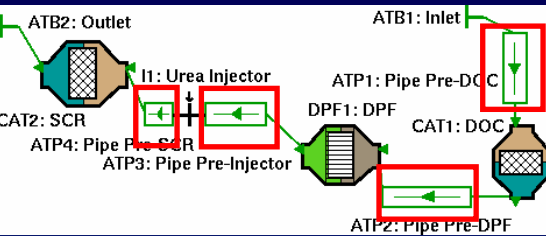
Transient 2D heat transfer model for an arbitrary number of wall layers¹

▪ Main features:

- Conduction in opaque layers
- Radiation
- Free convection in air-gaps
- Free and forced convection to ambient
- Temperature dependent physical properties

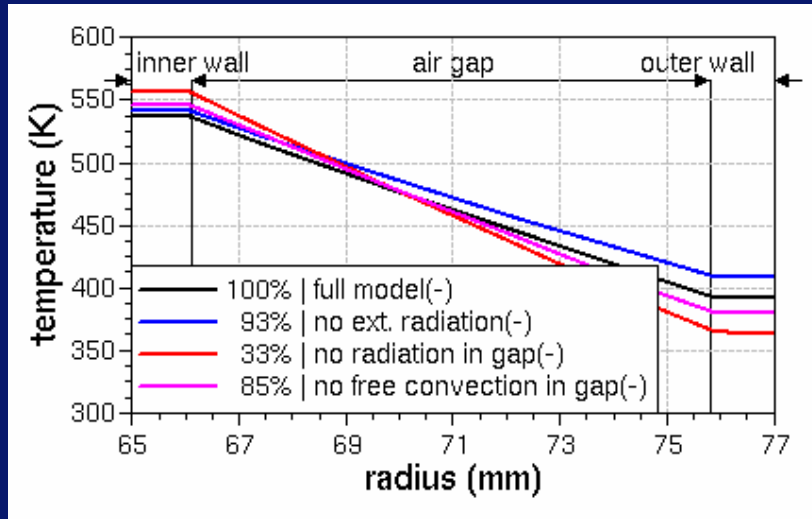
¹: see SAE 2008-01-0865

Pipe Wall Heat Loss Simulation

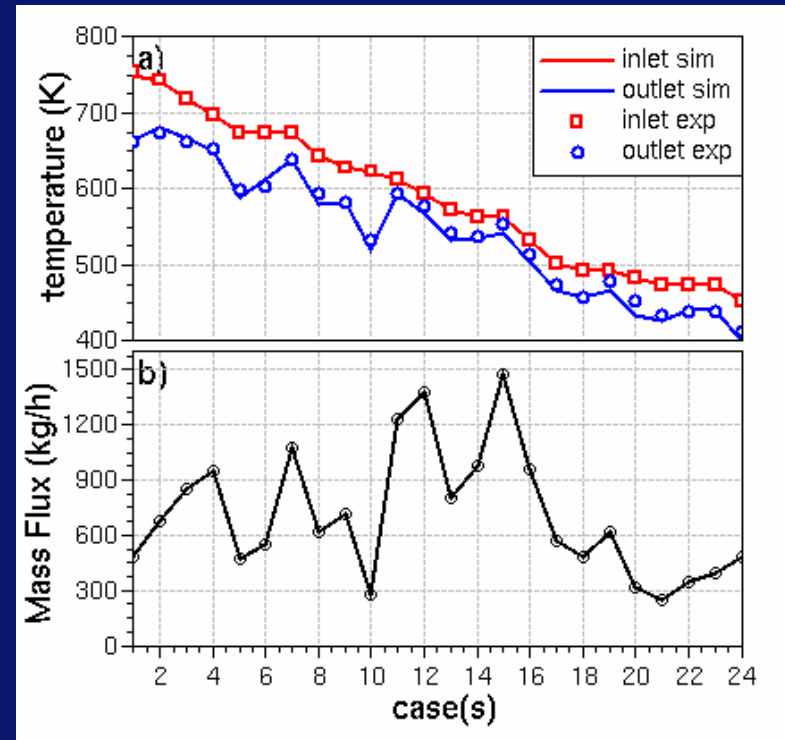


Simulation/experiment single wall pipe

Dual wall pipe, effect study

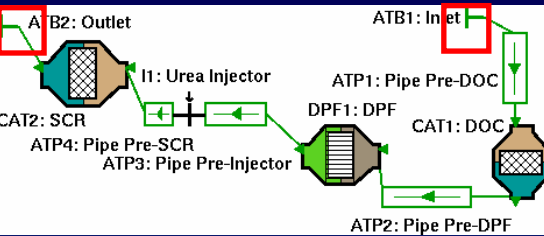


Impact of radiation in the gap is significant



Pipe outlet temperatures are well covered by the model (internal heat transfer factor was adapted)

Boundary Conditions for Drive Cycle

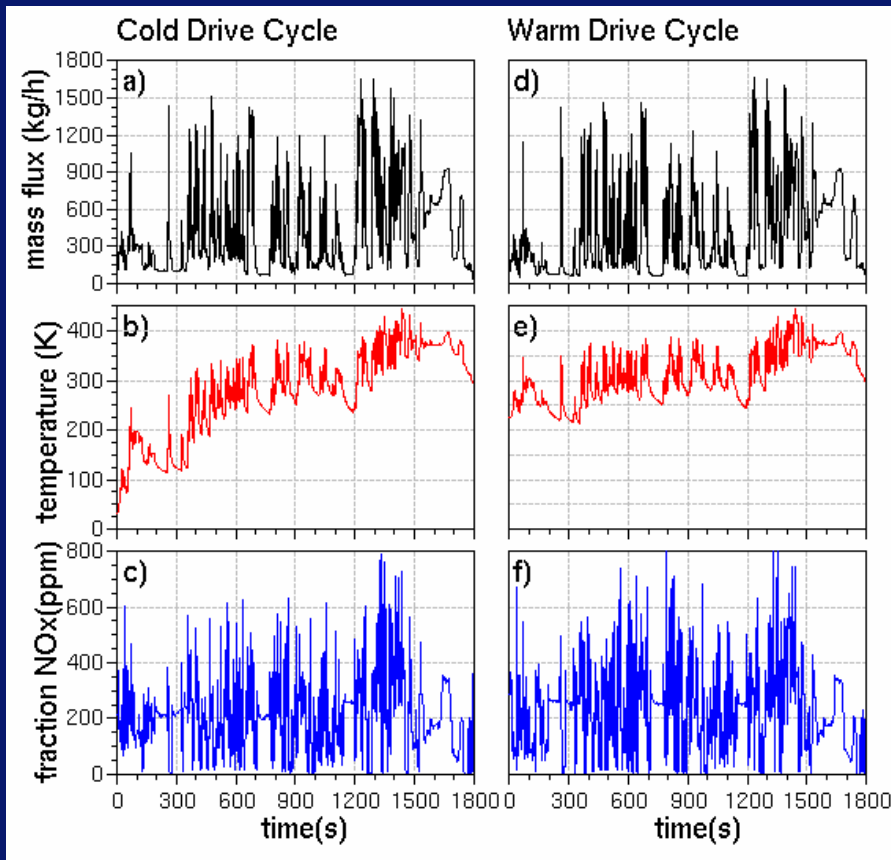


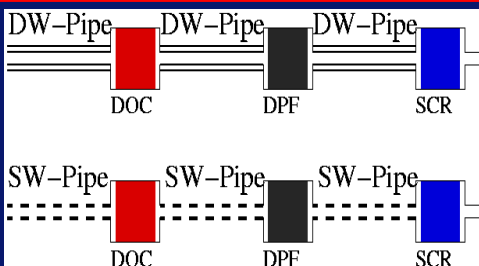
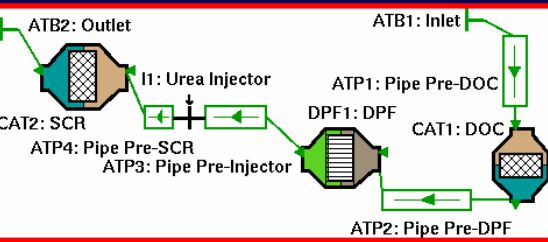
▪ Inlet Conditions:

- Engine Row Emissions for a WHTC given for **cold** and **warm** engine conditions

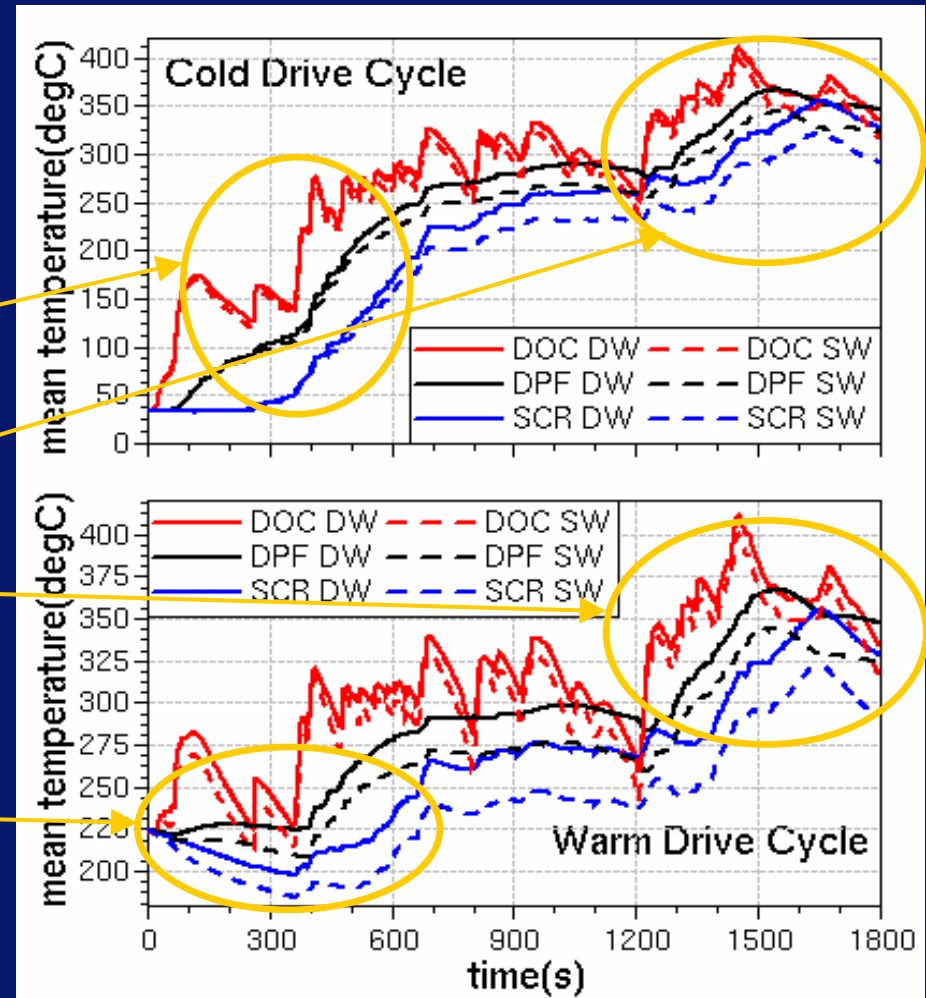
▪ Outlet Conditions:

- Constant ambient back pressure



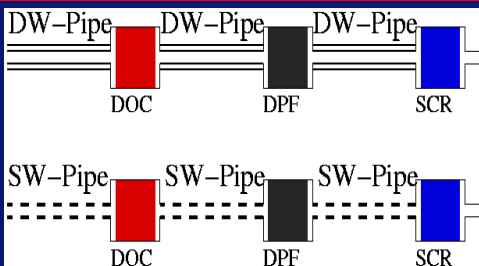
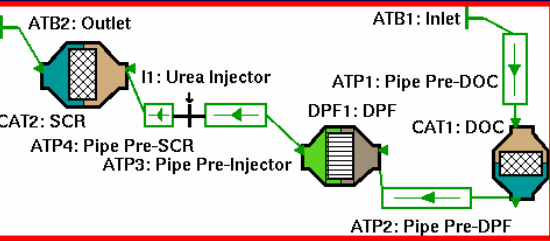


Mean DOC/DPF/SCR temperatures during cold and warm WHTC

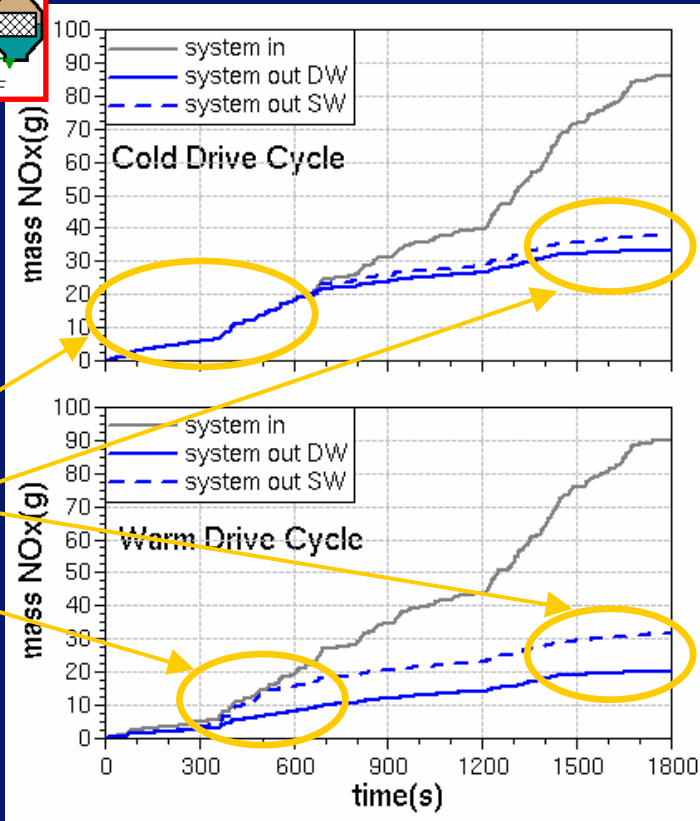


- **Heat-up phase:**
 - Small impact of pipe insulation
- **High-load phase:**
 - Dual-wall insulation shows higher temperatures
- **Low-load phase:**
 - Dual-wall insulation holds SCR operating temperature

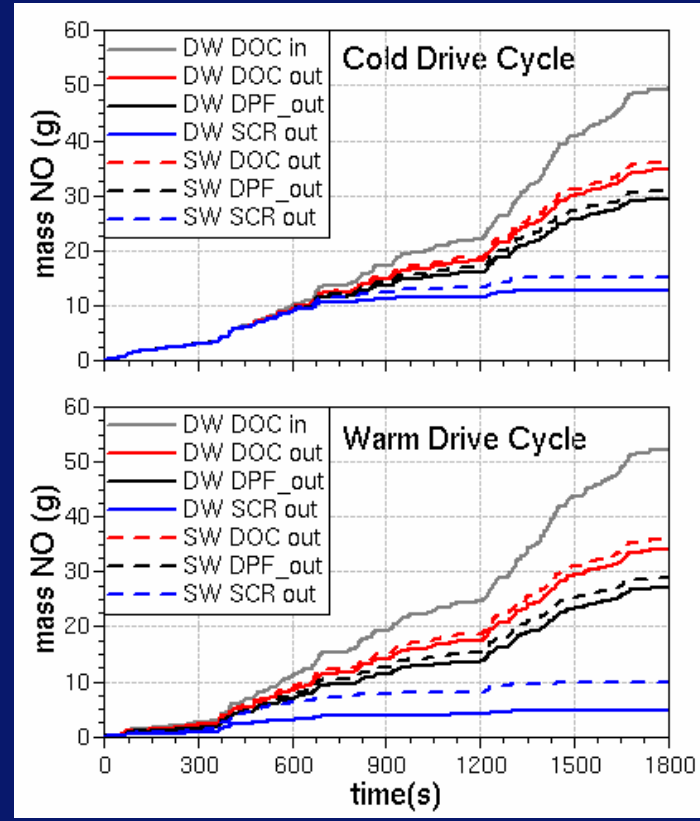
WHTC Simulation, Pipe Insulation Study II



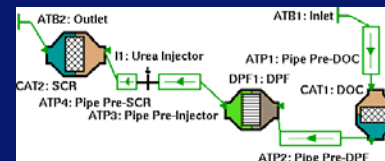
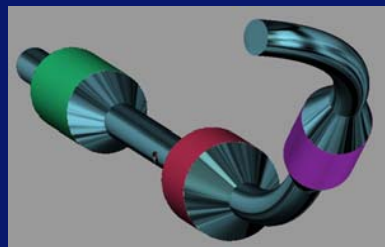
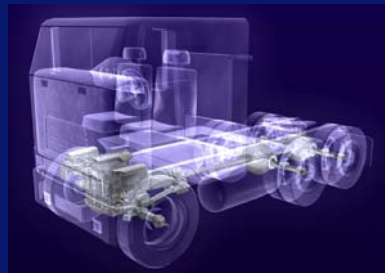
Overall NOx-emissions



Overall NO-emissions



- Heat-up phase
- High-load phase
- Low-load phase



- Demonstration of a 1D/3D aftertreatment system simulation framework by the example of a heavy-duty application
 - All components are pre-calibrated with experimental data
 - BOOST is used to investigate the overall system is investigated in 1D
 - FIRE is used to perform 3D detail simulations
- Sufficient modeling depth of all components is essential
- Simulation approach can be used for various system configurations