Mechanism Development for the Simulation of LNT Lean/Rich Cycling

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Develop an elementary surface reaction mechanism, complete with values for the kinetic parameters, that accounts for the observed product distribution from a lean NOx trap during both steady state and cyclical operation and under various conditions of temperature and inlet gas composition.







- Assemble tentative mechanisms for both precious metal (regeneration) and oxide (storage) sites, using reactions from literature together with additional hypothesized steps.
- Infer kinetic parameters for regeneration mechanism by matching product distributions from steady flow temperature ramp experiments done at ORNL.
 - Use Chemkin PLUG code to simulate (pseudo-) steady flow of reactant mixture through a catalyst monolith channel; temporarily discard storage mechanism.
 - Use Sandia APPSPACK code to carry out optimization.
 - Apply thermodynamic constraints to kinetic parameters in order to ensure complete consistency.



Basic approach (continued)

- Infer kinetic parameters for storage mechanism by matching product distributions from cycling experiments done at ORNL.
 - Use new Chemkin-based transient plug flow code to simulate inherently unsteady storage/regeneration processes.
 - Incorporate thermodynamic constraints on kinetic parameters in storage mechanism.
 - Use regeneration parameters previously determined (ideally) or allow adjustments and reconsider temperature ramp data.



- Formulated and implemented a complete set of thermodynamic constraints (all reactions treated as reversible with mass action kinetics).
- Completed construction of regeneration mechanism and optimization of kinetic parameters (72 adjustable, 96 total).
- Implemented a rate constant cap in order to alleviate mathematical stiffness.
- Verified thermodynamic consistency of regeneration mechanism via comparison of kinetic (tube flow) and equilibrium calculations.





- Identified several instances of steady state multiplicity in simulations of temperature ramp experiments.
- Initiated simulation of complete storage/regeneration cycles with combined mechanism.





- 10 gas phase species: O2, NO, NO2, CO, H2, CO2, N2, H2O, N2O, NH3
- 13 surface species on precious metal (nominally platinum) sites: *(PT), O(PT), NO(PT), NO2(PT), CO(PT), H(PT), N(PT), OH(PT), H2O(PT), NH(PT), NH2(PT), NCO(PT), NH3(PT)
- No homogeneous gas phase reactions
- 24 surface reactions, all of them reversible (in principle; five are found to be effectively irreversible)



The reaction set includes many adsorption/ desorptions (some dissociative) ...

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O2 + 2 * (PT) = 2O(PT)NO + *(PT) = NO(PT)NO2 + *(PT) = NO2(PT)CO + *(PT) = CO(PT)H2 + 2 * (PT) = 2H(PT)H2O + *(PT) = H2O(PT)NH3 + *(PT) = NH3(PT)2N(PT) = N2 + 2 * (PT)CO(PT) + O(PT) = CO2 + 2 * (PT)







NO2(PT) + *(PT) = NO(PT) + O(PT)NO(PT) + *(PT) = N(PT) + O(PT)H2O(PT) + *(PT) = H(PT) + OH(PT)OH(PT) + *(PT) = H(PT) + O(PT)NH(PT) + *(PT) = N(PT) + H(PT)NH2(PT) + *(PT) = NH(PT) + H(PT)NH3(PT) + *(PT) = NH2(PT) + H(PT)



Indirect reduction with CO can take place via two distinct pathways.

Hydrogen production via a water-gas shift reaction:

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H2O(PT) + CO(PT) = 2H(PT) + CO2
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Reaction of water with an isocyanate intermediate:

N(PT) + CO = NCO(PT)

NCO(PT) + H2O(PT) = NH2(PT) + CO2 + *(PT)







The remaining reactions can be categorized as atom transfers.

N2O + H(PT) = N2 + OH(PT)2NO(PT) = N2O + O(PT) + *(PT)NO2(PT) + CO(PT) = NO(PT) + CO2 + *(PT)NO(PT) + NH2(PT) = N2O + 2H(PT)

NH3(PT) + O(PT) = NH2(PT) + OH(PT)

Recap of steady flow experiments (ORNL)

- 21 separate runs with inlet compositions involving NO/H2, NO/CO, NO2/H2, NO2/CO, N2O/H2, N2O/CO, NH3/O2, NH3/NO, NH3, H2, or CO
- 5% H2O, 5% CO2, N2 carrier gas in all runs
- Temperature ramped from below 100 C to 500 C at 5 C/min
- Space velocity 100,000/hr
- Commercially available Umicore GDI LNT catalyst
- Chemiluminescent analyzers for NO and total NOx; FTIR for CO, NH3, and N2O; net N2 by difference



For a stoichiometric NO/H2 feed, nearly all features are reproduced accurately.



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For NO with excess H2, the onset temperature for NH3 formation is now reproduced quite well.







Reduction of NO2 by H2 is now simulated significantly better than before.







For 1:10 NO2/CO, the observed two-step drop in CO is mostly smoothed out by the model.

Simulation of steady flow temperature sweep experiment for 1:10 NO₂/CO 6000 concentration of N-containing species (ppm) Outlet mole fraction of N-containing species 0.006 500 CO NH 5 10⁻⁴ 5000 0.005 4000 (bbm) 2000 concentration (bbm) Outlet mole fraction of CO 400 NO 4 10-4 NO 0.004 NO2 300 - N2O 3 10-4 - NH3 0.003 — N2 (net) 200 2 10-4 0.002 CO 1 10-4 100 0.001 1000 N₂O N2 0.000 0 🞜 500 100 200 300 400 500 200 400 100 300 Temperature (C) catalyst temperature (°C) CO





For reduction of N2O with a large excess of H2, the model predicts some NH3 formation.



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In direct oxidation of NH3 by O2, production of N2O tends to be seriously underpredicted.







Oxidation of NH3 by a large excess of O2 is handled better, but NO appears too early.







Thermodynamic consistency has been verified via infinite residence time tube flow simulations.

Verification of thermodynamic consistency of regeneration mechanism using 500 ppm NH3 and 1500 ppm O2 (N2 chemistry suppressed)





Transient simulations confirm that the temperature ramps can *generally* be treated as pseudo-steady.

pseudo-steady

transient

ORNL





The complexity of the mechanism causes multiple steady states to occur locally, generally at low T.

Pseudo-steady simulation of steady flow temperature sweep experiment for 1:1 NO/CO





Fully transient simulations show local nonpseudo-steady behavior and hysteresis.

Transient and pseudo-steady simulations of steady flow temperature sweep experiment for 1:1 NO/CO









NO2(PT) + *(BAO) = NO2(BAO) + *(PT)

NO2 + CO3(BAO) = NO3(BAO) + CO2

NO + CO3(BAO) = NO2(BAO) + CO2

CO2 + O(BAO) = CO3(BAO)

NO2 + O(BAO) = NO3(BAO)

NO + O(BAO) = NO2(BAO)

O2 + 2 *(BAO) = 2O(BAO)

NO2 + NO2(BAO) = NO + NO3(BAO)

NO2 + *(BAO) = NO2(BAO)

The regeneration mechanism has been augmented with reactions occurring on storage sites.

Preliminary cycle simulations with the combined mechanism show the correct qualitative behavior.



Long cycle test on Umicore catalyst at 200 C and 30000/hr space velocity;

15 min lean (300 ppm NO, 10% O2), 10 min rich (625 ppm CO, 375 ppm H2)



- A robust, thermodynamically consistent mechanism for LNT regeneration has been developed.
- The mechanism tends to underestimate N2O production during NH3 oxidation and overestimate NH3 production during N2O reduction.
- Multiple steady states can occur and appear to be the result of parallel paths for reduction of NOx by CO.
- The proposed storage mechanism seems promising, but much work on parameter estimation (at least) is needed.
- Eventually, companion mechanisms for reduction by hydrocarbons and for sulfation/desulfation will be required.

