Microkinetic Modeling of Lean NOx Trap Storage/Regeneration and Sulfation/Desulfation

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- Overall project goal: Obtain the fundamental surface chemistry knowledge needed for the design and optimal utilization of NOx trap catalysts, thereby helping to speed the widespread adoption of this technology.
- Specific objective: Develop an elementary surface reaction mechanism, complete with values for the kinetic parameters, that accounts for the observed product distribution from a benchmark lean NOx trap (LNT) during both normal cyclical operation and hightemperature desulfation, allowing for variations in both temperature and inlet gas composition.





- Assemble tentative reaction sets for precious metal (catalytic), baria (NOx storage), and ceria (oxygen storage) sites.
- Infer kinetic parameters for precious metal sites by matching product distributions from steady flow experiments done at ORNL.
 - Use Chemkin plug flow code to simulate flow of reactant mixture through a catalyst monolith channel.
 - Use Sandia APPSPACK code to find kinetic parameters by optimizing overall fit to experimental data.
 - Apply thermodynamic constraints during fitting procedure in order to ensure complete consistency.
- Infer kinetic parameters for baria and ceria sites by matching product distributions from long cycle experiments.
 - Use transient plug flow code with allowance for radial mass transfer.
- Augment all three sub-mechanisms with reactions involving sulfurcontaining species, and estimate parameters from sulfation and desulfation runs.



Storage mechanism

- The mechanism describing chemistry on the baria and ceria sites involves nine new chemical species.
 - On baria: V(BAO), NO2(BAO), CO3(BAO), NO3(BAO), O(BAO), (OH)2(BAO), BA(NO3)2 ("bulk" nitrate)
 - On ceria: V(CERIA), O(CERIA)
- Seven reversible reactions account for NOx storage on baria sites:
 - O2 + 2V(BAO) = 2O(BAO)
 - NO2 + O(BAO) = NO3(BAO)
 - NO2 + NO2(BAO) = NO + NO3(BAO)
 - NO2 + CO3(BAO) = NO3(BAO) + CO2
 - (OH)2(BAO) + NO2 = NO3(BAO) + H2O
 - (OH)2(BAO) + CO2 = CO3(BAO) + H2O
 - NO2(BAO) + O(BAO) = NO3(BAO) + V(BAO)



Storage mechanism (continued)

- Three reactions describe formation of "bulk" nitrate:
 - 2NO3(BAO) = BA(NO3)2 + O(BAO)
 - NO3(BAO) + NO2 = BA(NO3)2
 - NO3(BAO) + NO2(BAO) = BA(NO3)2 + V(BAO)
- There are five spillover reactions (involving species on both BAO and PT):
 - NO2(PT) + V(BAO) = NO2(BAO) + V(PT)
 - NO3(BAO) + H(PT) = NO2(BAO) + OH(PT)
 - NO3(BAO) + CO(PT) = NO2(BAO) + CO2 + V(PT)
 - BA(NO3)2 + H(PT) = NO3(BAO) + OH(PT) + NO
 - BA(NO3)2 + CO(PT) = NO3(BAO) + CO2 + V(PT) + NO
- Oxygen storage on ceria is described by just one simple reaction:
 - O2 + 2V(CERIA) = 2O(CERIA)
- These reactions are combined with the precious metal mechanism and used with a transient plug flow code (including radial mass transfer resistance) to simulate complete storage/regeneration cycles.



Simulation vs. experiment at 200 C

- Simulation of NOx storage, release, and reduction (i.e., a complete storage/regeneration cycle) at 200 C is basically successful.
 - Artificially long cycle time is used to allow resolution of transients.
 - Feed gas contains 288 ppm NO and 10% O2 during storage phase, 625 ppm CO and 375 ppm H2 during regeneration phase.
 - Principal failures are underprediction of N2O and overprediction of NO during early part of regeneration.



Simulation vs. experiment at 300 C

- The simulation at 300 C is likewise mostly successful but with some noticeable imperfections.
 - Predicted NO peak following the onset of regeneration is not observed experimentally, but predicted slip of total NOx is not far off.
 - Timing of NH3 spike is reproduced accurately, but peak is too high and narrow.
 - In this case, N2O production is simulated fairly well.



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Simulation vs. experiment at 400 C

- Simulation of cycle at 400 C appears to be less demanding (presumably dominated by equilibrium) and is correct in most respects.
 - Falloff in NO2 at onset of regeneration is somewhat too rapid.
 - Well-known NO puff is reproduced very well.
 - Once again, timing of NH3 pulse (quite small here) is correctly reproduced.



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Axial profiles — NH3 as reduction intermediate

- The oft-proposed role of NH3 as an intermediate in the reduction of released NOx is consistent with the simulations.
 - Near the leading edge of the unregenerated zone, excess reductant converts desorbed NOx to NH3.
 - As reductant is depleted, NH3 is oxidized by desorbed NOx and O2.
 - After NH3 and original reductant have been consumed, stored NOx and O2 desorb unhindered and exit the reactor.



Evolution of storage phase compositions

- The simulations predict the changes in the storage phase composition over the course of a cycle.
 - During NOx storage, carbonates are (partially) replaced by nitrites and nitrates.
 - At both 300 C and 400 C, but not 200 C, the baria phase is completely cleansed of NOx during regeneration.







Spatially-averaged concentrations of storage phase species during long storage/regeneration cycle at 300 C



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Predictions of short cycle behavior

- The mechanism inferred from long cycle experiments can be used to predict behavior during a short (60 s lean/5 s rich) cycle.
 - First cycle begins with a completely clean surface.
 - Simulation is isothermal (questionable) and now uses argon as the bath gas.
 - Essentially no NOx escapes during first two lean periods.
 - NH3 production during regeneration is attributable largely to CO.







Sulfation/desulfation mechanism

- A mechanism describing the effects of sulfur compounds on all aspects of the chemistry has been developed but not yet finalized.
 - 7 new species on PT: SO2(PT), SO3(PT), H2S(PT), SO(PT), S(PT), HS(PT), COS(PT)
 - 1 new species each on baria and ceria: SO4(BAO), SO4(CERIA)
 - 18 new reactions (tentatively) on PT, accounting for SO2 oxidation during lean phase and reduction of SO3 to H2S during desulfation
 - 7 new reactions on baria and 1 on ceria, accounting for sulfate formation
- The overall mechanism has been used to simulate loss of NOx storage capacity during normal cycling and evolution of products during high-temperature desulfation.
- The mechanism is currently too complex for all parameters to be extracted from experimental data; some reactions are inoperative.



Simulation of long cycle with SO2 in feed

- Simulations of long cycles with SO2 in the lean-phase feed can be carried out to check the mechanism for qualitatively correct behavior.
 - 10 ppm SO2 is added to the 288 ppm NO and 10% O2 already present.
 - Spatially-averaged sulfate level rises linearly during storage (no SO2 slip) and remains constant during regeneration (no desulfation).







Spatially-averaged concentrations of storage phase species

10 ppm SO2 added

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Time (s)

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Spatial profile of sulfation

- The simulations are also consistent with the observation that sulfation of the NOx storage sites tends to be concentrated at the front of the reactor.
 - At ordinary cycle temperatures, sulfate permanently displaces both nitrite and carbonate.



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Preliminary simulation of desulfation

- Simulation of desulfation by temperature-programmed reduction is in reasonable qualitative agreement with experiment.
 - After sulfation at 300 C, temperature ramped at 5 C/min under 0.1% H2.
 - Experimental concentrations are in arbitrary units (i.e., magnitude unspecified).
 - Simulated peaks should be shifted and reshaped by adjusting kinetic constants.



Experiment (ORNL)

Simulation

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Future directions

- Complete evaluation of kinetic parameters describing sulfur chemistry on precious metal, baria, and ceria sites.
 - Reduce mechanism by discarding reactions if insufficient data exist to distinguish between parallel pathways.
- Augment mechanism with reactions accounting for reductants other than CO and H2.
 - Unburned and/or partially burned hydrocarbons may play a role, depending on mode of operation.
 - Addition of reforming reactions should provide a bridge between hydrocarbon reductants and existing mechanism.
- Develop computational tools to handle fully nonisothermal simulations.
 - Current code uses imposed (e.g., experimentally determined) spatial and temporal variations in temperature.
 - The capability to compute temperatures internally is obviously desirable, especially for short cycle simulations.



Conclusions

- We have attempted to construct a complete mechanism for LNT operation (including sulfation/desulfation) which involves (a) elementary reactions obeying mass-action kinetics, (b) full and rigorous thermodynamic consistency, and (c) both H2 and CO as reductants.
- We have used a three-tiered approach to developing the mechanism and benchmarking it against experimental data.
 - A mechanism for precious metal sites, based on steady flow experiments, has been completed and published.
 - A mechanism for NOx and O2 storage sites, based on long cycle experiments, has been tentatively completed, although future modifications are possible.
 - A supplemental mechanism for sulfur chemistry has been constructed, and preliminary parameter evaluation has been accomplished.
- A fourth tier, aimed at simulating the use of reductants other than H2 and CO, is to be started shortly.
- Observed shortcomings in the simulations may be due to defects in the mechanism or overly simplified modeling of the reactor (monolith channel) itself.



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