

Effect of Length on LNT Performance

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This work is undertaken to determine if/how monolith length affects LNT performance

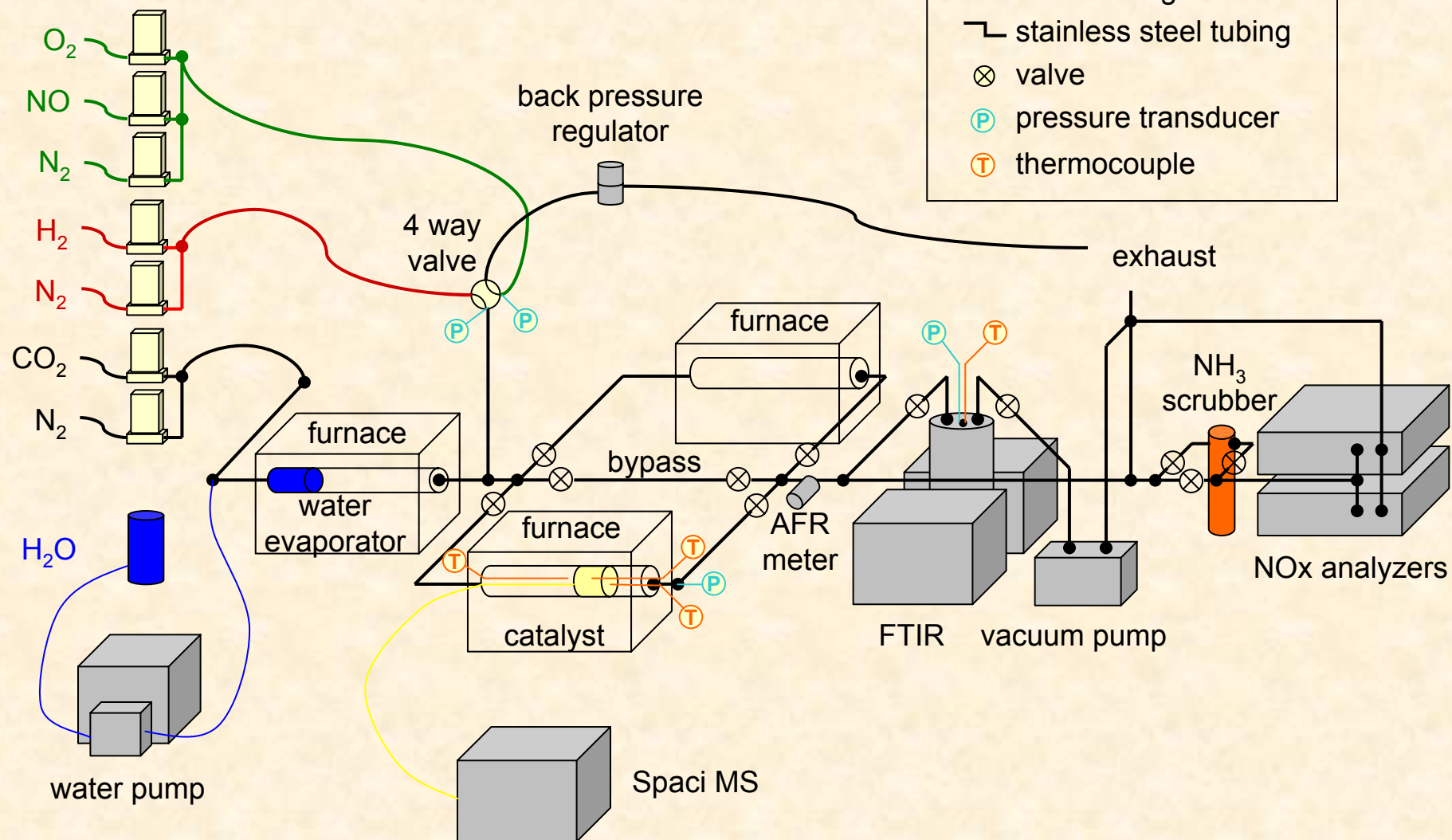
- **Conventional census rules out performance dependence on length at a given space velocity**
 - **Reacting system is governed by residence time (reciprocal of space velocity) and mass transfer coefficient**

$$-\frac{\partial C_A^*}{\partial z^*} - \tau k_{m,A} a_c (C_A^* - C_{As}^*) = \frac{\partial C_A^*}{\partial t^*} \quad C_A^* = 1 \quad \text{at } z^*=0 \quad \frac{\partial C_A^*}{\partial z^*} = 0 \quad \text{at } z^*=1$$

- **Mass transfer coefficient is constant in a fully-developed laminar flow**
- **Significant difference in LNT performance data are often obtained under the same conditions by different labs (cf. John Hoard, 8th CLEERS Workshop)**
 - **Different experimental catalyst sizes are used at different labs**
 - **No standard reactor size**
 - **Suspected as the culprit of LNT performance disparity**
- **Length effect issue needs to be addressed**
 - **To compare data from different sources**
 - **To develop commercial design criteria**
 - **To develop models**

Approach: evaluation of core samples using well-controlled bench reactor

mass flow controllers



Two LNTs of different formulation and physical properties were evaluated

- **SCONO_x**
 - EmeraChem LNT used in the power generating industry
 - 200 cpsi cordierite brick washcoated with Pt/K/ γ -Al₂O₃
- **Umicore**
 - Umicore GDI LNT used by CLEERS LNT Focus Group
 - 625 cpsi cordierite brick washcoated with Pt, Pd, Rh, Ba, CeO₂, ZrO₂, γ -Al₂O₃ and etc.

Samples of 7/8" OD and 1", 2" and 3" long were evaluated at $SV=30,000 \text{ h}^{-1}$ using long and short cycles

Long-cycle Experiments:

- **SCONO_x**

Mode	Time	Gas Composition
Lean	15 min	300 ppm NO, 10% O ₂ , 5% H ₂ O, 5% CO ₂ , balance N ₂
Rich	10 min	0.2% or 0.5% H₂ , 5% H ₂ O, 5% CO ₂ , balance N ₂

Temperatures: 200, 300 and 400°C

- **Umicore**

Mode	Time	Gas Composition
Lean	15 min	300 ppm NO, 10% O ₂ , 5% H ₂ O, 5% CO ₂ , balance N ₂
Rich	10 min	0.4% H₂ , 5% H ₂ O, 5% CO ₂ , balance N ₂

Temperatures: 230, 325 and 500°C

- **Gas Analysis:**

- NO/NO_x (chemiluminescence detectors)
- NO₂/N₂O/NH₃/CO/CO₂/H₂O (FTIR)

Samples of 7/8" OD and 1", 2" and 3" long were evaluated at $SV=30,000 \text{ h}^{-1}$ using long and short cycles

Short-cycle Experiments:

- **SCONO_x**

Mode	Time	Gas Composition
Lean	56 s	300 ppm NO, 10% O ₂ , 5% H ₂ O, 5% CO ₂ , balance N ₂
Rich	4 s	1% or 2% H₂ , 5% H ₂ O, 5% CO ₂ , balance N ₂

Temperatures: 200, 300 and 400°C

- **Umicore**

Mode	Time	Gas Composition
Lean	60 s	300 ppm NO, 10% O ₂ , 5% H ₂ O, 5% CO ₂ , balance N ₂
Rich	5 s	1.4% or 3.4% H₂ , 5% H ₂ O, 5% CO ₂ , balance N ₂

Temperatures: 230, 325 and 500°C

- **Gas Analysis:**

- NO/NO_x (chemiluminescence detectors)
- NO₂/N₂O/NH₃/CO/CO₂/H₂O (FTIR)
- H₂ (SpaciMS)

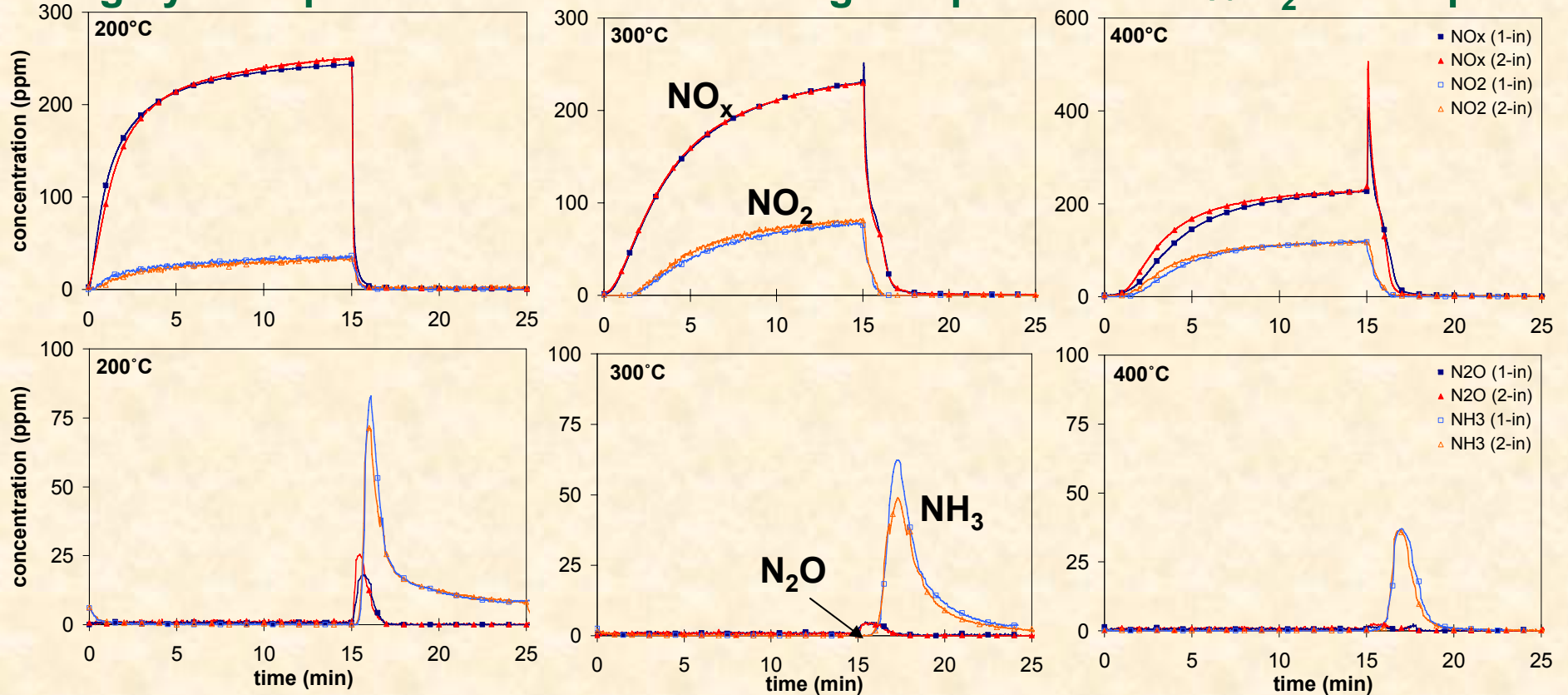
SCONO_x

Three “identical” 7/8” OD x 1” long cores were selected as building blocks

- **To evaluate and compare performance of 1”, 2” and 3” long samples**
- **Experimental artifacts needed to be addressed for meaningful comparison**
 - **Sample-to-sample variation**
 - **Effect of channel misalignment and “discontinuity” on catalyst performance**
 - **Develop “degreening” protocol for obtaining reproducible data of catalyst activity**

Performance of SCONO_x is not affected by sample's length in long-cycle experiments

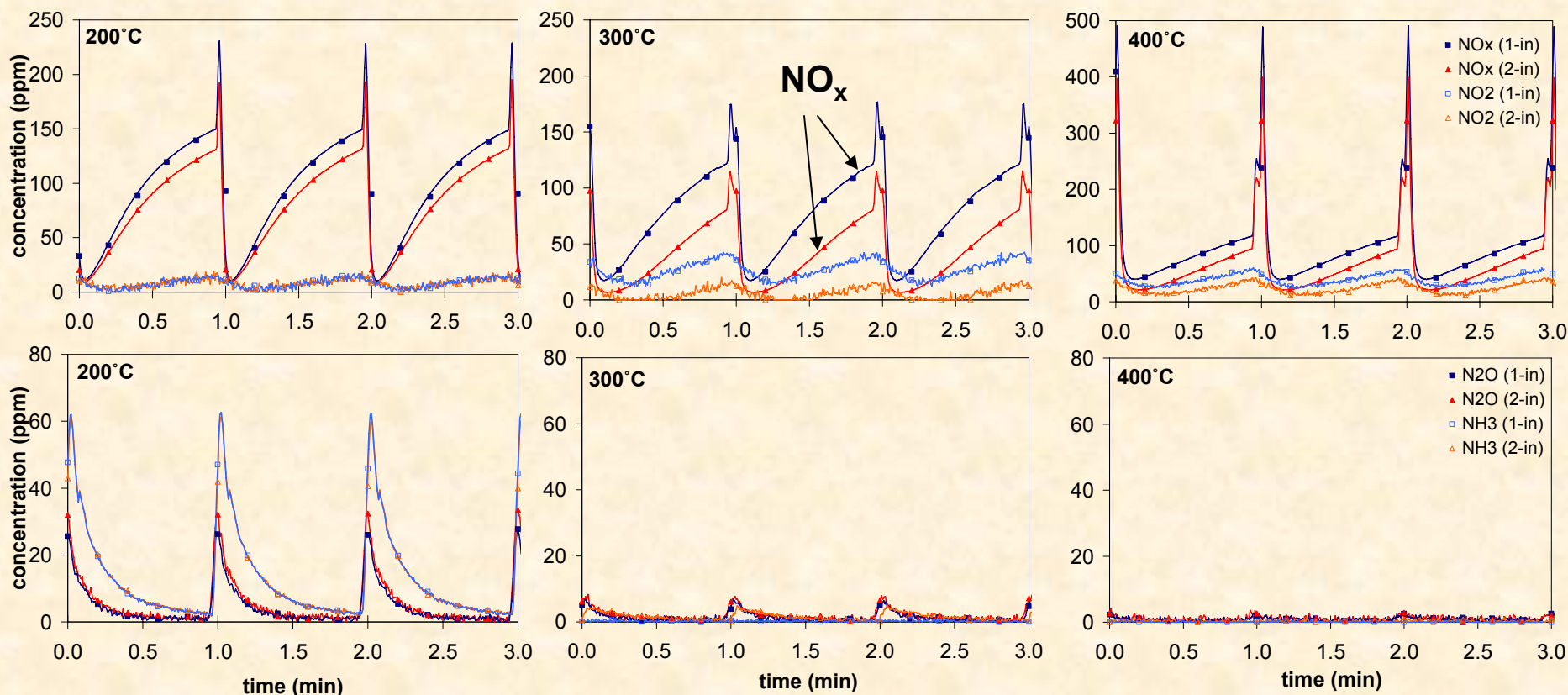
Long-cycle experiments in 1'' and 2'' long samples with 0.2% H₂ in rich phase



NO_x conversion efficiencies

Length \ T	200°C	300°C	400°C
1''	21.5%	36.0%	33.2%
2''	24.5%	36.5%	33.1%

Performance of SCONO_x is affected by sample's length in short-cycle experiments with partial regeneration (1% H₂)

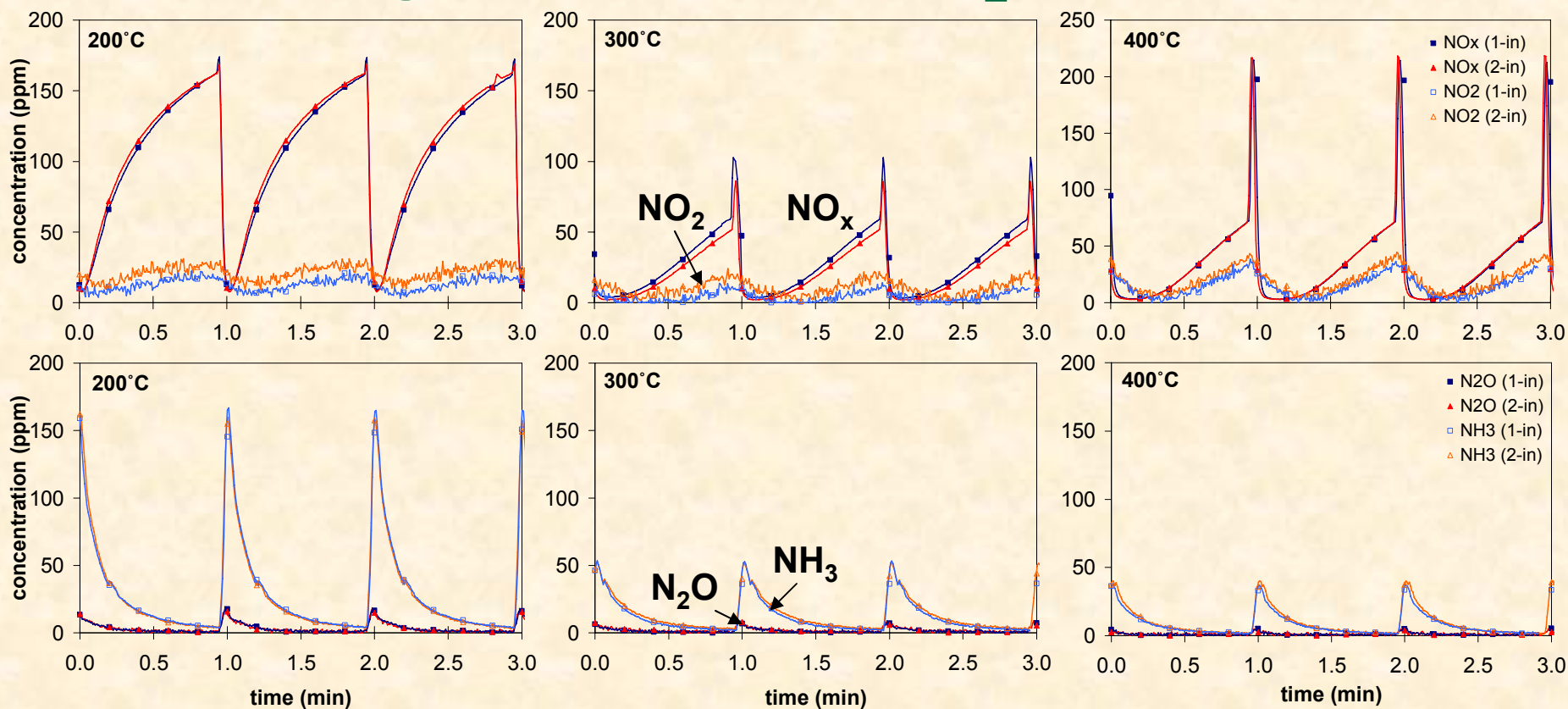


- Largest difference of 15% in NO_x conversion is at 300°C
- Longer the sample better the performance

NO_x conversion efficiencies

Length \ T	200°C	300°C	400°C
1"	61.1%	68.7%	61.1%
2"	67.4%	83.6%	73.8%

Performance of SCONO_x is not affected by sample's length in short-cycle experiments with full regeneration (2% H₂)

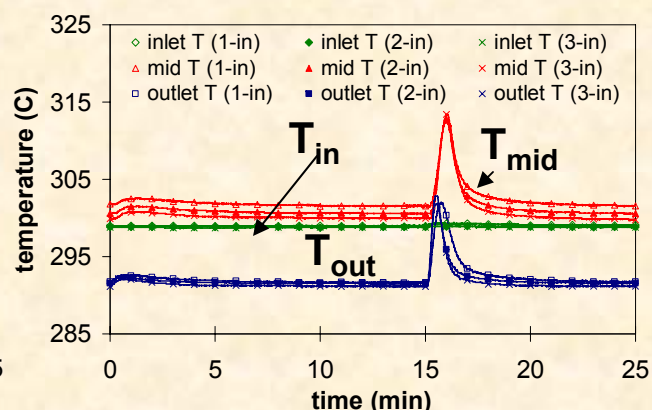
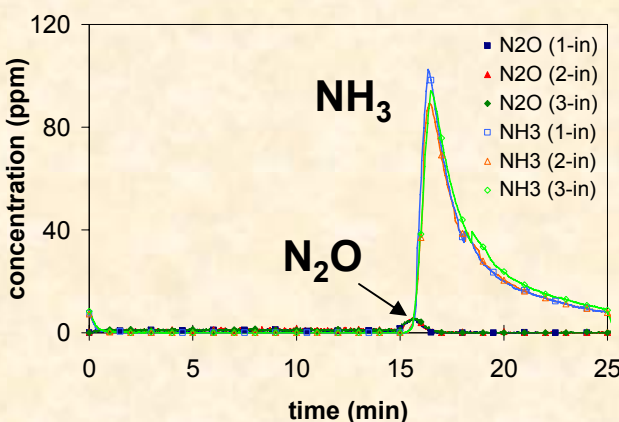
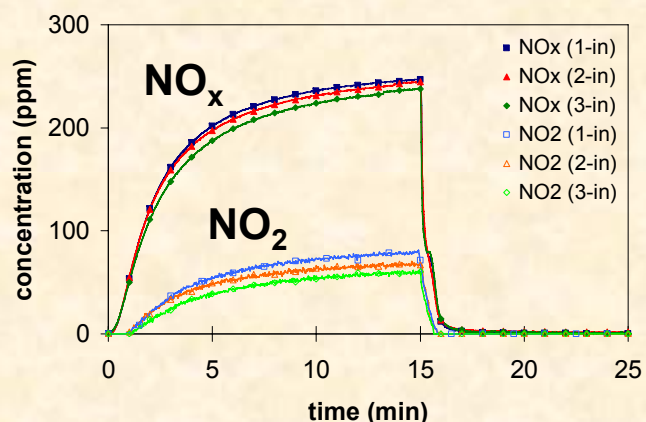


NO_x conversion efficiencies

Length \ T	200°C	300°C	400°C
1"	58.5%	89.2%	86.0%
2"	57.5%	91.0%	86.6%

Trend was further confirmed with 1", 2" and 3" long samples: performance in long cycling is not affected by sample's length

Long-cycle experiments in 1", 2" and 3" long samples at 300°C with 0.2% H₂ in rich phase

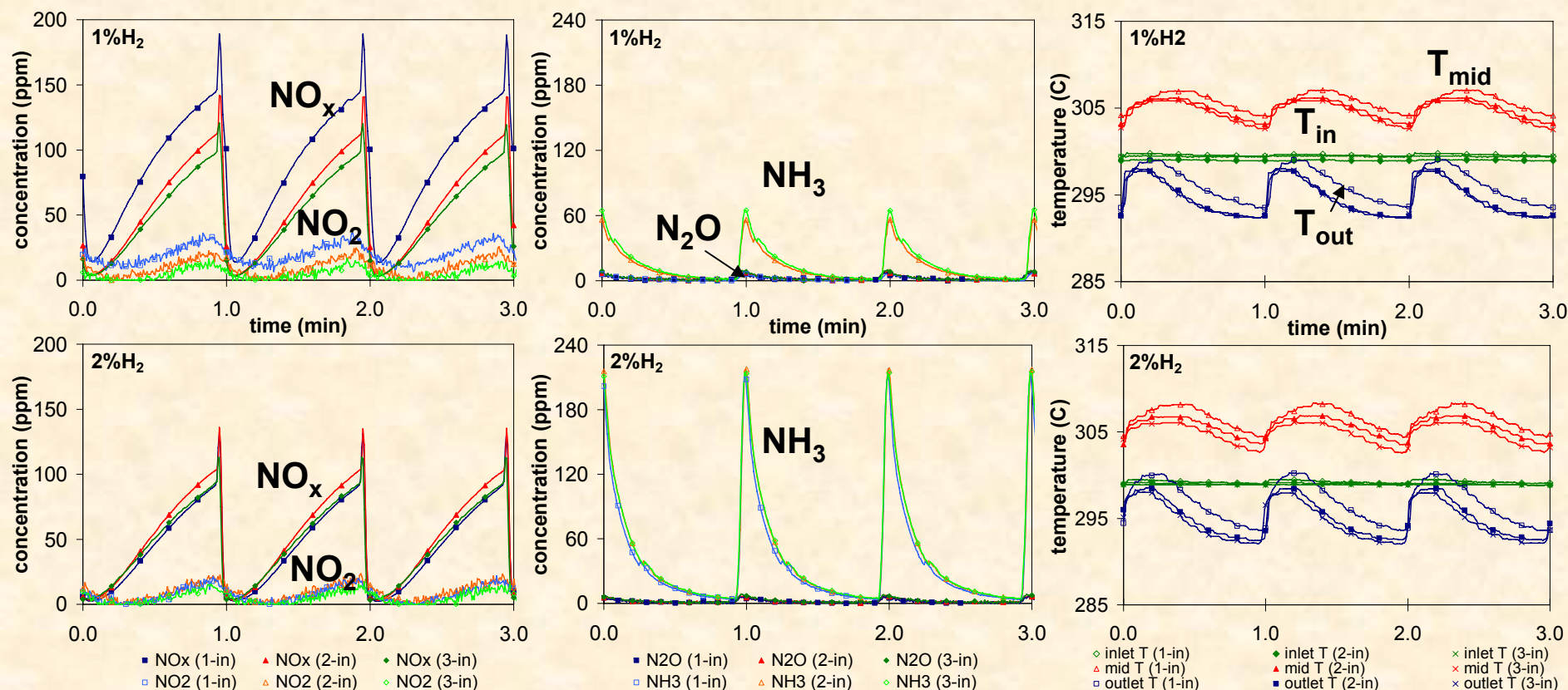


Observed difference is within experimental uncertainty

NOx conversion efficiencies

Length \ T	300°C
1"	25.4%
2"	26.4%
3"	29.1%

Trend was further confirmed with 1", 2" and 3" long samples: performance in short cycling is affected by sample's length with 1% but not with 2% H₂ at 300°C



With 1% H₂:
2" > 1" by 11%
3" ≈ 2"

NO_x conversion efficiencies

Length \ C	1% H ₂	2% H ₂
1"	65.7%	82.1%
2"	77.1%	79.5%
3"	80.5%	81.7%

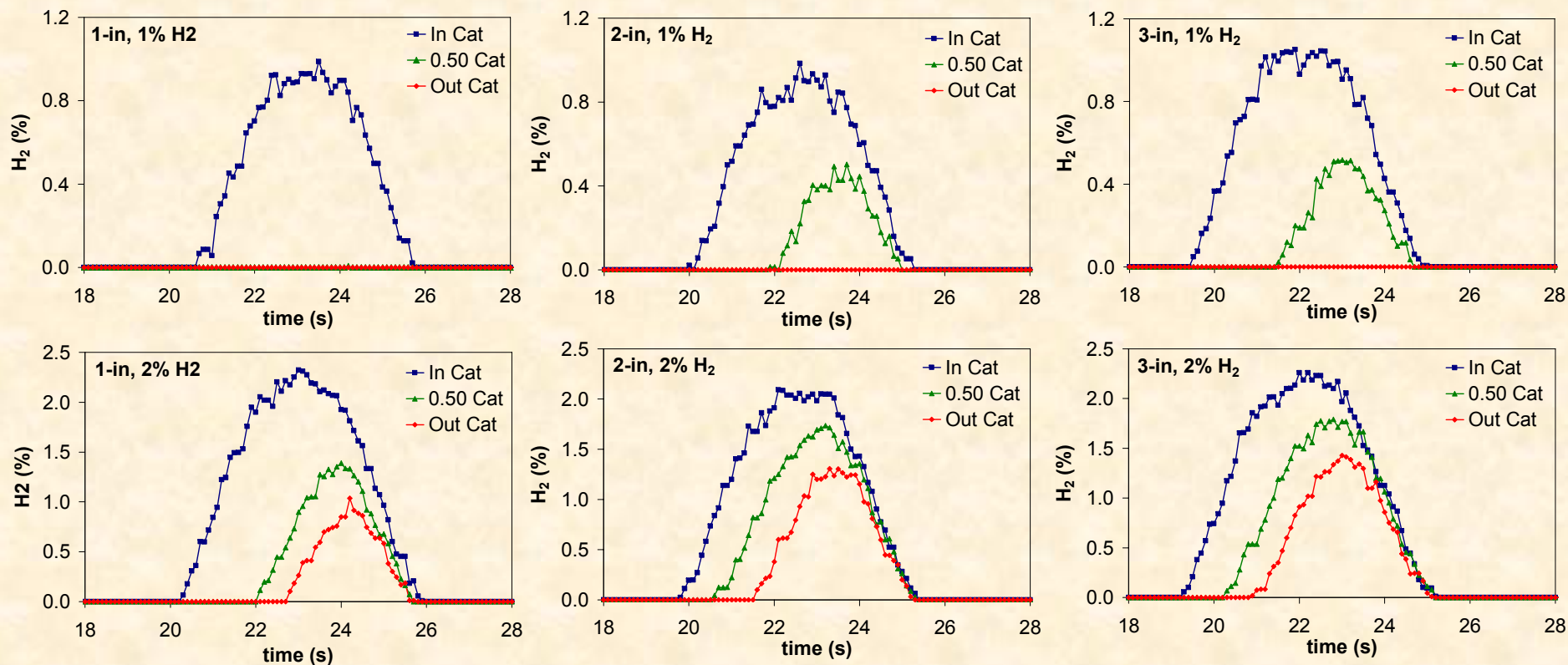
SCONO_x Performance vs. Length: Summary

- **Performance in short-cycle experiments with full regeneration (2% H₂) and in long-cycle experiments is not affected by monolith length**
3 in = 2 in = 1 in
- **Performance in short-cycle experiments with partial regeneration (1% H₂) is affected by monolith length**
2 in > 1 in & 3 in = 2 in
- **Little difference in temperature profiles is observed: negligible thermal effect**

H₂ Consumption Trends in
Short-Cycle Experiments at 300°C
SCONO_x
(measured with SpaciMS)

More H₂ is consumed in 1'' than in 2'' and 3'' long samples

Short-cycle experiments with 1% and 2% H₂ at 300°C

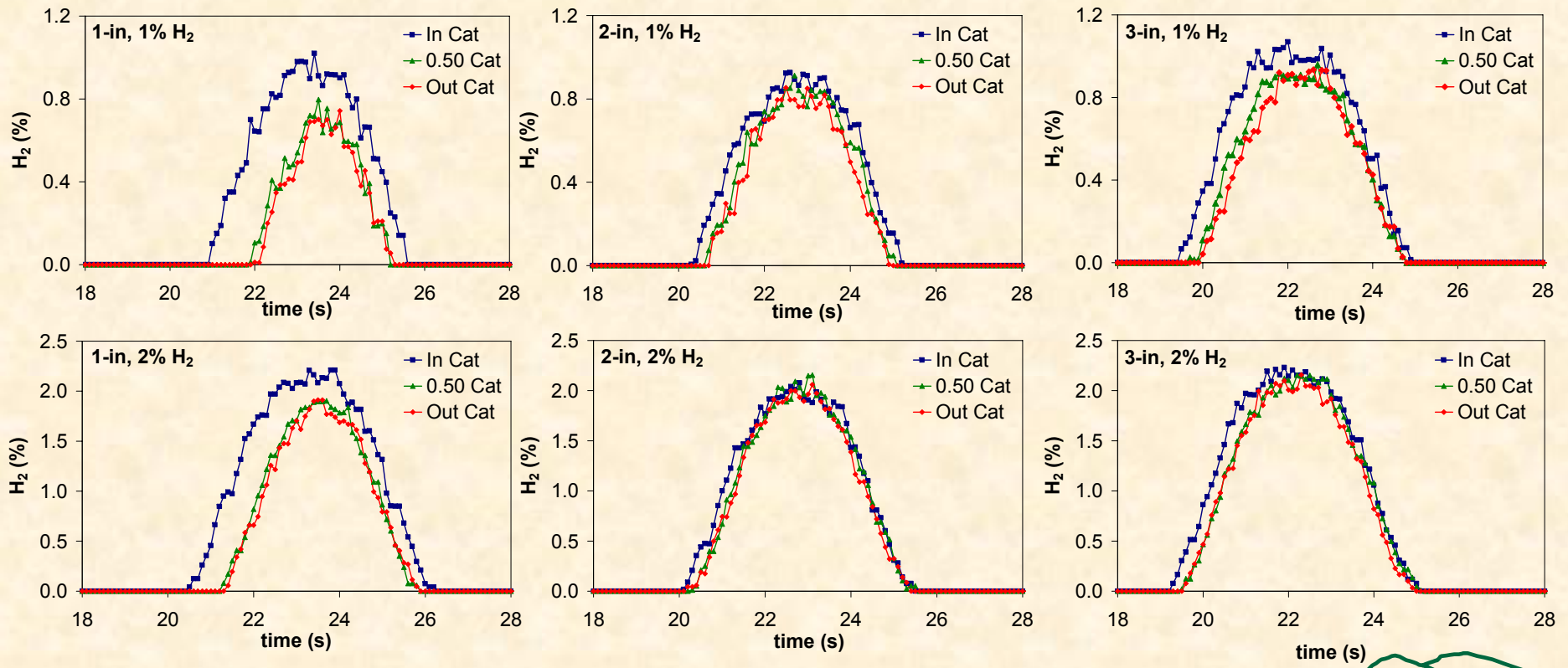


- With 1% H₂, 100% is consumed in first half of 1'' vs. 75% in 2'' and 3''
- With 2% H₂, 80% is consumed in 1'' vs. 60% in 2'' and 3''

Same trend in OSC experiments: more H₂ is consumed in 1'' than in 2'' and 3'' long samples

Short-cycle experiments without NO in the lean phase

Mode	Time	Gas Composition
Lean	56 s	0% NO, 10% O ₂ , 5% H ₂ O, 5% CO ₂ , balance N ₂
Rich	4 s	1% or 2% H₂ , 5% H ₂ O, 5% CO ₂ , balance N ₂

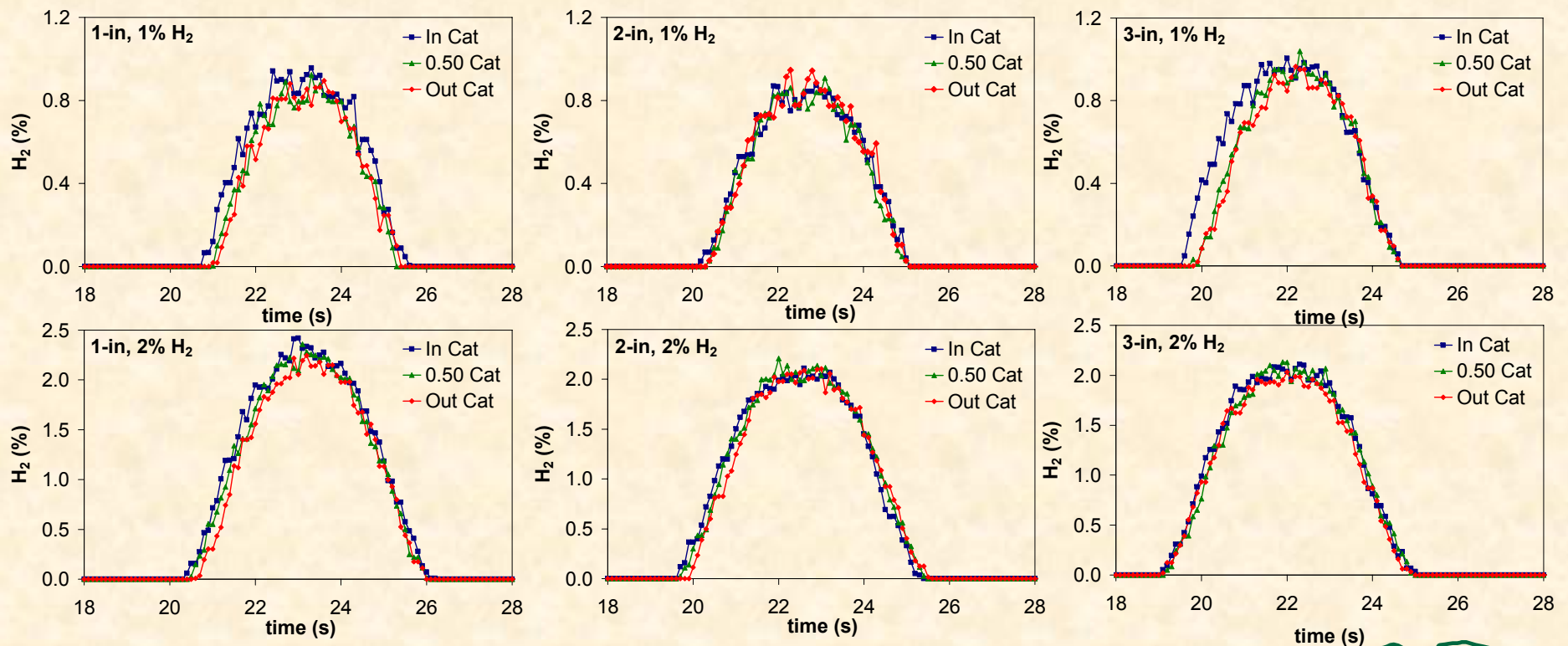


Lean/rich front back-mixing may contribute to significant reductant loss and in turn affects NO_x conversion efficiency

- **With 1% H_2 , 50% of H_2 is consumed in the front half of 1'' long sample compared to 18% in 2'' and 3''**
- **Different H_2 consumption in OSC experiments indicates other mechanisms for H_2 consumption might occur in addition to reaction with surface O_2**
 - **Catalytic reaction between H_2 and O_2 at the interface between the lean and rich phases; the extent of which depends on the degree of mixing at the lean/rich interface**
 - **Higher back-mixing \rightarrow higher H_2 consumption \rightarrow less amount of H_2 available for reducing $\text{NO}_x \rightarrow$ lower NO_x conversion**
 - **Similar H_2 consumption in 2'' and 3'' indicates lesser degree of back-mixing with increasing flow rate (at a fixed SV and catalyst diameter, i.e., gas velocity or flow rate increases with increasing length)**

Difference in H₂ consumption trends between 1", 2" and 3" disappears with neutral purge: evidence of different degree of back-mixing

Mode	Time	Gas Composition
Lean	56 s	0% NO, 10% O ₂ , 5% H ₂ O, 5% CO ₂ , balance N ₂
Purge	10 s	5% H ₂ O, 5% CO ₂ , balance N ₂
Rich	4 s	1% or 2% H₂ , 5% H ₂ O, 5% CO ₂ , balance N ₂



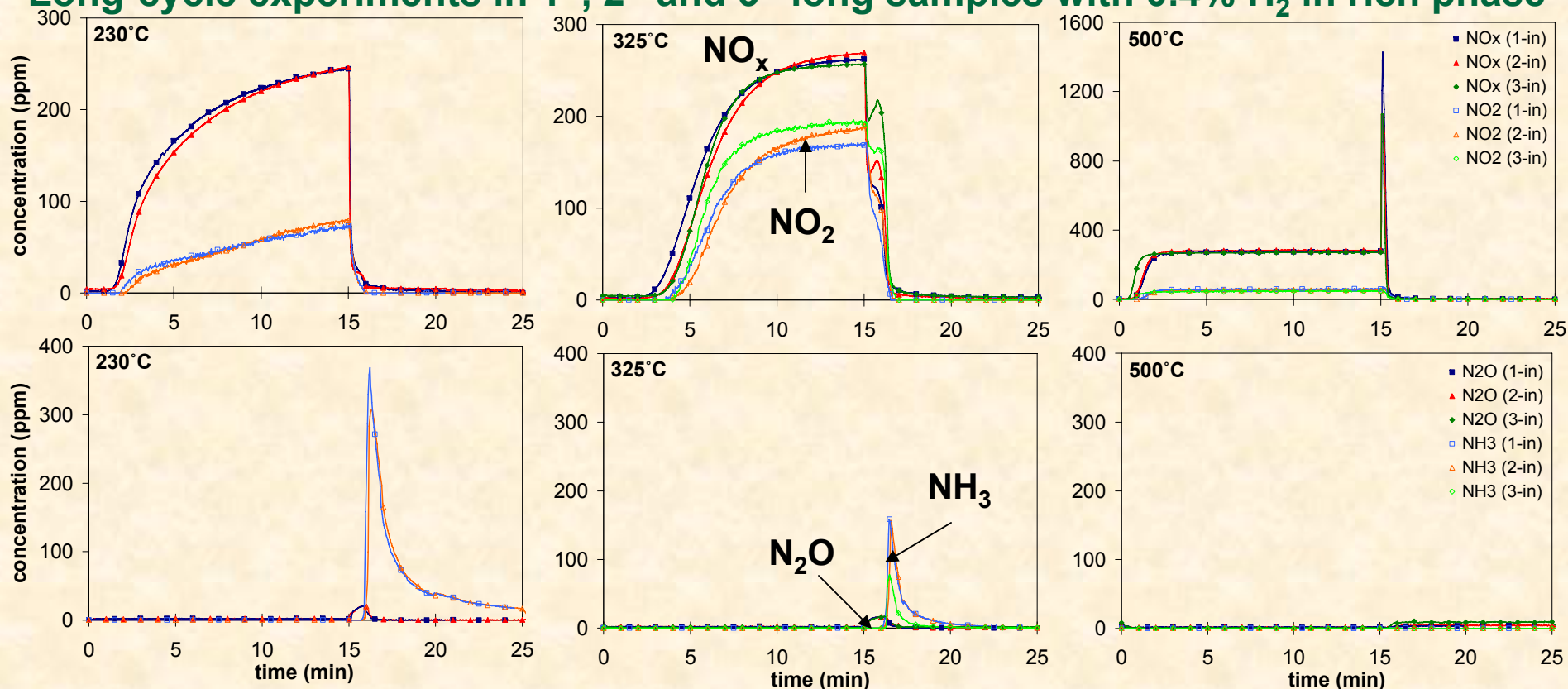
Back-mixing is responsible for differences in NO_x conversion between 1", 2" and 3" long samples as a result of H_2 loss

- In 1" long sample, ~35% of H_2 is consumed by the catalytic oxidation at the lean/rich interface, compared to ~ 10% in longer samples, resulting in a reduction of 15% in NO_x conversion in short-cycle experiments with 1% H_2
- If 2.5 moles of H_2 are required to reduce 1 mole of inlet NO , 25-30% less availability of H_2 would result in 10 to 14% decrease in NO_x conversion, which is consistent with experimental data
 - $\text{K}_2\text{CO}_3 + 2\text{NO} + 1.5\text{O}_2 \rightarrow 2\text{KNO}_3 + \text{CO}_2$
 - $2\text{KNO}_3 + 5\text{H}_2 + \text{CO}_2 \rightarrow \text{K}_2\text{CO}_3 + \text{N}_2 + 5\text{H}_2\text{O}$

Umicore

Performance of Umicore is not affected by sample's length in long-cycle experiments

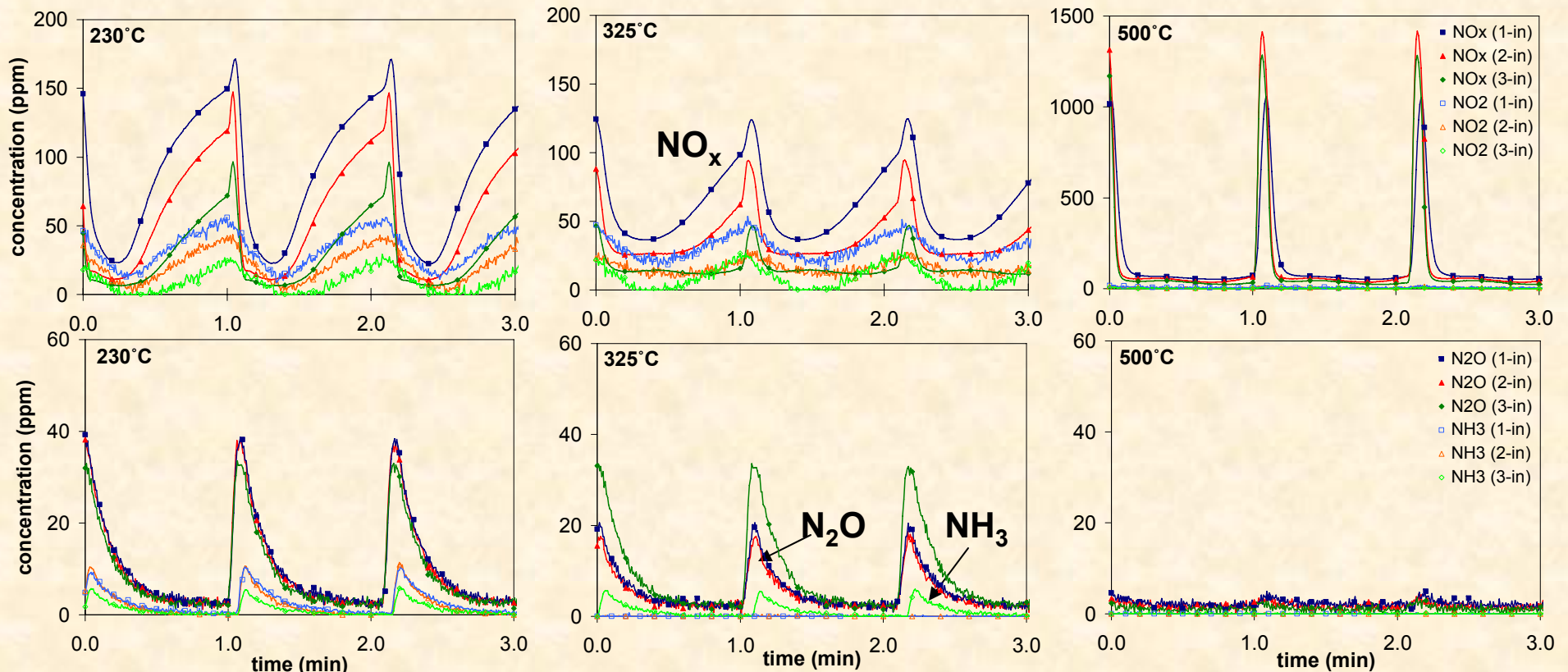
Long-cycle experiments in 1", 2" and 3" long samples with 0.4% H₂ in rich phase



NO_x conversion efficiencies

Length \ T	230°C	325°C	500°C
1"	36.6%	36.5%	1.6%
2"	40.7%	40.8%	1.9%
3"	--	35.8%	1.8%

Performance of Umicore is affected by sample's length in short-cycle experiments with partial regeneration (1.4% H₂)

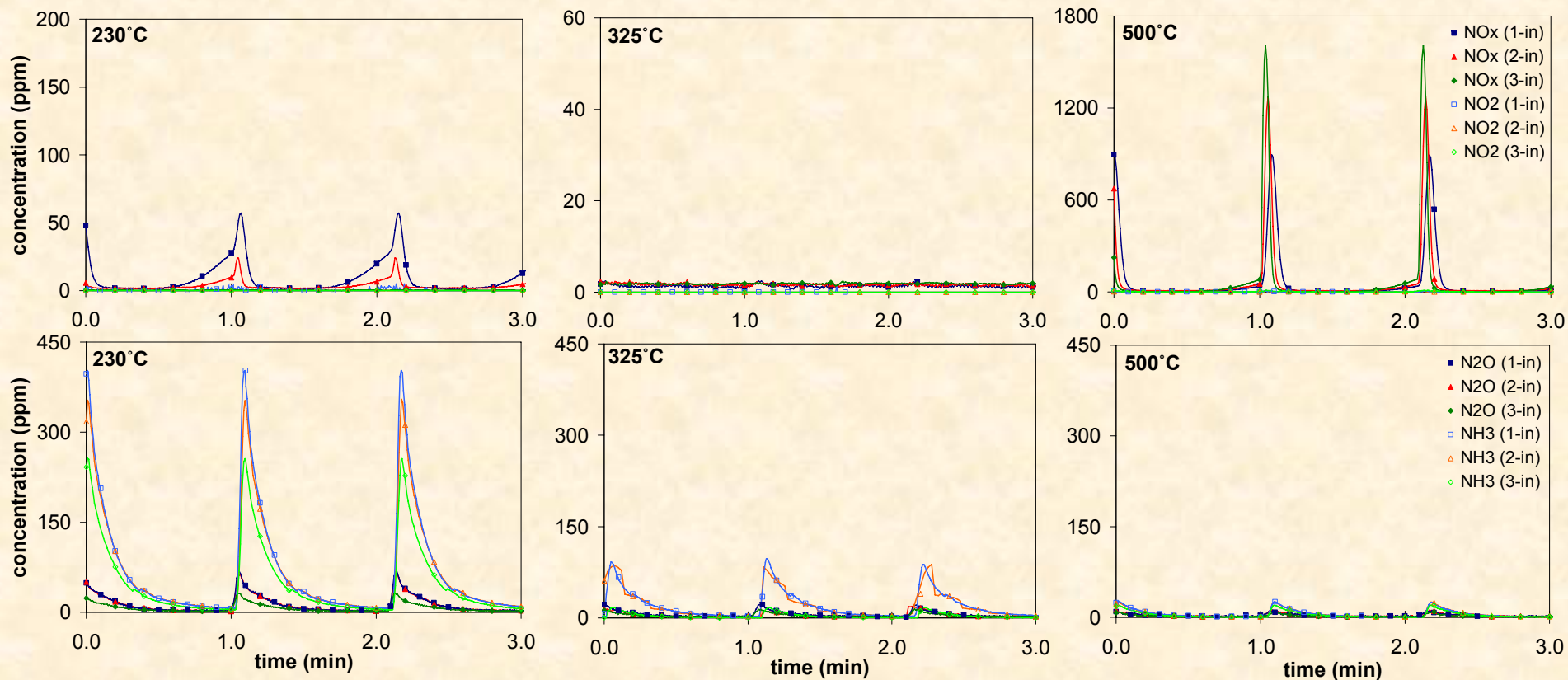


At 325°C
2" > 1" by 10%
3" > 2" by 8%

NOx conversion efficiencies

Length \ T	230°C	325°C	500°C
1"	64.3%	75.3%	43.0%
2"	76.9%	85.1%	45.1%
3"	86.4%	93.1%	49.1%

Performance of Umicore is not affected by sample's length in short-cycle experiments with full regeneration (3.4% H₂)



Length \ T	230°C	325°C	500°C
1''	96.0%	99.5%	72.9%
2''	98.5%	99.4%	71.3%
3''	99.8%	99.2%	62.9%

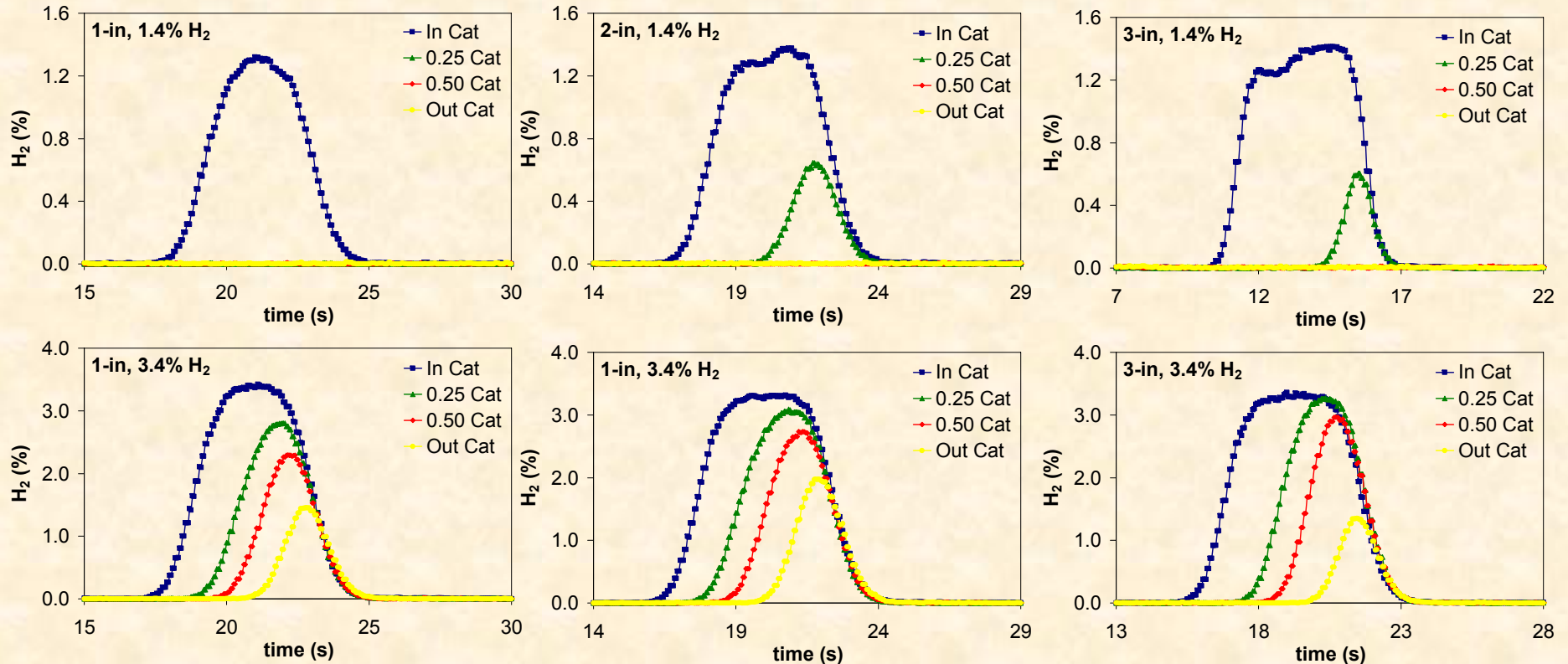
Umicore Performance vs. Length: Summary

- **Performance in short-cycle experiments with full regeneration (3.4% H₂) and in long-cycle experiments is not affected by monolith length as in the case of SCONO_x**
3 in = 2 in = 1 in
- **Performance in short-cycle experiments with partial regeneration (1.4% H₂) is affected by monolith length**
3 in > 2 in > 1 in
- **Little difference in temperature profiles is observed: negligible thermal effect**

H₂ Consumption Trends in
Short-Cycle Experiments
Umicore
(measured with SpaciMS)

More H₂ is consumed in shorter sample

Short-cycle experiments at 325°C with 1.4% & 3.4% H₂ in rich phase



- With 1.4% H₂, 100% is consumed in first quarter of 1'' vs. 77% in 2'' and 86% in 3''

Back-mixing is responsible for differences in NO_x conversion between 1", 2" and 3" long samples as a result of H_2 loss

- **Different slopes in catalyst's inlet H_2 profiles suggest different degree of lean/rich front back-mixing which may contribute to significant reductant loss**
- **Average inlet H_2 is different between samples**
 - 1.4%: 1.02%, 1.20% and 1.25% in 1", 2" and 3" long samples
 - 3.4%: 2.89%, 3.22% and 3.23% in 1", 2" and 3" long samples
 - Indicating H_2 consumption prior to the catalyst
- **Back-mixing depends on catalyst's length or linear velocity**

Theoretical explanation of back-mixing

- Back-mixing is attributed to axial diffusion of chemical species in gas mixture (transport = bulk flow + diffusion)
- Dimensionless form of fluid phase mole balance equation for each species for dispersion with reaction

$$\frac{D_a}{U_z L} \frac{\partial^2 C_A^*}{\partial z^{*2}} - \frac{\partial C_A^*}{\partial z^*} - \frac{L}{U_z} k_{m,A} a_c (C_A^* - C_{As}^*) = \frac{\partial C_A^*}{\partial t^*}$$
$$\left(-\frac{D_a}{U_z L} \frac{\partial C_A^*}{\partial z^*} + \frac{\partial C_A^*}{\partial z^*} \right)_{0^-} = \left(-\frac{D_a}{U_z L} \frac{\partial C_A^*}{\partial z^*} + \frac{\partial C_A^*}{\partial z^*} \right)_{0^+} \quad \text{at } z^*=0$$
$$\frac{\partial C_A^*}{\partial z^*} = 0 \quad \text{at } z^*=1$$

- The dimensionless group $D_a/U_z L$, referred to as the reactor dispersion number, measures the extent of axial dispersion

Conclusions

- **Similar results obtained from two LNT's with different formulations**
- **No significant length effect observed on SCONO_x and Umicore in long and short-cycle experiments with full regeneration**
- **Significant monolith “length effect” on LNT performance in short-cycle experiments with partial regeneration**
 - The longer the sample, the better the performance
- **Observed “length effect” comes from different degrees of lean/rich front axial back-mixing at different linear velocities**
 - The lower the linear velocity (i.e. shorter LNT), the higher the back-mixing
- **Higher back-mixing results in a higher reductant loss via oxidation by O_2**
 - Implication in fuel economy and modeling
 - Need to incorporate back-mixing effect into model
- **Back-mixing could explain in part lab-to-lab discrepancy**
 - Different degrees of back-mixing depending on bench reactor switching valve/gas delivery system specifications
 - In addition to other factors: degreening/pretreatment, sample-to-sample variation

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