

Investigation of NO Oxidation Rate as a Function of LNT Loading

Robert Middleton, Chris Depcik*, Dennis Assanis

Walter E. Lay Automotive Laboratory

University of Michigan

* Currently with University of Kansas

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Introduction

- **Rob Middleton:** New Ph.D. Student working on catalyst modeling
 - About 1 year into study of catalysts
 - Work partially supported by Michigan 21st Century Jobs Fund
- Focus on NO Oxidation as it is the rate limiting step for LNT lean phase operation
- Literature seems to be sparse on comparisons of varying catalysts between large groups



Objective

- Correlate global kinetic LNT model parameters to catalyst formulation and loading
- Goal is to reduce parameter fitting time for new catalysts
 - Hold as many terms constant as possible
 - Pick good initial values for non-constant terms
- Useful for improving formulations / performance



Existing Catalyst Model

- Model developed by Depcik, Assanis, Bevan
 - A one-dimensional lean NO_x trap model with a global kinetic mechanism that includes NH_3 and N_2O , *Int. J. Engine Res.* Vol. 9, 2008
- Uses custom C++/Fortran code
 - Optimization of parameters performed via MATLAB (fmincon)

$$\text{Gas Species: } \frac{\partial \bar{C}_{g,j}}{\partial t} + u \frac{\partial \bar{C}_{g,j}}{\partial x} = \frac{-k_{m,j} G_a}{\varepsilon} (\bar{C}_{g,j} - \bar{C}_{s,j})$$

$$\text{Gas Energy: } \rho_g c_{p,g} \left(\frac{1}{\gamma} \frac{\partial T_g}{\partial t} + u \frac{\partial T_g}{\partial x} \right) = \frac{-h_g G_a}{\varepsilon} (\bar{C}_{g,j} - T_m)$$

$$\text{Fluid Motion: } \frac{d\bar{C}_{s,j}}{dt} = \frac{k_{m,j} G_a}{1-\varepsilon} (\bar{C}_{g,j} - \bar{C}_{s,j}) - \frac{G_{ca} R_j}{1-\varepsilon}$$

$$\text{Surface Intermediates: } \frac{d\Theta_m}{dt} = \frac{\dot{s}_m}{\Gamma}$$

$$\text{Surface Energy: } \rho_m c_m \frac{dT_m}{dt} = \lambda_m \frac{\partial^2 T_m}{\partial x^2} + \frac{h_g G_a}{1-\varepsilon} (T_g - T_m) + \frac{G_{ca}}{1-\varepsilon} \sum_{j=1}^{NM} R_j h_j + \dot{q} + \frac{Q_{i \rightarrow m}}{1-\varepsilon} V_{cat}$$



Existing Catalyst Model

- NO Oxidation reaction $\text{NO} + \frac{1}{2}\text{O}_2 \rightleftharpoons \text{NO}_2$

Rate expression [mol/m³-s]:
$$\mathbf{R} = \frac{k \exp\left(-\frac{E}{R_u T_m}\right) X_{s,\text{NO}} X_{s,\text{O}_2}^{0.5} - X_{s,\text{NO}_2} / K_{eq}}{G}$$

$$G = T_m \left[1 + K_{\text{NO}} \exp\left(-\frac{\Delta H_{\text{NO}}}{R_u T_m}\right) X_{s,\text{NO}}^{0.7} + 1 + K_{\text{H}_2\text{O}} \exp\left(-\frac{\Delta H_{\text{H}_2\text{O}}}{R_u T_m}\right) X_{s,\text{H}_2\text{O}} \right]^2$$

Fit Parameters: k , E , K_{NO} , H_{NO} , $K_{\text{H}_2\text{O}}$, $H_{\text{H}_2\text{O}}$

- Origin of Inhibition terms:
 - NO site occupancy from Voltz (1973)
 - H₂O estimated functional dependence from literature



Method

- Used literature data
 - 13 papers surveyed, 25 sets of data
 - 10 different catalyst formulations, varying loading / dispersion
 - Al_2O_3 -CeO-SiO₂ supports
 - With and without Barium
 - Pd, Pt and Rh as PGM
- Some papers only partially report the reactor setup
 - Assumptions are needed for simulation



Method

- Optimize k , E , K_{NO} , H_{NO} , $K_{\text{H}_2\text{O}}$, $H_{\text{H}_2\text{O}}$ for all data
 - Analyze K_{NO} , H_{NO} , $K_{\text{H}_2\text{O}}$, $H_{\text{H}_2\text{O}}$
 - Hold values constant
- Optimize k , E using constant values for inhibition
 - Look for trends in E
 - Hold E constant – either globally or per material
- Optimize k alone using constant values for other terms
 - Look for trends in k
 - Compare trends to those in the literature



Our Assumptions

- Literature results can be replicated with a monolith
 - Used the geometry from Olsson '99 (clearest definition)
- Inlet velocity is constant
- Flow rates STP

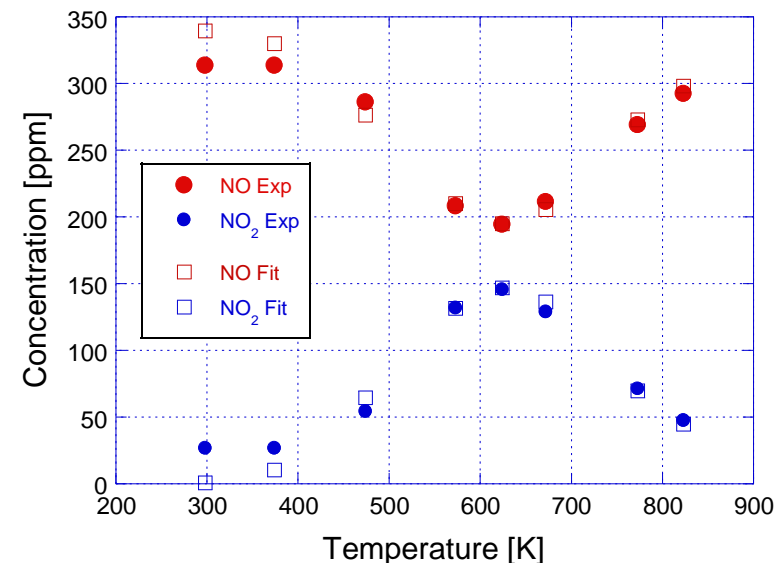
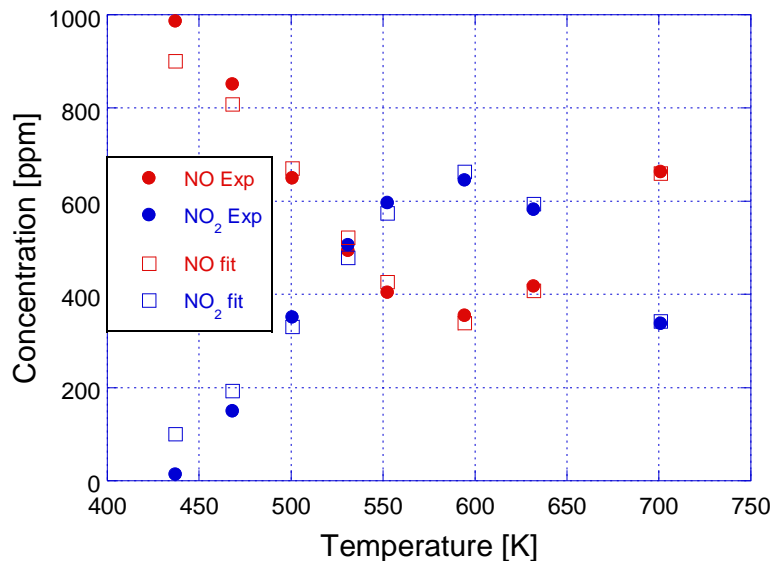
- Assumptions make it hard to compare pre-exponentials
 - Focus on trends under the same set of assumptions
 - Benard '05 shows the effect of Pt dispersion
 - Huang '01 shows the effect of precious metal

- Can still compare activation energies and inhibition terms



Optimizing All 6 Parameters

- The model matches experimental results well
 - Even matches catalysts with unclear descriptions requiring many assumptions
 - Yentikakis '05 has varying flow rates, crushed powder
 - Rodrigues '00 has no geometry reported – no reactor type



Averaging the NO Inhibition

- K_{NO} is less than reported by Voltz

$$1 + K_{NO} \exp \left(-\frac{\Delta H_{NO}}{R_u T_m} \right) X_{s,NO}^{0.7}$$

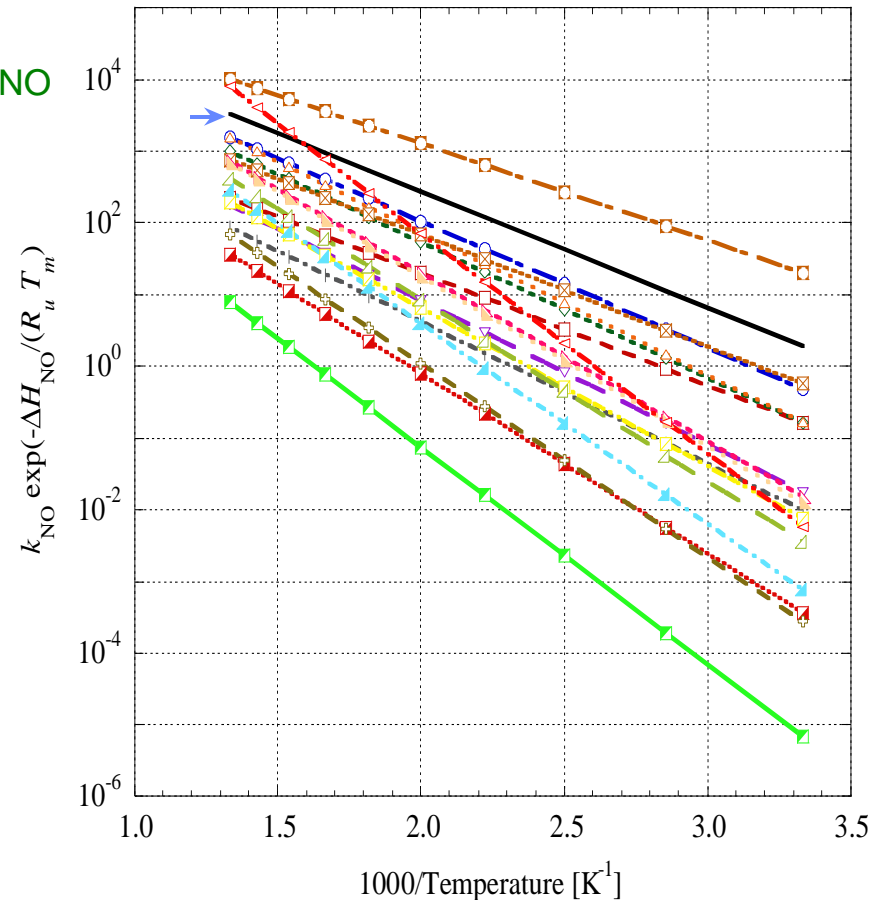
– Large variations seen in K_{NO} and H_{NO}

– Ideally one H_{NO} per material and K_{NO} correlated to loading

– Used average values:

- $K_{NO} = 4.7 \times 10^5$

- $H_{NO} = 41.3 \text{ [KJ/mol]}$



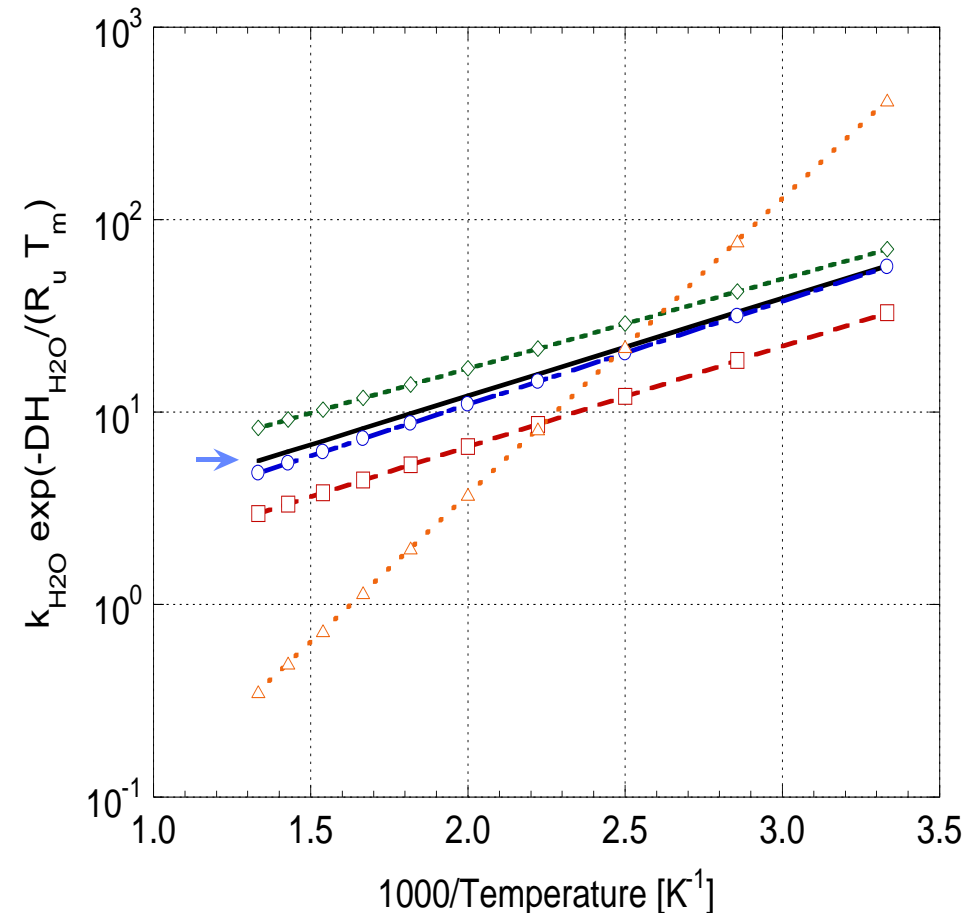
Averaging the H₂O Inhibition

- No literature results for this term

$$1 + K_{\text{H}_2\text{O}} \exp \left(-\frac{\Delta H_{\text{H}_2\text{O}}}{R_u T_m} \right) X_{s,\text{H}_2\text{O}}^2$$

- Only 4 data sets
- Negative activation energy
- Used average values:

- $K_{\text{H}_2\text{O}} = 1.18$
- $H_{\text{H}_2\text{O}} = -9.7$ [KJ/mol]



Method

- Optimize k , E , K_{NO} , H_{NO} , $K_{\text{H}_2\text{O}}$, $H_{\text{H}_2\text{O}}$ for all data
 - Analyze K_{NO} , H_{NO} , $K_{\text{H}_2\text{O}}$, $H_{\text{H}_2\text{O}}$
 - Hold values constant
- Optimize k , E using constant values for inhibition
 - Look for trends in E
 - Hold E constant - globally
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$$\begin{aligned}K_{\text{NO}} &= 4.7 \times 10^5 \\H_{\text{NO}} &= 41.3 \text{ [KJ/mol]} \\K_{\text{H}_2\text{O}} &= 1.18 \\H_{\text{H}_2\text{O}} &= -9.7 \text{ [KJ/mol]}\end{aligned}$$

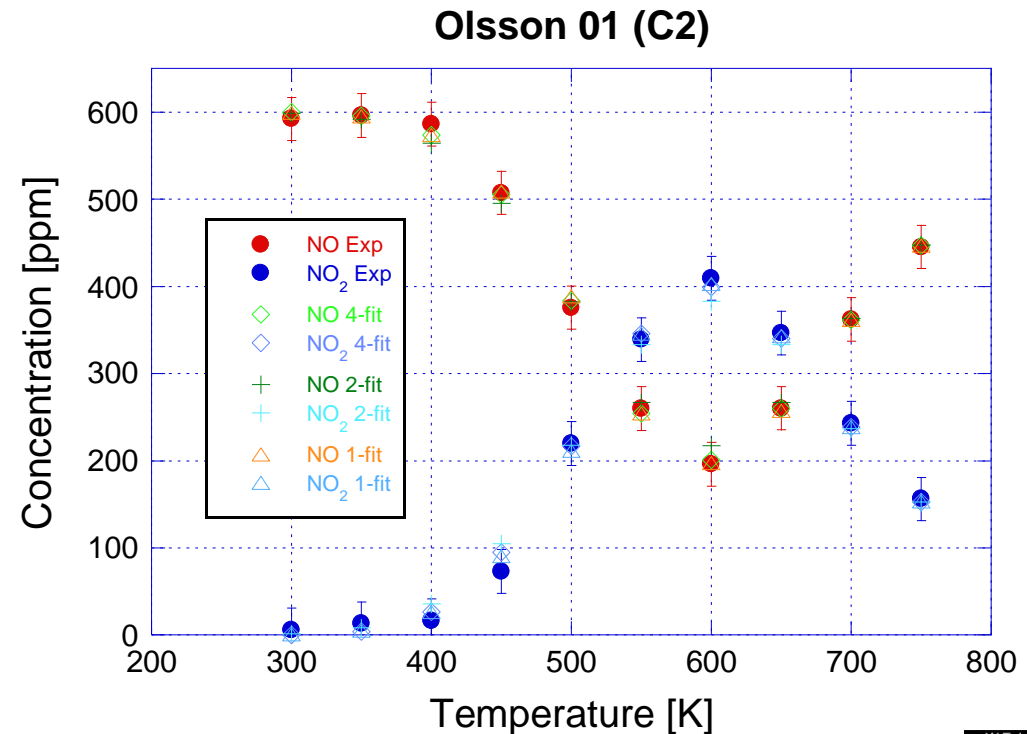
$$E = 39.72 \text{ [KJ/mol]}$$



Change in Accuracy with Constant Terms

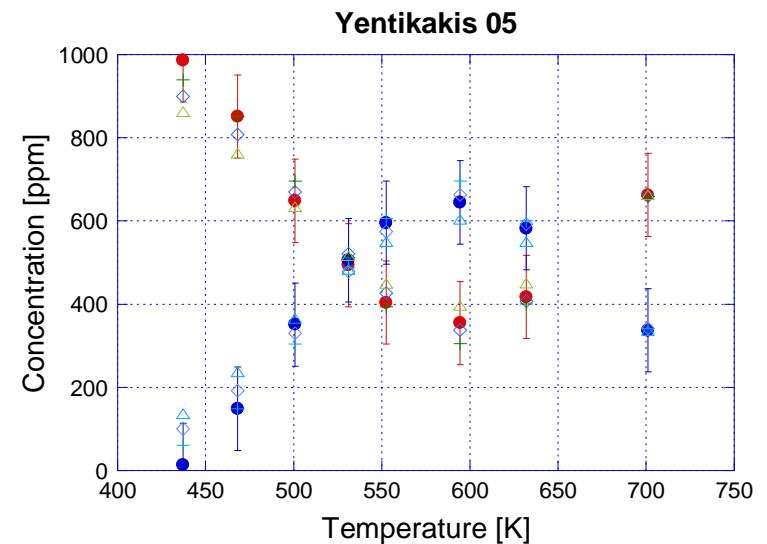
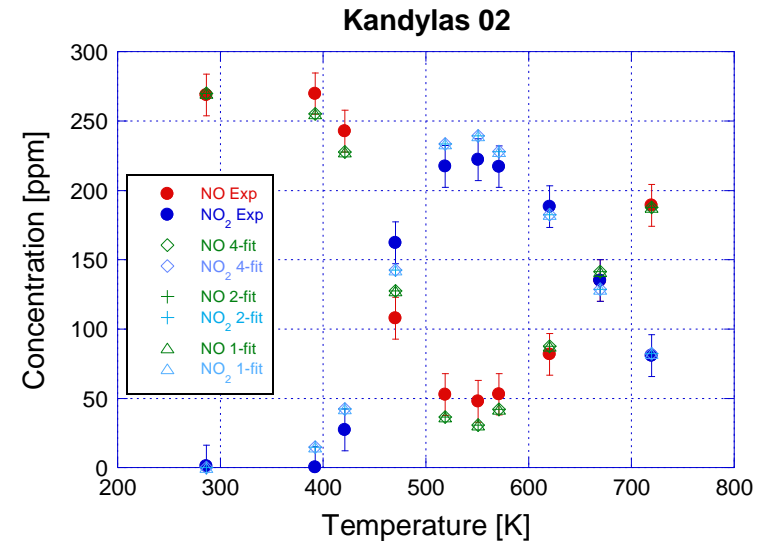
- Reducing the number of fit parameters does not adversely impact the quality of the results
 - Least squares fit increases between $\sim 0.1/\text{pt}$ and $20\text{-}40/\text{pt}$
 - Average increase of $8/\text{pt}$

- Results are within the expected error from reading the literature data
 - LSQ *decreased* from $3.5/\text{pt}$ to $3.34/\text{pt}$
 - Within ± 25 ppm (5% inlet)



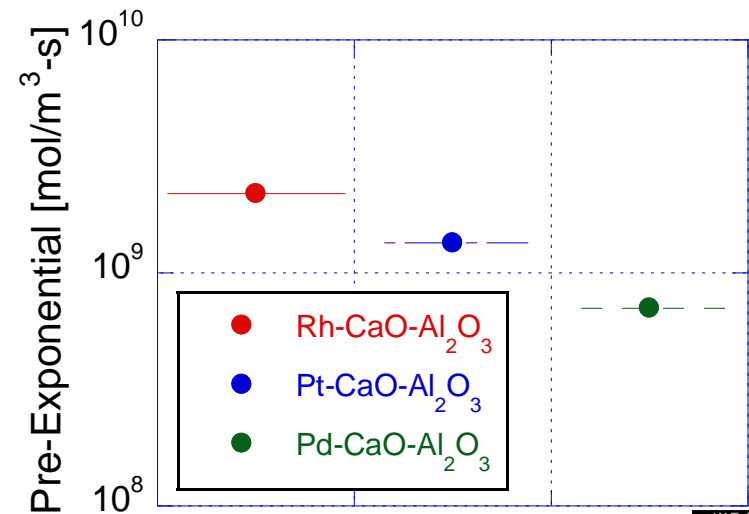
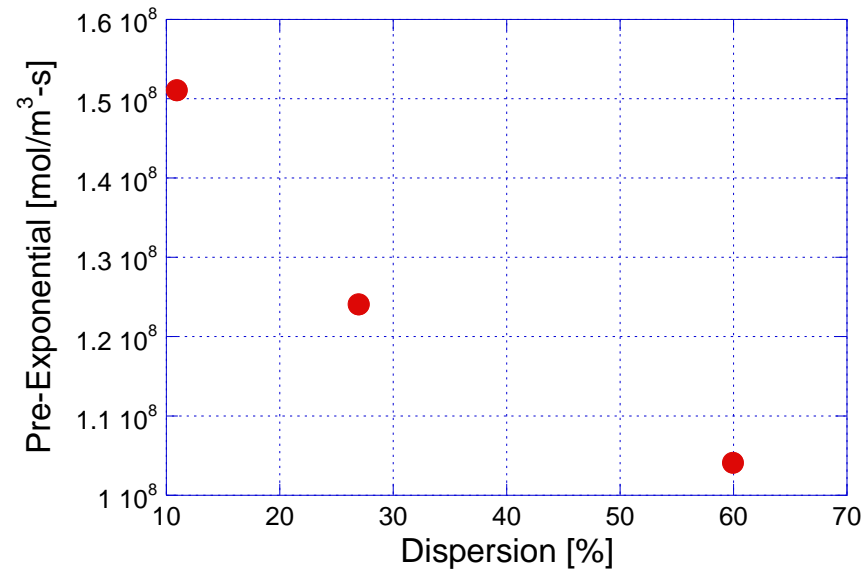
Change in Accuracy with Constant Terms

- From Kandylas '02:
 - LSQ nearly constant at 55 ppm total
 - Within ± 15 ppm (5% of inlet flow)
- From Yentikakis '05:
 - LSQ increases from 150 to 240 ppm
 - Within ± 100 ppm (10% of inlet flow)
- Reducing the number of fit parameters from 6 to 1 decreased the model accuracy by only 5-15%
 - The optimization search space decreased by 5 dimensions
 - Fit time decreased from ~5 hours to less than 1 hour



Effect of Dispersion and Metal Selection

- As a reality check ...
 - Under the same assumptions
 - Can we match literature trends?
- Benard '05 – Pt dispersion
 - Pt-Al₂O₃ – same Pt loading
 - Higher dispersion decreases activity
 - Matches the literature
 - Reportedly due to Pt-O formation
- Huang '01 – metal selection
 - Activity: Rh > Pt > Pd
 - Matches the literature



Lessons Learned

- Model can fit experimental data well over a wide range of catalysts
- Parameter optimization speed can be increased without significant decrease in accuracy by using average inhibition values
- Method looks promising – will continue to add data
 - From the literature
 - In-house via reactor bench
- Many assumptions are needed to use literature data



Acknowledgements

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Questions



Source Data

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